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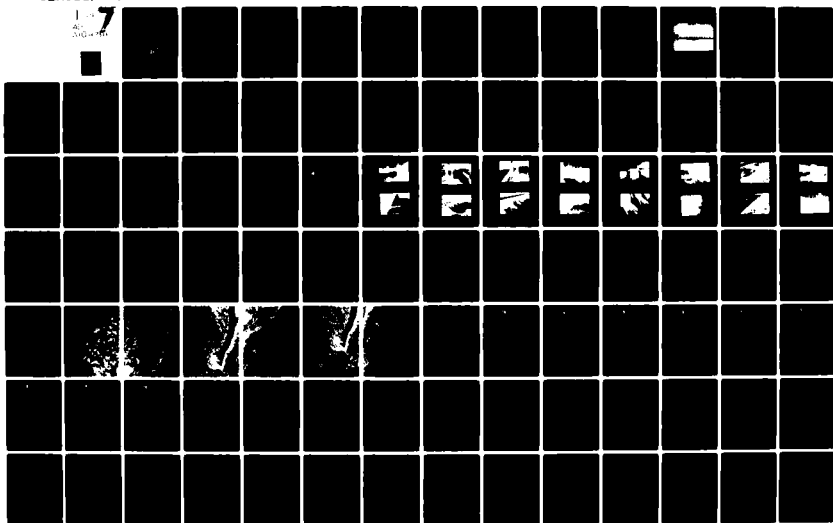
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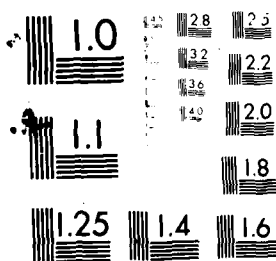
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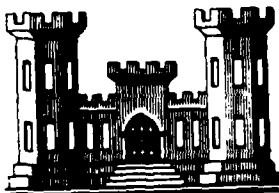
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OTSEGO LAKE DAM

OTSEGO COUNTY, NEW YORK
INVENTORY No. NY 361

PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM



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NEW YORK DISTRICT, CORPS OF ENGINEERS
JULY 1981

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization. Examination of available documents and a visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life or property. However, the dam has some deficiencies that need to be evaluated and remedied. → not for		

Using the Corps of Engineers' screening criteria for the initial review of spillway adequacy, it has been determined that the dam would be overtopped by all storms exceeding 29 percent of the Probable Maximum Flood (PMF) with the flashboards in place and 30 percent without them in place. Dam overtopping, the resulting instability of the overflow spillway and hence, dam breaching would cause water surface levels downstream to reach depths which would pose significant danger to residents. Therefore, the spillway is adjudged to be seriously inadequate and the dam is assessed as unsafe, nonemergency.

The classification "unsafe" applied to a dam because of a seriously inadequate spillway is not meant to connote the same degree of emergency as would be associated with an "unsafe" classification applied for a structural deficiency. It does mean that there appears to be a serious deficiency in spillway capacity and if a severe storm were to occur, overtopping and failure of the dam could take place, significantly increasing the hazard to life downstream of the dam.

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event, a finding that a spillway will not pass the test flood should not be interpreted as necessarily posing a highly inadequate condition. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
OTSEGO LAKE DAM
INVENTORY NO. NY 361
SUSQUEHANNA RIVER BASIN
OTSEGO COUNTY, NEW YORK

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam: Otsego Lake Dam
State Located: New York
County: Otsego
Watershed: Susquehanna River Basin
Watercourse: Susquehanna River
Date of Inspection: April 9, 1981

ASSESSMENT

Examination of available documents and a visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life or property. However, the dam has some deficiencies that need to be evaluated and remedied.

Using the Corps of Engineers' screening criteria for the initial review of spillway adequacy, it has been determined that the dam would be overtopped by all storms exceeding 29 percent of the Probable Maximum Flood (PMF) with the flashboards in place and 30 percent without them in place. Dam overtopping, the resulting instability of the overflow spillway and hence, dam breaching would cause water surface levels downstream to reach depths which would pose significant danger to residents. Therefore, the spillway is adjudged to be seriously inadequate and the dam is assessed as unsafe, nonemergency.

The classification "unsafe" applied to a dam because of a seriously inadequate spillway is not meant to connote the same degree of emergency as would be associated with an "unsafe" classification applied for a structural deficiency. It does mean that there appears to be a serious deficiency in spillway capacity and if a severe storm were to occur, overtopping and failure of the dam could take place, significantly increasing the hazard to life downstream of the dam.

It is recommended that the following additional investigations be performed by a registered professional engineer engaged by the owner:

1. Conduct a detailed hydrologic and hydraulic analysis to more accurately determine the site specific characteristics of the watershed.

2. Systematically investigate the seepage behind the left abutment wall and monitor it on a continuing basis, especially during periods of high flow. If the rate and extent of the seepage progressively increase, assess the causes of the seepage and recommend remedial measures.
3. Evaluate existing structural conditions based upon inspection of the dam sections and abutment structures with the reservoir drawn down.
4. Evaluate the structure including the interior of the dam to determine the condition of the underside of the old section and the joint between the two sections.
5. Evaluate the presence and magnitude of the uplift due to the theoretical forces acting on the base during operation with the flashboards in place and the assumed maximum flow.
6. Perform dam stability analyses based on actual existing conditions and if necessary, make recommendations to improve the stability of the dam.

It is recommended that within 3 months of the final approval date of this report, all of the additional investigations should be initiated and within 18 months, appropriate remedial measures should be completed. In the interim, a plan for providing around-the-clock surveillance of the dam during periods of unusually heavy precipitation should be developed and implemented.


The following remedial measures should be completed within 12 months to correct existing deficiencies:

1. Replace the existing steel H-beam posts having the buckled webs with new sections having reinforced webs and flanges or with a more "compact" H-beam post.
2. The bent steel channel braces should be replaced and all channel braces should be reinforced by welding a like, or similar channel (legs welded to legs) to make up a "box", thereby increasing its resistance to bending and torsion.
3. All spalled areas or minor cracks in concrete should be re-pointed with a nonshrink epoxy cement.
4. Repair or replace:
 - a. the concrete grouted rock slope protection at the toe of the right abutment wall which has experienced some minor erosion.
 - b. the rock slope protection which is in a deteriorated condition elsewhere on the right downstream slope within the stilling basin.

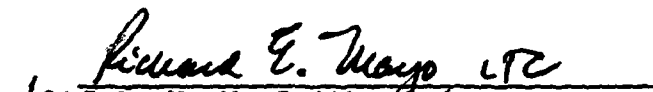
5. Develop and implement a flood warning and emergency evacuation plan to alert the downstream residents in the event conditions occur which could result in failure of the dam.
6. A program for regular maintenance should be developed and implemented.

Submitted by:

FLAHERTY GIAVARA ASSOCIATES, P.C.


Hugh C. Flaherty, P.E. & L.S.
Chairman of the Board
New York License No. 58508

Approved by:

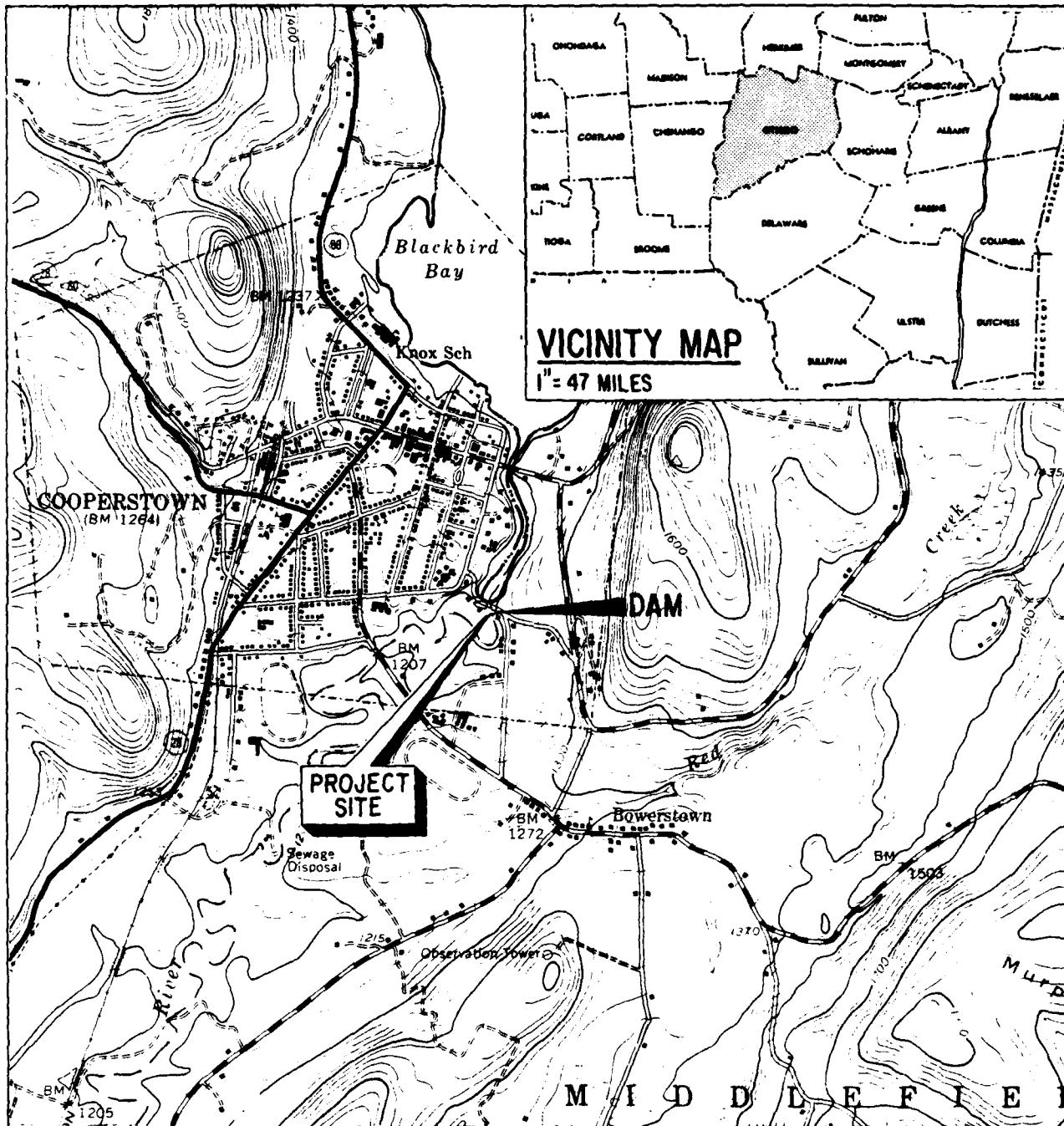

for Col. W. M. Smith, Jr.
New York District Engineer

Date:

17 SEPT 1987

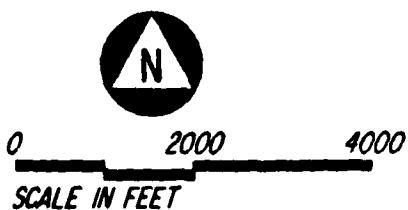


PHOTO #1: Overview of
Otsego Lake Dam
Inventory No. NY 361



LOCATION MAP

OTSEGO LAKE DAM
INVENTORY No. NY 361
SUSQUEHANNA RIVER BASIN
OTSEGO COUNTY
OTSEGO & MIDDLEFIELD, NEW YORK



FLAHERTY • GIAVARA ASSOCIATES, P.C.

NATIONAL DAM SAFETY PROGRAM
PHASE I INSPECTION REPORT
OTSEGO LAKE DAM
INVENTORY NO. NY 361
D.E.C. NO. 144A-918
SUSQUEHANNA RIVER BASIN
OTSEGO COUNTY, NEW YORK

SECTION 1 - PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase I Inspection reported herein was authorized by the Department of the Army, New York District, Corps of Engineers, to fulfill the requirements of the National Dam Inspection Act, Public Law 92-367. Flaherty Giavara Associates, P.C. has been retained by the New York District to inspect and report on selected dams in the State of New York. Authorization and notice to proceed was issued to Flaherty Giavara Associates, P.C. under a letter of December 24, 1980 from W. M. Smith Jr., Colonel, Corps of Engineers. Contract No. DACW 51-81-C-0006 has been assigned by the Corps of Engineers for this work.

b. Purpose

Evaluation of the existing conditions of the subject dam to identify deficiencies and hazardous conditions, determine if they constitute hazards to life and property and recommend remedial measures where necessary.

1.2 DESCRIPTION OF PROJECT

a. Description of Dam and Appurtenances

The Otsego Lake Dam is a concrete buttress structure consisting of an overflow spillway weir with flashboards and an apron, and spans the entire width of the outlet channel. The original dam was a concrete gravity structure which was rehabilitated in 1955 with concrete counterforts, a reinforcement to the spillway, steel H-beam sections braced with channels (for flashboards), pile supports and a timber plank walkway across the overflow spillway. The new structural steel sections were embedded into the new concrete. A plan and sections showing these modifications are included in Appendix G. Concrete abutment or retaining walls extend upstream at both ends of the overflow spillway and tie into the abutments of a highway bridge located approximately 50 feet from the dam. The overall length of the dam is approximately 70

feet and the height is 11 feet. A stilling basin equal to the width of the overflow spillway, extends 200+ feet downstream of the dam. The discharge channel is lined with boulders and cobbles and narrows downstream of the dam. The side slopes on the left side of the discharge channel are approximately 3 to 4 horizontal to 1 vertical near the bottom and steepen to approximately 1.5 to 2.5 horizontal to 1 vertical for an approximate height of 9 feet. A flat paved parking area exists above the right slope of the discharge channel. The left slope is grass and tree-covered and the right slope is covered with rock slope protection and miscellaneous concrete rubble. The rock slope protection behind and immediately downstream of the right abutment is grouted with concrete.

b. Location

The Otsego Lake Dam is located off Mill Street within the Village of Cooperstown in the Towns of Otsego and Middlefield, New York. The dam is located at latitude north $42^{\circ}-41.6'$ and longitude west $74^{\circ}-55.3'$ on the U.S. Geological Survey 7.5 minute series topographic map "Cooperstown, New York". The Location Map on page i indicates where the dam is situated.

c. Size Classification

The maximum height of the dam is 11 feet and the maximum storage capacity is 39,800 acre-feet at the top of dam. Therefore, Otsego Lake Dam is classified as an "Intermediate" dam as defined by the Recommended Guidelines for Safety Inspection of Dams.

d. Hazard Classification

There are three roads, approximately 2 buildings, two railroad crossings and a sewage treatment plant within the dam failure flood hazard area. Therefore, the dam is in the "High" hazard category as defined by the Recommended Guidelines for Safety Inspection of Dams.

e. Ownership

The dam is owned by the Village of Cooperstown. The address and telephone number are as follows:

Owner

Contact: Mr. Edward M. Gaynor
Director of Public Works
Village of Cooperstown
22 Main Street
Cooperstown, New York 13326

Telephone: (607) 547-2411

f. Purpose

Originally, the dam was constructed to provide hydropower for milling purposes. This power source was later used to operate water pumps for the Village Water Works. Sometime thereafter, the sluiceway used for the power generation was filled in (see the Location Map on page i). Presently, the purposes of this dam are to maintain the water level of Otsego Lake for recreational use, to regulate the stream flow of the Susquehanna River and to provide a water supply for the Village of Cooperstown.

g. Design and Construction History

The original date of construction is not known; however, according to a report dated March 17, 1913 which is included in Appendix E, it was sometime prior to 1910 when the dam was repaired.

The only other post construction modifications noted were the reconstruction of the spillway and the installation of the flashboards and walkway in 1955 and the raising of of the height of the spillway abutments in 1964 or 1965.

h. Normal Operating Procedure

The only regular operating procedure for this dam includes the insertion or removal of the flashboards to regulate the level of Otsego Lake as well as the Susquehanna River. The normal water level in the lake is maintained by the crest elevation of the overflow spillway weir at approximately 1190.0 (NGVD).

1.3 PERTINENT DATA

a. <u>Drainage Area (Square Miles)</u>	75.00
b. <u>Discharge at Dam Site (CFS)</u>	
- Top of Dam	
without flashboards	1428
with flashboards	758
- Top of Flashboards	
without flashboards	348
with flashboards	9
- Crest of Overflow Spillway	-

c. Elevations (NGVD - estimated)

- Top of Dam	1194.2
- Top of Flashboards	1191.6
- Low Flow Notch	1191.1
- Crest of Overflow Spillway	1190.0

d. Reservoir Surface Area (Acres)

- Top of Dam	4,272
- Top of Flashboards	4,158
- Crest of Overflow Spillway	4,088

e. Storage (Acre-Feet)

- Top of Dam	39,800
- Top of Flashboards	27,400
- Crest of Overflow Spillway	20,440

f. Dam

- Type: Concrete buttress with concrete abutments and wingwalls	
- Length (Feet)	69.5
- Upstream Slope (H:V)	vertical
- Downstream Slope (H:V)	-
- Crest Width (Feet)	2.0

g. Overflow Spillway

- Type: Concrete spillway with timber plank walkway	
- Length (Feet)	67.5
- Width (Feet)	12
- Side Slopes (H:V)	vertical
- Channel Bottom Slopes (Feet/Foot)	-
- Control: Adjustable flashboards	

h. Reservoir Drain

No reservoir drain is known to exist.

SECTION 2 - ENGINEERING DATA

2.1 GEOTECHNICAL DATA

a. Geology

The Otsego Lake Dam is located at the headwaters of the Susquehanna River, approximately one half mile south of Otsego Lake, in the Village of Cooperstown, New York. It is situated in the Allegheny Plateau physiographic province of New York State. Local topography ranges from elevation 1200+ in the floodplain downstream from the dam to elevation 1720 atop the hill northeast of the site. The elevation of Otsego Lake is 1190± (NGVD).

The underlying bedrock at the site is probably the Marcellus Formation, belonging to the Middle Devonian Hamilton group. This formation consists mostly of fine-bedded, dark grey to black, silty shales. The bedding of these deposits is quite even and laminated, splitting readily into thin sheets upon exposure.

The bedrock is probably overlain by a deposit of glacial till, a heterogeneous mixture of clay, silt, sand, gravel, and cobbles deposited beneath a glacier ice sheet, which once covered this region. Overlying the till is probably a deposit of lacustrine clays and/or fine-grained fluvial channel and overbank deposits of the present-day Susquehanna River.

b. Subsurface Conditions

There is no record of subsurface explorations at the site of the Otsego Lake Dam.

2.2 DESIGN RECORDS

No design records were obtained for this dam.

2.3 CONSTRUCTION RECORDS

This dam was constructed sometime prior to 1910, when the dam was repaired and it was reconstructed in 1955. A plan and sections showing these modifications are included in Appendix G. No other construction records were obtained.

2.4 OPERATION RECORDS

The level of Otsego Lake is recorded daily; however, no operation records were obtained for this dam.

2.5 EVALUATION OF DATA

The data presented herein was obtained primarily from the files of the New York State Department of Environmental Conservation (DEC) and also from the Village Water Works in Cooperstown. This information appears to be reliable and adequate for the purposes of a Phase I Inspection Report.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

a. General

A visual inspection of the Otsego Lake Dam was conducted on April 9, 1981. The weather was overcast and the temperature was 55+°F. At the time of the inspection, water was flowing in the overflow spillway (See Photos No. 5 and 7).

b. Dam

The dam is generally in good condition (See Photos No. 3, 4, 5, 6 and 7). There was no visible evidence of lateral movement, settlement, or cracking of the dam.

The following specific items were noted:

1. Seepage was noted along the earthen side of the left abutment wall near the base of the weir, approximately 6.5 feet below the top of the wall (See Photos No. 14 and 15). Minor seepage was noted along an old masonry and concrete wall.
2. Minor undermining of the right concrete abutment wall and of the grouted slope protection downstream of the abutment wall was noted (See Photo No. 13).
3. A separation crack has developed between the right abutment and the downstream retaining wall (See Photo No. 12).
4. The rock slope protection on the right slope of the downstream discharge channel within the stilling basin is in poor condition (See Photo No. 16). In some places it has been eroded away or displaced.
5. Some erosion of the left slope of the downstream discharge channel was observed (See Photo No. 17).

c. Overflow Spillway

The overflow spillway consists of a 67.5 foot long broad-crested weir and stilling basin (See Photo No. 8). The spillway has 1.6 foot high flashboards which are supported by concrete counterforts and steel H-beam posts braced with steel channel sections. The upstream flange of the steel H-beam posts has been reinforced by welding a 3/8 inch thick steel plate to the flange (See Photo No. 10). The upstream face and sides of the concrete counterforts (which are exposed to flow) have been "armored" with a

3/8 inch thick steel plate (See Photo No. 6).

The following specific items were observed:

1. The second and third steel H-beam posts from the right abutment are bent out of their planned vertical alignment.
2. The webs of the second, third, and fourth steel H-beam posts show evidence of buckling; i.e., the flanges are not parallel (See Photo No. 10).
3. The channel braces for the second and third steel H-beam posts are bent, approximately 6 inches from its vertical axis for the second post and 8 inches for the third post (See Photos No. 7 and 11).
4. The timber plank walkway is in good condition (See Photos No. 3 and 6).

d. Downstream Channel

The natural channel downstream of the dam is in good condition having a bed of gravel, a width of 25+ feet and a depth of 24 inches (See Photo No. 9).

e. Reservoir - Storage Pool Area

The reservoir area is bordered on the right by moderate to steep slopes, approximately 15 to 20 feet high, and on the left by very flat and gentle tree-covered slopes (See Photo No. 2). Sloughing at the base of the right slopes is apparently due to wave action, and a few trees have collapsed into the water; however, there is no significant possibility of major landslides into the storage pool affecting the safety of the dam.

3.2 EVALUATION OF OBSERVATIONS

The visual inspection revealed several deficiencies on this structure. The following observations were made:

- a. Seepage was observed along the earthen side of the left abutment wall.
- b. The second and third steel H-beam posts from the right abutment were bent out of their planned vertical alignment.
- c. The webs of the second, third and fourth steel H-beam posts showed evidence of buckling.

- d. The steel channel braces for the second and third steel H-beam posts were bent.
- e. Minor undermining of the right concrete abutment wall and of the slope protection downstream from this wall was evident.
- f. A separation crack was observed between the right abutment and the downstream retaining wall.
- g. The rock slope protection on the right slope of the downstream discharge channel was eroded or displaced.
- h. Some erosion of the left downstream channel was noted.

SECTION 4 - OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

The normal water surface level is maintained by the flashboards. The only operational procedure in effect at this time is the insertion or removal of the flashboards to regulate the level of Otsego Lake as well as that of the Susquehanna River.

4.2 MAINTENANCE OF DAM

There was no evidence of any routine maintenance operations at the Otsego Lake Dam.

4.3 WARNING SYSTEM

No warning system is presently in effect.

4.4 EVALUATION

Presently, only a few maintenance procedures are in effect for this dam. Therefore, a program for regular maintenance should be developed and implemented.

SECTION 5 - HYDROLOGIC/HYDRAULIC

5.1 DRAINAGE AREA CHARACTERISTICS

The dam is located in the Towns of Otsego and Middlefield, approximately one half mile downstream of Otsego Lake in the Village of Cooperstown. Otsego Lake is at the headwaters to the Susquehanna River, approximately twenty-two miles upstream of Oneonta, New York.

The watershed (shown on the Watershed Map on Page C-5 in Appendix C) consists of 48,000 acres (75.00 square miles) of hilly uplands with typical slopes of 10 percent. Land within the watershed is primarily agricultural with extensive open fields.

The watercourse upon which the reservoir is located, is the Susquehanna River, having a typical flow width of 25 feet and a typical flow depth of 24 inches.

5.2 ANALYSIS CRITERIA

The purpose of the hydrologic/hydraulic analysis is to evaluate the spillway capacity and the potential for overtopping. The analysis of the spillway capacity of the dam and storage of the reservoir was performed using the Corps of Engineers' HEC-1 Computer Model - Dam Safety Version. The procedure included determining the Probable Maximum Flood (PMF) runoff from the watershed and routing the inflow hydrograph through the impoundment to determine the outflow hydrograph. The unit hydrograph was defined by the Snyder Synthetic Unit Hydrograph method, and the Modified Puls routing procedure was incorporated.

The initial rainfall loss was assumed to be 1.0 inches, and the uniform rainfall loss was assumed to be 0.1 inches per hour. In accordance with recommended guidelines of the Corps of Engineers, the Probable Maximum Precipitation (PMP) was 19.3 inches (24 hour duration, 200 square mile area).

The drainage area of Otsego Lake was divided up into seven subwatershed areas for the HEC-1 DB computer model. Runoff unit hydrographs and peak lag times were developed for each subwatershed and combined before being routed through the dam. Due to its large ratio of surface area to watershed area, the impoundment was treated as a separate subwatershed and as being impervious in the analysis. Other impervious surfaces in the watershed were estimated from the USGS 7.5 minutes series topographic maps.

The dam is located approximately 0.5 miles downstream of Otsego Lake and is connected to the lake via a 100+ foot wide channel. Due to the effect of flow restriction, it was nec-

essary to perform a backwater analysis of the channel under PMF flow conditions to determine the resulting additional storage in the lake. The results of this analysis are included in Appendix C.

Two analyses were conducted for both the full PMF and for several fractional PMF conditions; one with the spillway flashboards in place and the other without them in place. The PMF inflow of 81,113 CFS was routed through the reservoir and the peak outflow was determined to be 11,660 CFS with the flashboards and 12,831 CFS without them.

5.3 SPILLWAY CAPACITY

The total outlet capacity is the discharge from the overflow spillway. There were seven sets of removable flashboards in place at the time of the inspection; six sets were 1.6 feet high by 8.9 feet long and one was 1.6 feet by 8.6 feet. The length of the overflow section of the weir is 67.5 feet.

The stage discharge data for the overflow spillway weir with the flashboards in place was calculated for the stages tabulated below:

<u>Stage (Feet)</u>	<u>Discharge Capacity (CFS)</u>	<u>Element of Structure</u>
1191.1	0	Low-Flow Notch
1191.6	9	Top of Flashboards
1192.0	58	--
1192.5	166	--
1192.8	248	Bottom of Walkway
1192.9	307	Top of Walkway
1193.0	324	--
1193.1	351	Top of H-Beam Posts
1193.5	482	--
1194.0	624	--
1194.2	758	Top of Dam

The total spillway capacity at the top of dam is 758 CFS.

The stage discharge data for the overflow spillway weir without the flashboards in place was calculated for the stages tabulated below:

<u>Stage (Feet)</u>	<u>Discharge Capacity (CFS)</u>	<u>Element of Structure</u>
1190.0	0	Crest of Overflow Spillway
1190.5	25	--
1191.0	172	--

1191.5	316	--
1192.0	486	--
1192.5	679	--
1192.8	732	Bottom of Walkway
1192.9	783	Top of Walkway
1193.0	813	--
1193.1	858	Top of H-Beam Posts
1193.5	1053	--
1194.0	1317	--
1194.2	1428	Top of Dam

The total spillway capacity at the top of the dam is 1428 CFS.

5.4 RESERVOIR CAPACITY

The storage capacity of the reservoir was calculated for the stages indicated below:

<u>Stage (Feet)</u>	<u>Storage (Acre-Feet)</u>	<u>Storage (Inches of Runoff)</u>
1190.0	20,440	5.11
1191.6	27,440	6.86
1194.2	39,800	9.95

5.5 FLOODS OF RECORD

No precise data regarding flood levels was obtained for this dam; however, it was estimated that during one period of high spillway discharge (since 1955), the water level rose to 1+ foot over the timber plank walkway (elevation 1193.9+ NGVD). This would be equal to a flow of 633 CFS with the flashboards in place and 1263 CFS without them.

5.6 OVERTOPPING POTENTIAL

The results of the HEC-1 DB computer analyses indicate that the crest of the dam is overtopped by all storms exceeding 29 percent of the PMF event with the flashboards in place and 30 percent without them in place. The PMF discharge rate of 11,660 cubic feet per second (CFS) with the flashboards in place would occur at a peak flood stage of 1207.4 feet, which is 13.2 feet above the crest of the dam. Without the flashboards in place, the PMF discharge rate of 12,831 CFS peaks at elevation 1206.9 which is 12.7 feet above the crest of the dam.

The results of the analyses are tabulated on the following page:

- With the flashboards in place:

<u>Flood Condition</u>	<u>Peak Inflow (CFS)</u>	<u>Peak Outflow (CFS)</u>	<u>Maximum Stage Elevation (NGVD)</u>
0.5 PMF	40,557	3,317	1198.9
1.0 PMF	81,113	11,660	1207.4

- Without the flashboards in place:

<u>Flood Condition</u>	<u>Peak Inflow (CFS)</u>	<u>Peak Outflow (CFS)</u>	<u>Maximum Stage Elevation (NGVD)</u>
0.5 PMF	40,557	4,092	1197.9
1.0 PMF	81,113	12,831	1206.9

5.7 EVALUATION

Using the Corps of Engineers' screening criteria for the initial review of spillway adequacy, it has been determined that the capacity of the spillway is not adequate to pass either the full PMF or one half the PMF, with or without the flashboards in place.

The extent of overtopping is summarized in the table below:

<u>Flashboards</u>	<u>Ratio of PMF Passed Safely (Percent)</u>	<u>Maximum Depth Over Dam (Feet)</u>	<u>Duration Over Top of Dam (Hours)</u>
With	29	13.2	18.5
Without	30	12.7	18.5

It is estimated that breaching of the dam as a result of overtopping and instability of the overflow spillway, would cause water surface levels downstream to reach depths which would pose significant danger to residents. Therefore, the spillway is adjudged to be seriously inadequate and the dam is assessed as unsafe, nonemergency.

SECTION 6 - STRUCTURAL STABILITY

6.1 EVALUATION OF STRUCTURAL STABILITY

a. Visual Observations

Except for the bent steel H-beam posts with the buckled webs and the bent steel channel braces, both of which support the flashboards, there was no visible evidence of settlement, lateral movement, or other signs of overall structural instability of the dam during the site examination. Based on the conditions that were observed, there is no reason to question the static structural stability of the dam.

b. Design and Construction Data

There is no construction data to confirm the nature and physical properties of the foundation bearing materials. The apparent satisfactory performance of the dam indicates that there is some safety margin with respect to stability under static loading conditions and that the seepage beneath the dam is not a significant problem.

c. Operating Records

No operating records were obtained for Otsego Lake Dam.

d. Post Construction Changes

The only post construction changes noted were the reconstruction of the spillway and the installation of the flashboards and timber plank walkway in 1955 and the raising of the height of the spillway abutments in 1964 or 1965.

6.2 STRUCTURAL STABILITY ANALYSIS

Design drawings available for review show a plan and cross sections for the dam and overflow spillway but do not include information on the properties of the dam and its foundation materials. As part of the present study, stability evaluations have been performed for the overflow spillway sections. Actual properties of the construction materials and foundations were not determined as part of this study; therefore, where information on properties was necessary for computations but was lacking, assumptions felt to be practical were made. The stability computations assume a composite structural cross section based on dimensions indicated by the drawing included in Appendix G of this report.

The stability analysis is presented in Appendix D. The results of the stability computations are summarized in the

following table:

Loading Condition (Spillway Section)	¹ Factors of Safety		³ Location of Resultant Passing Through Base
	Over- turning	² Sliding	
1. Normal operating condition: water 3 feet above existing gravity section (flashboards in place)	5.60	1.75	0.60b
2. Maximum operating condition: water level at top of dam (4.2 feet above spillway crest)	3.94	1.40	0.55b
3. 0.5 PMF condition (with flashboards): water level at El. 1198.9 (7.3 feet above flashboards)	1.56	0.70	0.27b
4. 0.5 PMF condition (without flashboards): water level at El. 1197.9 (7.9 feet above spillway crest)	1.65	0.84	0.27b
5. Ice loading condition: 5.0 Kips per foot acting at top of flashboards	0.93	0.65	*

¹These factors of safety indicate the ratio of moments resisting overturning to those moments causing overturning and the ratio of forces resisting sliding to those causing sliding.

²As determined applying the friction-shear method.

³Indicated in terms of the base dimension of the dam (b), measured from the toe of the dam.

* Location of the resultant falls outside of

the spillway width.

The analysis indicates that the combined sections are stable against overturning for all normal operating conditions to and including the maximum height of water (equal to the top of dam). Instability is indicated when the sections are subjected to forces possible under ice loading conditions and both 0.5 PMF loading conditions.

For nearly all conditions of loading, the factors of safety against sliding were very low; this in part was due to the assumed active soil pressure upstream and a typical coefficient of sliding friction.

Tension stresses produced in the concrete base section due to uplift forces are negligible compared with the mass of the base and reinforcing provided.

The discussed analysis applies to the composite sections of the dam acting monolithically and in structurally good condition. The field observations indicate some damaged structural elements and varying degrees of surface deterioration. Although this analysis indicates generally satisfactory stability under normal operating conditions, severe loading conditions, such as ice or 0.5 PMF, result in unsatisfactory stability. Therefore, a more detailed structural stability analysis is necessary, taking into account the actual conditions and composition of the dam. Remedial measures deemed appropriate as a result of the stability investigation should then be accomplished.

The Otsego Lake Dam is located in Seismic Zone 1 and in accordance with recommended Phase I guidelines does not require seismic analysis.

SECTION 7 - ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Condition

On the basis of the visual examination, there were no signs of impending structural failure or other conditions which would warrant urgent remedial action, but several deficiencies were noted.

b. Adequacy of Information

The evaluation of this dam is based primarily on visual examination, reference to the 1953 plan, approximate hydraulic and hydrologic computations, and application of engineering judgement. No information was available on the nature of the foundation soils. The available information that was obtained is adequate for the purposes of a Phase I assessment.

c. Need for Additional Investigations

It is recommended that the following additional investigations be performed by a registered professional engineer engaged by the owner:

1. Conduct a detailed hydrologic and hydraulic analysis to more accurately determine the site specific characteristics of the watershed.
2. Systematically investigate the seepage behind the left abutment wall and monitor it on a continuing basis, especially during periods of high flow. If the rate and extent of the seepage progressively increase, assess the causes of the seepage and recommend remedial measures.
3. Evaluate the existing structural conditions based upon inspection of the dam sections and abutment structures with the reservoir drawn down.
4. Evaluate the structure including the interior of the dam to determine the condition of the underside of the old section and the joint between the two sections.
5. Evaluate the presence and magnitude of the uplift due to the theoretical forces acting on the base during operation with the flashboards in place and the assumed maximum flow.

6. Perform dam stability analyses based on the actual existing conditions and if necessary, make recommendations to improve the stability of the dam.

d. Urgency

It is recommended that within 3 months of the final approval date of this report, all of the additional investigations should be initiated and within 18 months, appropriate remedial measures should be completed. In the interim, a plan for providing around-the-clock surveillance of the dam during periods of unusually heavy precipitation should be developed and implemented. The recommended corrective measures presented in Section 7.2 should be completed within 12 months of final approval.

7.2 RECOMMENDED MEASURES

It is considered important that the following items be accomplished in addition to any items required as a result of the additional investigations recommended in Section 7.1c:

- a. Replace the existing steel H-beam posts having the buckled webs with new sections having reinforced webs and flanges or with a more "compact" H-beam post.
- b. The bent steel channel braces should be replaced and all channel braces should be reinforced by welding a like, or similar channel (legs welded to legs) to make up a "box", thereby increasing its resistance to bending and torsion.
- c. All spalled areas or minor cracks in concrete should be repointed with a nonshrink epoxy cement.
- d. Repair or replace:
 1. the concrete grouted rock slope protection at the toe of the right abutment wall which has experienced some minor erosion.
 2. the rock slope protection which is in a deteriorated condition elsewhere on the right downstream slope within the stilling basin.
- e. Develop and implement a flood warning and emergency evacuation plan to alert downstream residents in the event conditions occur which could result in the failure of the dam.
- f. A program for regular maintenance should be developed and implemented.

APPENDIX A
PHOTOGRAPHS

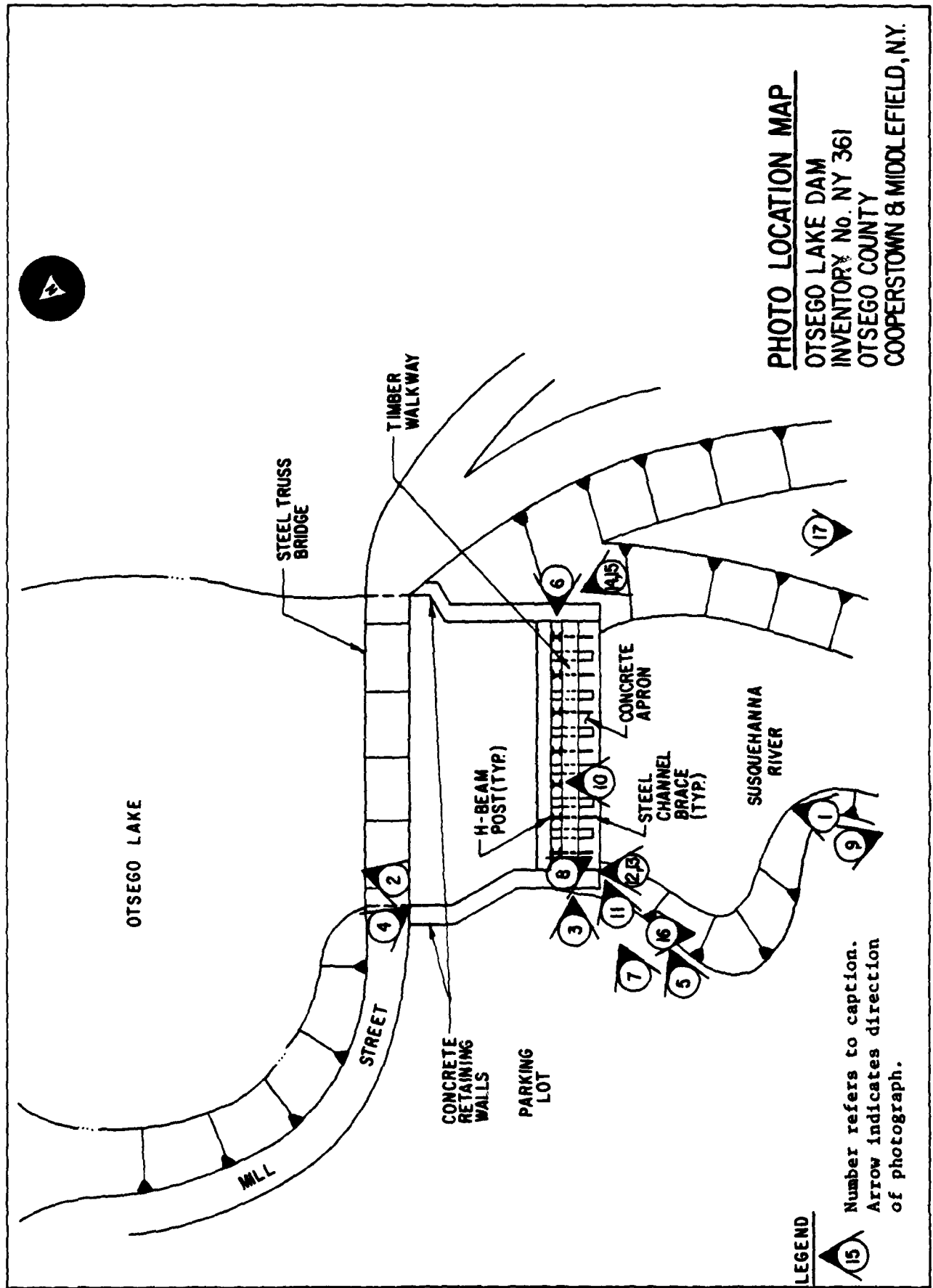




PHOTO #2: Approach channel from Otsego Lake

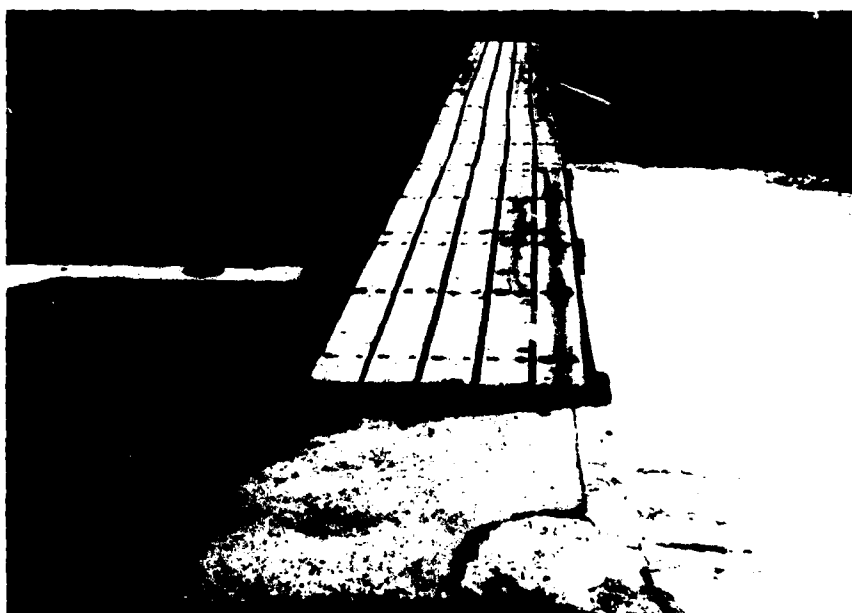


PHOTO #3: Crest of dam looking toward
left abutment

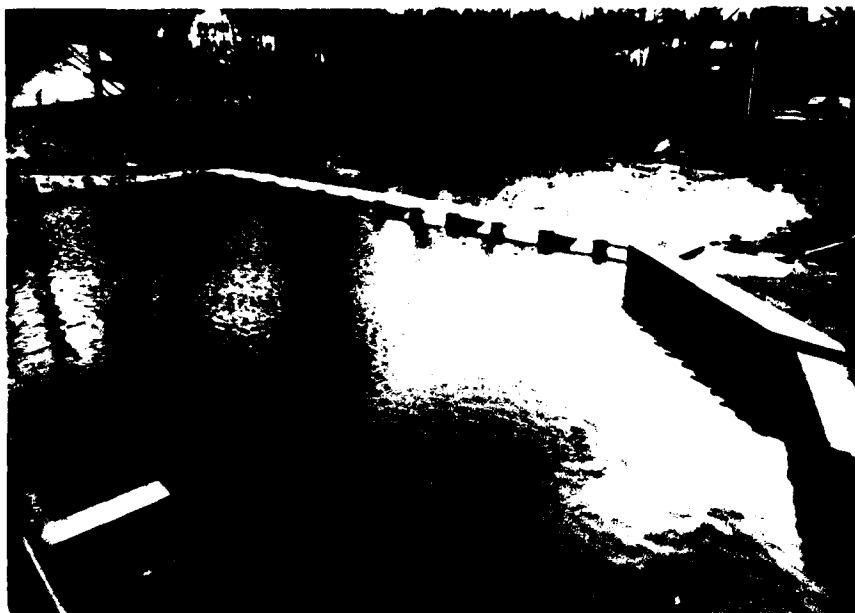


PHOTO #4: Overview of upstream face of dam

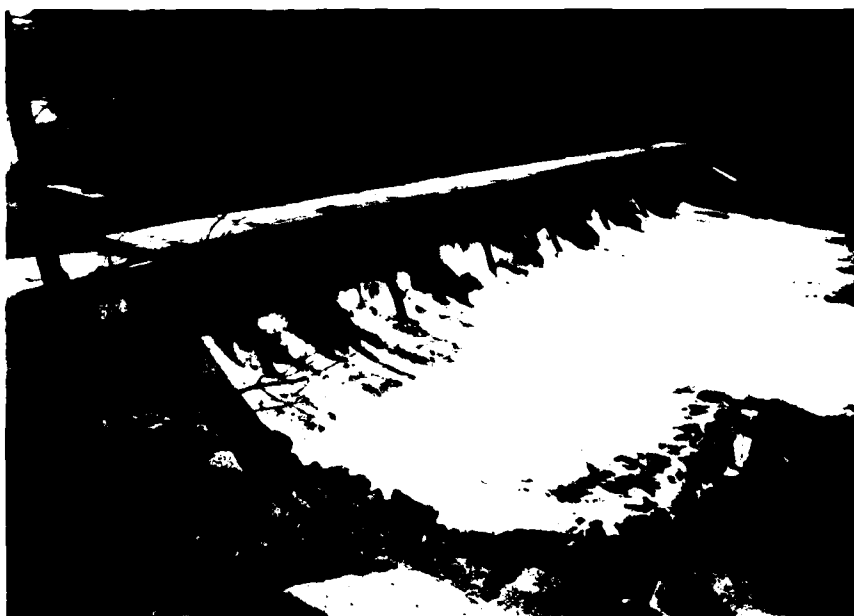


PHOTO #5: Overview of downstream face of dam

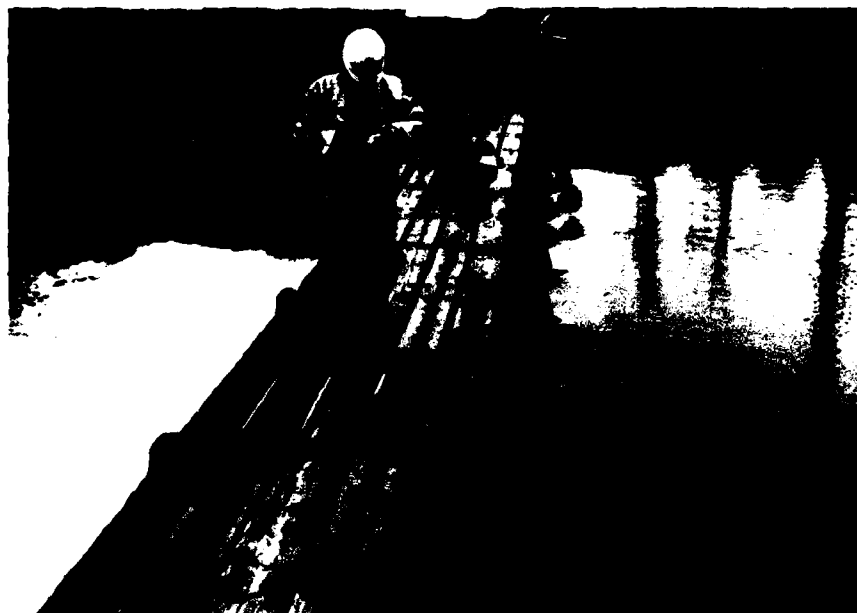


PHOTO #6: Upstream face of dam

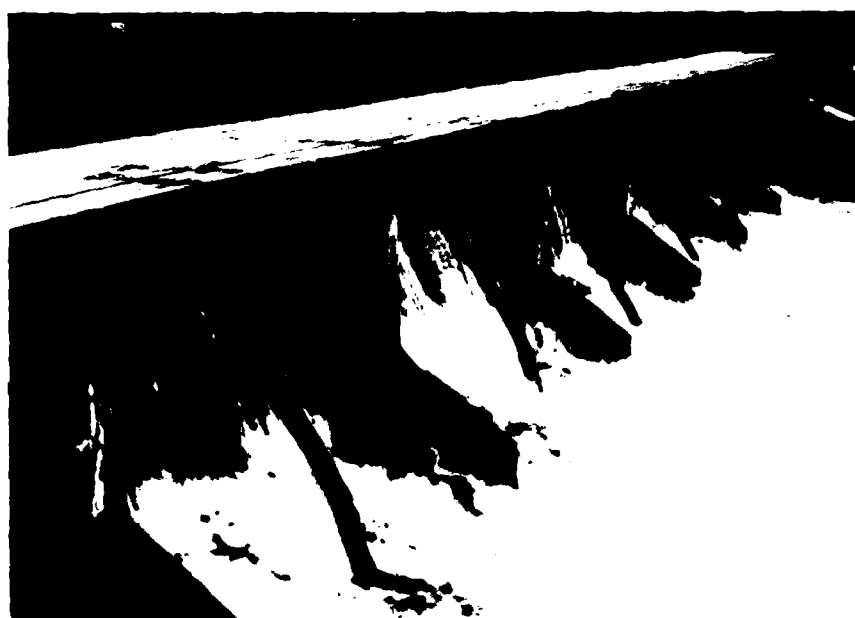


PHOTO #7: Downstream face of dam



PHOTO #8: Stilling basin



PHOTO #9: Downstream channel conditions



PHOTO #10: Buckled web of steel H-beam post
for support of flashboards

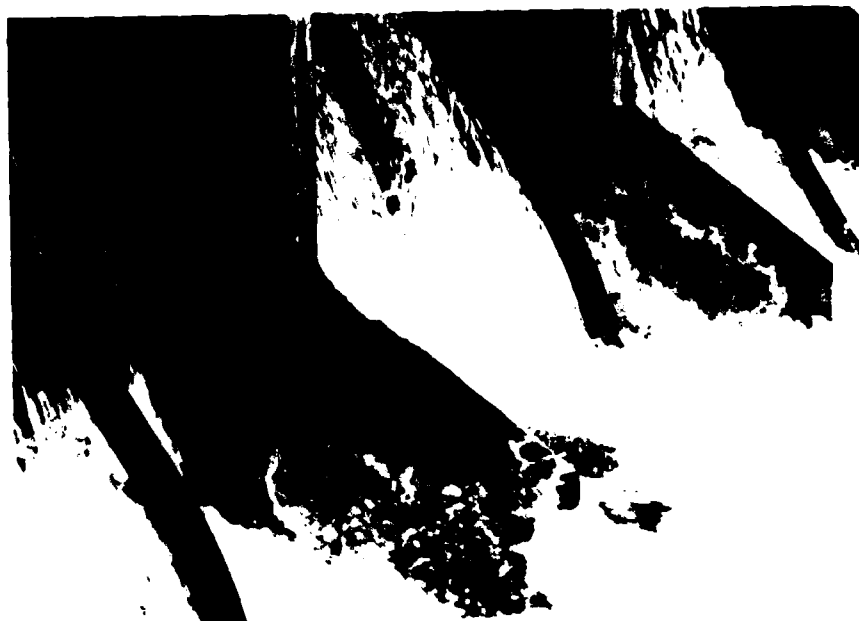


PHOTO #11: Bent steel channel braces for H-beam
post



PHOTO #12: Crack between right concrete abutment
and retaining wall

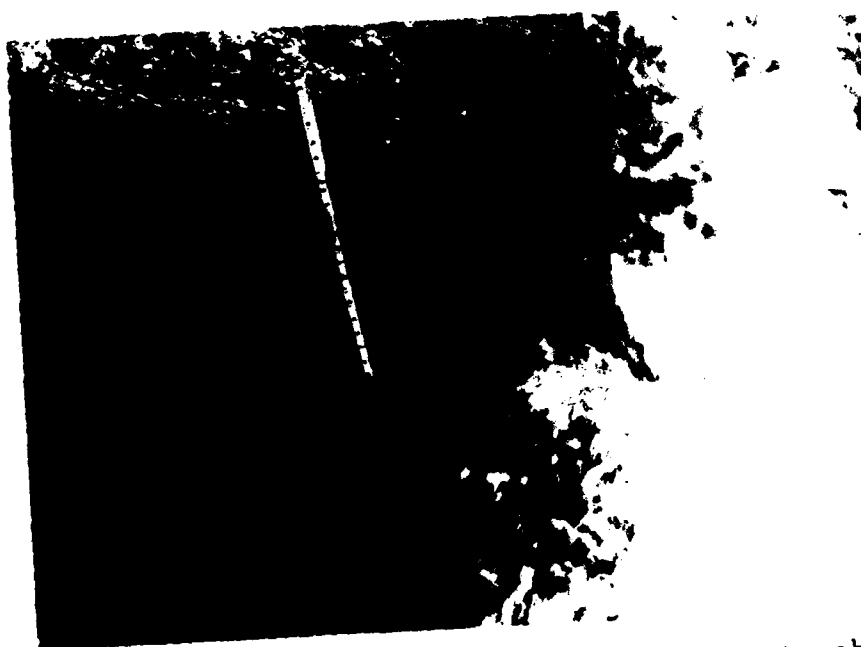


PHOTO #13: Undermining of right concrete abutment



PHOTO #14: Seepage at left concrete abutment



PHOTO #15: Close-up of seepage



PHOTO #16: Right downstream channel side slope



PHOTO #17: Erosion of left downstream channel side slope

APPENDIX B

VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1) Basic Data

a. General

Name of Dam Otsego Lake Dam
Fed. I.D. # NY 361 DEC Dam No. 144A-918
River Basin Susquehanna
Location: Town Otsego and Middlefield County Otsego
Stream Name Susquehanna River
Tributary of Chesapeake Bay
Latitude (N) 42°-41.6' Longitude (W) 74°-55.3'
Type of Dam Concrete buttress
Hazard Category High
Date(s) of Inspection April 9, 1981
Weather Conditions Overcast, 60° ± F.
Reservoir Level at Time of Inspection Elevation 1190.2 ± (NGVD)

b. Inspection Personnel T. L. Ward & R. A. Criscuolo of Flaherty Giavara Associates, P.
J. J. Rixner & C. W. Eller of Haley & Aldrich, Inc.; B. McL. Whittingham of Salmon
Associates

c. Persons Contacted (Including Address & Phone No.)
Mr. Edward M. Gaynor Mr. Carl St. John
Director of Public Works Filtration Plant
Village of Cooperstown Village of Cooperstown Water Works
22 Main Street Mill Street
Cooperstown, New York 13326 Cooperstown, New York 13326
(607) 547-2411

d. History:

Date Constructed Prior to 1910 Date(s) Reconstructed 1955
Designer Unknown
Constructed By Unknown
Owner Village of Cooperstown

2) Embankment

a. Characteristics

- (1) Embankment Material Not applicable
- (2) Cutoff Type None
- (3) Impervious Core None
- (4) Internal Drainage System None observed
- (5) Miscellaneous No comments

b. Crest

- (1) Vertical Alignment Good
- (2) Horizontal Alignment Good
- (3) Surface Cracks None observed
- (4) Miscellaneous No comments

c. Upstream Slope

- (1) Slope (Estimate - V:H) Vertical
- (2) Undesirable Growth or Debris, Animal Burrows Not applicable
- (3) Sloughing, Subsidence or Depressions Not Applicable

(4) Slope Protection Not applicable

(5) Surface Cracks or Movement at Toe None evident

d. Downstream Slope

(1) Slope (Estimate - V:H) Not applicable

(2) Undesirable Growth or Debris, Animal Burrows Not applicable

(3) Sloughing, Subsidence or Depressions Not applicable

(4) Surface Cracks or Movement at Toe None observed

(5) Seepage Minor seepage was noted along the old masonry and concrete wall;
some seepage observed at base of spillway weir

(6) External Drainage System (Ditches, Trenches, Blanket) _____

(7) Condition Around Outlet Structure Concrete apron

(8) Seepage Beyond Toe None evident

e. Abutments - Embankment Contact

Left: good condition

Right: good condition

(1) Erosion at Contact Some surface erosion along wall at overflow
spillway weir

(2) Seepage Along Contact Seepage was noted along the earthen side of the
left abutment wall

3) Drainage System

a. Description of System Broad-crested concrete weir and concrete discharge
apron leading to the natural streambed

b. Condition of System Good

c. Discharge from Drainage System Concrete discharge apron dropping
approximately 5 feet from weir to streambed

4) Instrumentation (Monumentation/Surveys, Observation Wells, Weirs, Piezometers, Etc.)
None observed

5) Reservoir

- a. Slopes Moderate to steep slopes on the left, gentle wooded slopes on the right and lakeside buildings border the impoundment
- b. Sedimentation Possible accumulation of sediment behind the dam
- c. Unusual Conditions Which Affect Dam Usually large watershed and impoundment

6) Area Downstream of Dam

- a. Downstream Hazard (No. of Homes, Highways, etc.) Approximately 2 buildings, two railroad crossings, a sewage treatment plant and three roads are within the dam failure flood hazard area
- b. Seepage, Unusual Growth None observed
- c. Evidence of Movement Beyond Toe of Dam None evident
- d. Condition of Downstream Channel Good; fine to coarse gravel streambed material with some cobbles; no obstructions

7) Spillway(s) (Including Discharge Conveyance Channel)

Overflow spillway and discharge channel

- a. General Overflow spillway and discharge channel handle all flows
- b. Condition of Principal Spillway Good; however, a separation crack has developed between the right concrete abutment and downstream retaining wall; minor undermining of the right concrete abutment and of the slope protection downstream from this wall was evident.

c. Condition of Emergency Spillway Not applicable

d. Condition of Discharge Conveyance Channel Good condition, presently stable

8) Reservoir Drain/Outlet

Type: Pipe None Conduit None Other None

Material: Concrete Metal Other

Size: Length

Invert Elevations: Entrance Exit

Physical Condition (Describe): Unobservable

Material:

Joints: Alignment

Structural Integrity:

Hydraulic Capability:

Means of Control: Gate Valve Uncontrolled

Operation: Operable Inoperable Uncontrolled

Present Condition (Describe):

9) Structural

- a. Concrete Surfaces Concrete of the overflow spillway is in good condition
with only minor spalling
- b. Structural Cracking No evidence of any structural cracks in concrete; however,
some H-beam posts showed evidence of web buckling and some are bent out of
their vertical alignment; channel braces supporting H-beam posts have buckled
- c. Movement - Horizontal & Vertical Alignment (Settlement) Apparently, some
settlement has occurred at the right concrete abutment as evidenced by
the separation crack described in 7) b.
- d. Junctions with Abutments or Embankments Good condition; some seepage was
noted along the earthen side of the left abutment
- e. Drains - Foundation, Joint, Face None evident
- f. Water Passages, Conduits, Sluices Flashboards partially removed between
H-beam posts 2 and 3 from right abutment to form low-flow match
- g. Seepage or Leakage Described in 2) d. (5)

- h. Joints - Construction, etc. Good condition; but slight gap at the right abutment and downstream retaining wall
- i. Foundation Inaccessible
- j. Abutments See 9) d. above
- k. Control Gates None observed
- l. Approach & Outlet Channels Not Applicable
- m. Energy Dissipators (Plunge Pool, etc.) Overflow spillway discharges to concrete apron with circular section
- n. Intake Structures Not applicable
- o. Stability Appears to be stable
- p. Miscellaneous No comments

10) Appurtenant Structures (Power House, Lock, Gatehouse, Other)

a. Description and Condition None observed

[illegible]

APPENDIX C

HYDROLOGIC/HYDRAULIC ENGINEERING DATA AND COMPUTATIONS

CHECK LIST FOR DAMS
HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA

AREA-CAPACITY DATA:

	<u>Elevation</u> (ft.)	<u>Surface Area</u> (acres)	<u>Storage Capacity</u> (acre-ft.)
1) Top of Dam	<u>1194.2</u>	<u>4,272</u>	<u>39,800</u>
2) Design High Water (Max. Design Pool)	<u>--</u>	<u>--</u>	<u>--</u>
3) Emergency Spillway Crest	<u>--</u>	<u>--</u>	<u>--</u>
4) Pool Level with Flashboards	<u>1191.6</u>	<u>4,158</u>	<u>27,440</u>
5) Overflow Spillway Crest	<u>1190.0</u>	<u>4,088</u>	<u>20,440</u>

DISCHARGES: (without flashboards)

	<u>Volume</u> (cfs)
1) Average Daily	<u>Unknown</u>
2) Overflow Spillway @ Maximum High Water (Top of Dam)	<u>1428</u>
3) Emergency Spillway @ Design High Water	<u>--</u>
4) Principal Spillway @ Emergency Spillway Crest	<u>--</u>
5) Low Level Outlet @ Principal Spillway Crest	<u>--</u>
6) Total (of all facilities) @ Maximum High Water	<u>1428</u>
7) Maximum Known Flood	<u>Unknown</u>
8) At Time of Inspection	<u>35 +</u>

CREST:

ELEVATION: 1194.2 (NGVD)

Type Concrete buttress structure

Width 2 feet

Length 69.5 feet

Spillover Concrete overflow spillway weir

Location Center of dam

SPILLWAY:

OVERFLOW		EMERGENCY	
1190.0 (NGVD)	Elevation		
Broad-crested weir	Type		
12 feet	Width		
	Type of Control		
Weir	Uncontrolled		
--	Controlled		
1.6 foot high flashboards	Type:		
	(Flashboards; gate)		
7 sets	Number		
67.5 foot weir/1.6 feet high	Size/Length		
Concrete	Invert Material		
Continuously	Anticipated Length of Operating Service		
Unknown	Chute Length		
3.0 feet	Height Between Spillway Crest & Approach Channel Invert (Weir Flow)		

Type: _____

Location: _____

Records:

Date Unknown

Max. Reading Unknown

FLOOD WATER CONTROL SYSTEM:

Warning System None in effect

Method of Controlled Releases (mechanisms) None

DRAINAGE AREA: 48,000 acres = 75.00 square miles

DRAINAGE BASIN RUNOFF CHARACTERISTICS:

Land Use - Type Agricultural

Terrain - Relief Hilly uplands

Surface - Soil Glacial till

Runoff Potential (existing or planned extensive alterations to existing surface or subsurface conditions)

Primarily agricultural with extensive open fields; glacial till soils;

average watershed slope is $10 \pm$ percent, some residential homes (Cooperstown)

and roadways; some future development around lake possible

Potential Sedimentation problem areas (natural or man-made; present or future)

Possible surface erosion from agricultural fields during fallow periods

Potential Backwater problem areas for levels at maximum storage capacity including surcharge storage:

Flooding of some lakeside buildings is possible

Dikes - Floodwalls (overflow & non-overflow) - Low reaches along the reservoir perimeter:

Location: None observed

Elevation:

Reservoir:

Length @ Maximum Pool 44,400 \pm feet = 8.4 miles (Miles)

Length of Shoreline (@ Spillway Crest) 20.0 miles (Miles)

JORDANVILLE
RICHFIELD SPRINGS

SUBWATER No. 3

CANADARAGO LAKE

Allen Lake

Young Lake





3

RICHFIELD SPRINGS
COOPERSTOWN

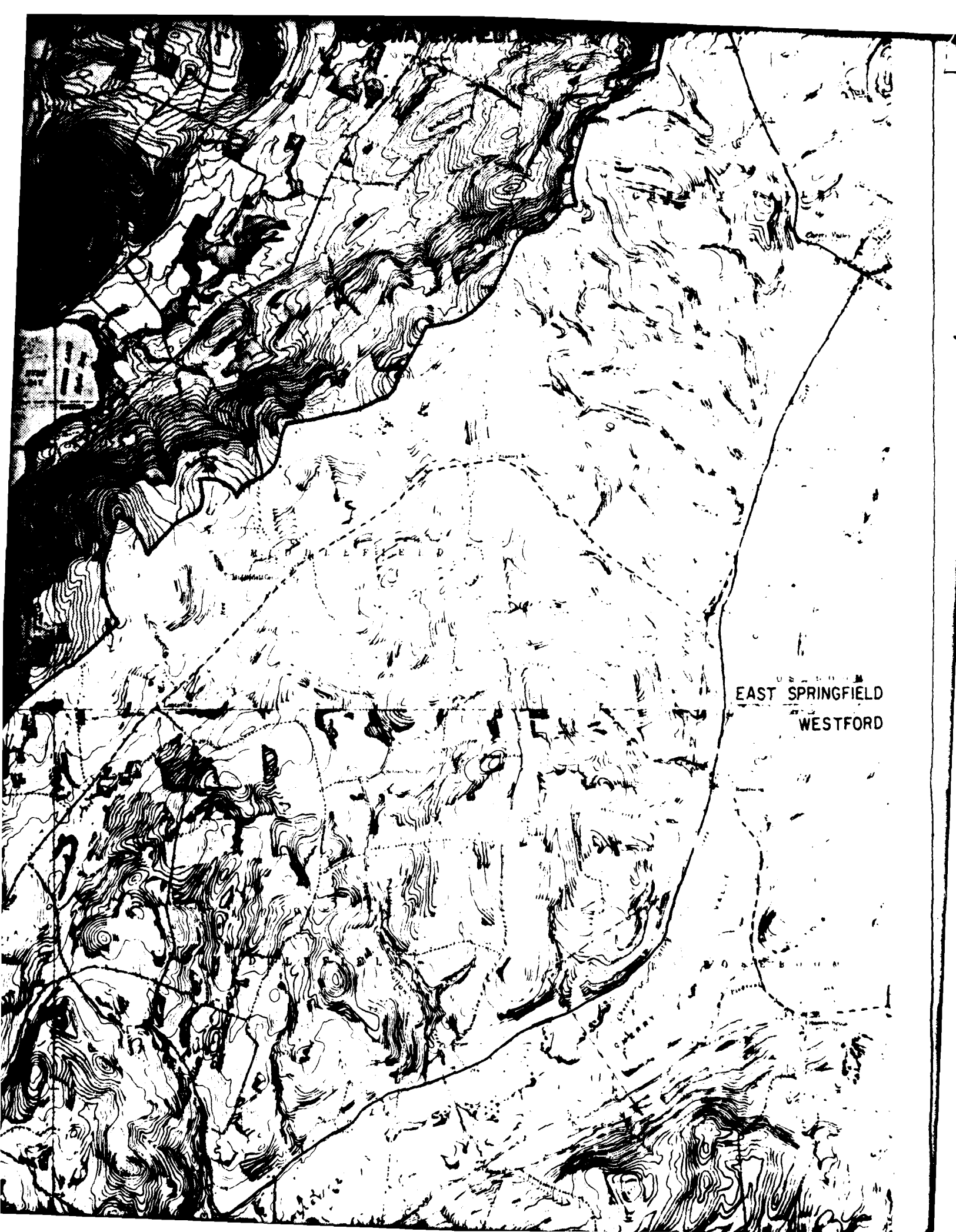
SUBWATERSHED

SUBWATERSHED No. 7

072200

LAKE

INDA





RICHFIELD SPRINGS
COOPERSTOWN

SUBWATERSHED No. 7

BRIDGES



0 4000 8000

SCALE IN FEET

5



EAST SPRINGFIELD
WESTFORD

WATERSHED MAP

OTSEGO LAKE DAM
INVENTORY No. NY 361
SUSQUEHANNA RIVER BASIN
OTSEGO COUNTY
OTSEGO & MIDDLEFIELD, NEW YORK

CALCULATIONS



WATERSHED DATA FOR HEC 1 SNYDER HYDROGRAPH

Sub WATERSHED No. 1

$$T_p = C_t (L L_c)^{0.3}$$

$L = 7.89$ miles

$L_c = 1.97$ miles

$C_t = 2.0$ for average slopes

$$T_p = 2.0 (7.89 \times 1.97)^{0.3} = 4.56 \text{ Hours}$$

$$t_r = \frac{t_p}{5.5} = \frac{4.56}{5.5} = 0.8 \quad \text{USE } t_r = 1.0$$

$$t_{pr} = t_p + 0.25 (t_r - t_p) = 4.56 + 0.25 (1.0 - 0.8) = 4.61 \text{ Hours}$$

SET $C_p = 0.63$ for HIGHLAND AREA

DRAINAGE AREA = 23.84 sq. mi.

% IMPERVIOUS = 1.0%

Sub WATERSHED No. 2

$$T_p = C_t (L L_c)^{0.3}$$

$L = 4.34$ miles

$L_c = 2.17$ miles

$C_t = 2.0$ for average slopes

$$T_p = 2.0 (4.34 \times 2.17)^{0.3} = 3.92 \text{ Hours}$$

$$t_r = \frac{t_p}{5.5} = \frac{3.92}{5.5} = 0.71 \quad \text{USE } t_r = 0.5$$

$$t_{pr} = t_p + 0.25 (t_r - t_p) = 3.92 + 0.25 (0.5 - 0.71) =$$

$$= 3.87 \text{ Hours}$$

PROJECT NY DAMS
NY 361
OTSEGO



FLAHERTY-GIAVARA ASSOCIATES
ENVIRONMENTAL DESIGN CONSULTANTS
ONE COLUMBUS PLAZA, NEW HAVEN, CONN. 06510/203/789-1280

SHEET NO. 2 OF 9
BY RAC DATE 7-28-81
CHK'D BY TLW DATE 7-30-81

SET $C_p = 0.63$ FOR HIGHLAND AREA
DRAINAGE AREA = 13.03 sq. mi.
% IMPERVIOUS = 1.0

SUB WATERSHED NO. 3

$$T_p = C_t (L L_c)^{0.3}$$

$L = 7.89$ miles

$L_c = 4.34$ miles

$C_t = 2.0$ for average slopes

$$T_p = 2.0 (7.89 \times 4.34)^{0.3} = 5.77 \text{ Hours}$$

$$t_r = \frac{T_p}{5.5} = \frac{5.77}{5.5} = 1.05 \quad \text{USE } t_r = 1.0$$

$$t_{pr} = t_p + 0.25(t_r - t_p) = 5.77 + 0.25(1.0 - 1.05) = 5.76 \text{ Hours}$$

SET $C_p = 0.63$ FOR HIGHLAND AREA
DRAINAGE AREA = 17.97 sq. mi.
% IMPERVIOUS = 1.0

SUB WATERSHED NO. 4

$$T_p = C_t (L L_c)^{0.3}$$

$L = 4.34$ miles

$L_c = 2.17$ miles

$C_t = 2.0$

$$T_p = 2.0 (4.34 \times 2.17)^{0.3} = 3.92 \text{ Hours}$$

$$t_r = \frac{T_p}{5.5} = \frac{3.92}{5.5} = 0.71 \quad \text{USE } t_r = 0.5$$

$$t_{pr} = 3.92 + 0.25(0.5 - 0.71) = 3.87 \text{ Hours}$$

SET $C_p = 0.63$ FOR HIGHLAND AREA
DRAINAGE AREA = 4.77 sq. mi.
% IMPERVIOUS = 1.0



Sub WATERSHED No 5

$$T_p = C_t (L L_c)^{0.3}$$

$$L = 2.98 \text{ miles}$$

$$L_c = 1.38 \text{ miles}$$

$$C_t = 2.0 \text{ for average slopes}$$

$$T_p = 2.0 (2.98 \times 1.38)^{0.3} = 3.06 \text{ Hours}$$

$$t_r = \frac{t_p}{5.5} = \frac{3.06}{5.5} = 0.56 \text{ USE } t_r = 0.5$$

$$t_{PR} = 3.06 + 0.25 (0.5 - 0.56) = 3.05 \text{ Hours}$$

SET $C_p = 0.63$ for HIGHLAND AREA

DRAINAGE AREA = 5.56 sq. mi

% Impervious = 05 %

Sub WATERSHED No. 6

$$T_p = C_t (L L_c)^{0.3}$$

$$L = 3.95 \text{ miles}$$

$$L_c = 0.99 \text{ miles}$$

$$C_t = 2.0 \text{ for average slopes}$$

$$T_p = 2.0 (3.95 \times 0.99)^{0.3} = 3.01 \text{ Hours}$$

$$t_r = \frac{t_p}{5.5} = \frac{3.01}{5.5} = 0.55 \text{ USE } t_r = 0.5$$

$$t_{PR} = t_p + 0.25 (t_r - t_p) = 3.01 + 0.25 (0.5 - 0.55) = 3.00 \text{ Hours}$$

SET $C_p = 0.63$ for HIGHLAND AREA

DRAINAGE AREA = 10.33 sq mi

% Impervious = 2.0

PROJECT NO DAMS
OTSEGO



FLAHERTY-GIAVARA ASSOCIATES
ENVIRONMENTAL DESIGN CONSULTANTS
ONE COLUMBUS PLAZA, NEW HAVEN, CONN. 06510/203/769-1260

SHEET NO. 4 OF 9
BY RAC DATE 7-28-81
CHK'D. BY TLW DATE 7-30-81

SUB WATERSHED NO. 7

SURFACE AREA OF OTSEGO LAKE

SET $T_p = 0$

% IMPERVIOUS = 100

DRAINAGE AREA = 6.38 sq mi

RAINFALL DATA (FROM HYDROMETEOROLOGICAL
REPORT NO. 33)

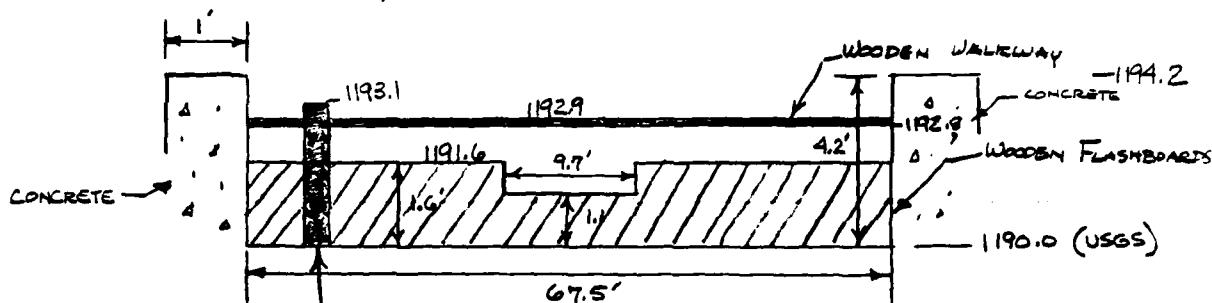
24 HOUR DURATION PMP = 9.3 INCHES
FOR 200 sq miles

<u>DURATION (HRS)</u>	<u>Adj FACTOR (%)</u>
6	86
12	100
24	112
48	119



STAGE DISCHARGE DATA

W/FLASHBOARDS IN PLACE



13 SUPPORTS RANGING FROM 8 TO 11 INCHES
WIDE, SPACED THROUGHOUT THE WEIR SECTION

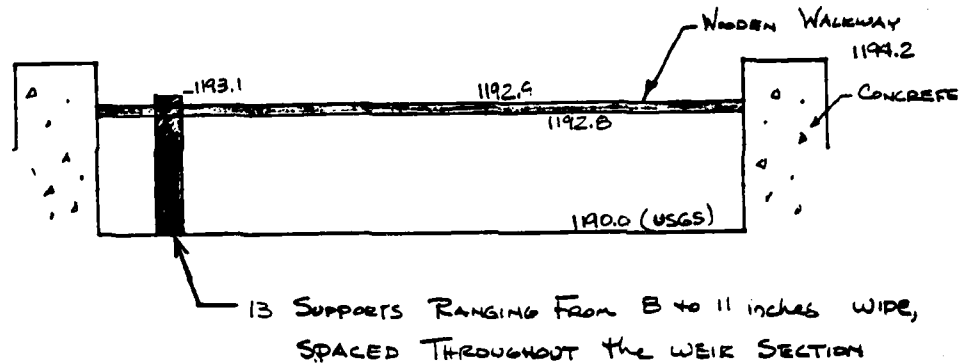
STAGE (FT)	WEIR $Q = 243H^{1.5}$	WEIR $Q = 147.6H^{1.5}$	* ORIFICE $Q = 66.4H^{0.5}$	* ORIFICE $Q = 284.1H^{0.5}$	WEIR $Q = 202.5H^{1.5}$	WEIR $Q = 10.25H^{1.5}$	DISCHARGE (CFS)
1191.1	0						0
1191.6	24.3(.5) ^{1.5}						8.6
1192.0	24.3(.9) ^{1.5}	147.6(.4) ^{1.5}					58.1
1192.2	24.3(1.1) ^{1.5}	147.6(.6) ^{1.5}					96.6
1192.5	24.3(1.4) ^{1.5}	147.6(.9) ^{1.5}					166.3
1192.8	24.3(1.7) ^{1.5}	147.6(1.2) ^{1.5}					247.9
1192.93			66.4(.93) ^{0.5}	284.1(.93) ^{0.5}			306.8
1193.0			66.4(1) ^{0.5}	284.1(1) ^{0.5}	171.75(.07) ^{1.5}		323.7
1193.1			66.4(1.1) ^{0.5}	284.1(1.1) ^{0.5}	171.75(.17) ^{1.5}		351.2
1193.5			66.4(1.5) ^{0.5}	284.1(1.5) ^{0.5}	171.75(.57) ^{1.5}	10.25(.4) ^{1.5}	481.8
1194.0			66.4(2) ^{0.5}	284.1(2) ^{0.5}	171.75(1.07) ^{1.5}	10.25(.9) ^{1.5}	673.9
1194.2			66.4(2.2) ^{0.5}	284.1(2.2) ^{0.5}	171.75(1.27) ^{1.5}	10.25(1.1) ^{1.5}	757.9
1195.0			66.4(3) ^{0.5}	284.1(3) ^{0.5}	171.75(2.07) ^{1.5}	10.25(1.9) ^{1.5}	1128.8
1200.0			66.4(8) ^{0.5}	284.1(8) ^{0.5}	171.75(7.07) ^{1.5}	10.25(6.9) ^{1.5}	4395.7
1208.0			66.4(16) ^{0.5}	284.1(16) ^{0.5}	171.75(15.07) ^{1.5}	10.25(14.9) ^{1.5}	12032.1
1210.0			66.4(18) ^{0.5}	284.1(18) ^{0.5}	171.75(17.07) ^{1.5}	10.25(16.9) ^{1.5}	14305.3

* THE ORIFICE FLOW CONDITION WAS ASSUMED TO EXIST FOR STAGES EQUAL TO THE WALKWAY. FOR STAGES GREATER THAN THE WALKWAY THE SPILLWAY SECTION WAS ANALYZED AS BOTH ORIFICE AND WEIR FLOW CONDITIONS EXISTING.



STAGE DISCHARGE DATA

W/OUT FLASHBOARDS IN PLACE



STAGE	WEIR $Q = 171.75 H^{1.5}$	* ORIFICE $Q = 771.8 H^{2.5}$	WEIR $Q = 10.25 H^{1.5}$	DISCHARGE (CFS)
1190.0	-	-	-	0
1190.5	$171.75 (.5)^{1.5}$	-	-	25.4
1191.0	$171.75 (1)^{1.5}$	-	-	171.8
1191.5	$171.75 (1.5)^{1.5}$	-	-	315.5
1192.0	$171.75 (2)^{1.5}$	-	-	485.0
1192.2	$171.75 (2.2)^{1.5}$	-	-	560.4
1192.5	$171.75 (2.5)^{1.5}$	-	-	678.9
1192.8	-	$771.8 (A)^{2.5}$	-	732.2
1192.93	-	$771.8 (1.03)^{2.5}$	-	783.3
1193.0	$171.75 (1.07)^{1.5}$	$771.8 (1.1)^{2.5}$	-	812.7
1193.1	$171.75 (1.17)^{1.5}$	$771.8 (1.2)^{2.5}$	-	857.5
1193.5	$171.75 (1.57)^{1.5}$	$771.8 (1.6)^{2.5}$	$10.25 (4)^{1.5}$	1052.8
1194.0	$171.75 (1.07)^{1.5}$	$771.8 (2.1)^{2.5}$	$10.25 (9)^{1.5}$	1317.3
1194.2	$171.75 (1.27)^{1.5}$	$771.8 (2.3)^{2.5}$	$10.25 (1.1)^{1.5}$	1428.1
1195.0	$171.75 (2.07)^{1.5}$	$771.8 (3.1)^{2.5}$	$10.25 (1.9)^{1.5}$	1897.2
1200.0	$171.75 (7.07)^{1.5}$	$771.8 (8.1)^{2.5}$	$10.25 (6.9)^{1.5}$	5611.0
1208.0	$171.75 (15.07)^{1.5}$	$771.8 (16.1)^{2.5}$	$10.25 (14.9)^{1.5}$	13734.1

* SEE NOTE ON THE PREVIOUS PAGE

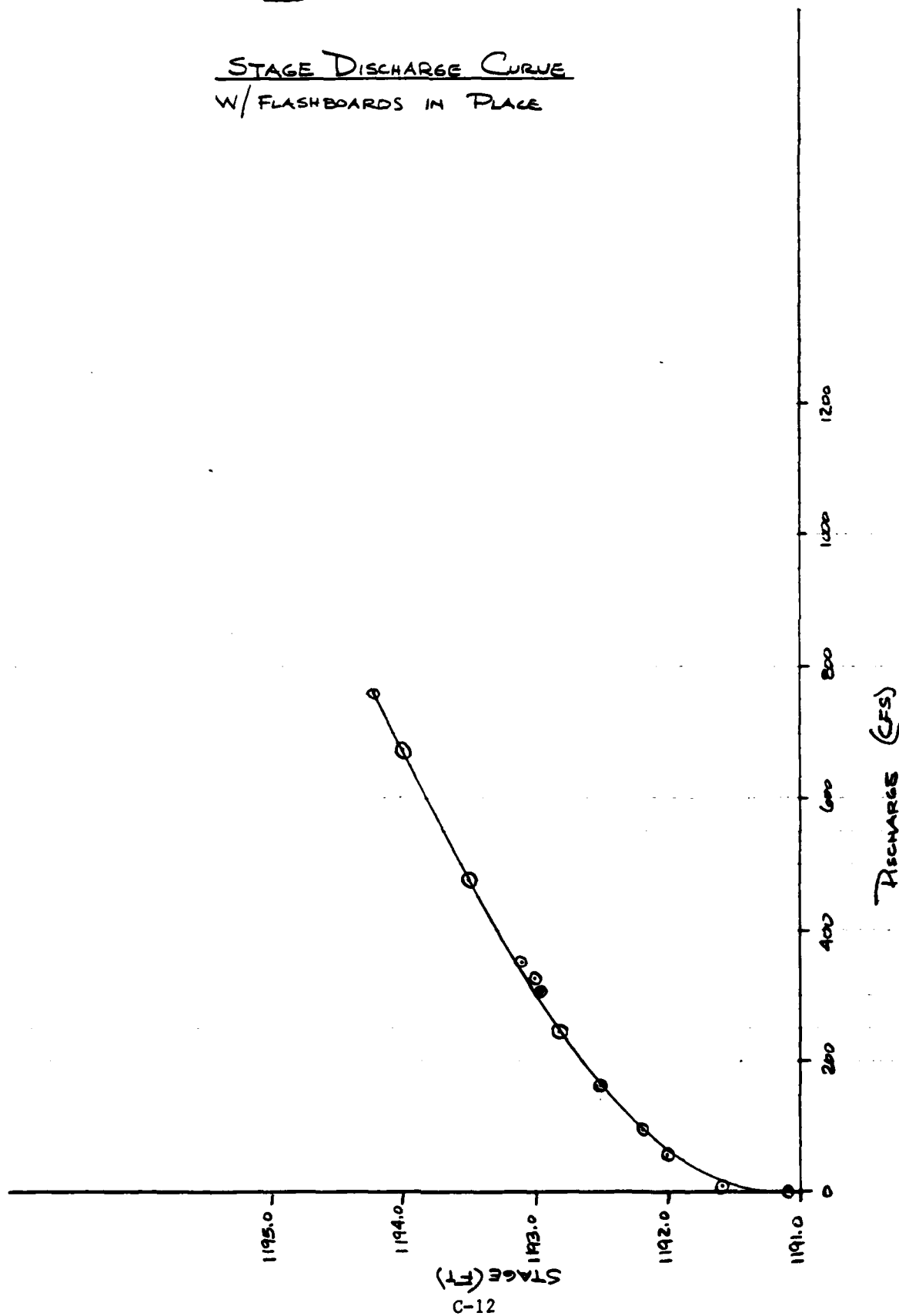
PROJECT CORPS DAMS
OTSEGO



FLAHERTY-GIAVARA ASSOCIATES
ENVIRONMENTAL DESIGN CONSULTANTS
ONE COLUMBUS PLAZA, NEW HAVEN, CONN. 06510/203/780-1280

SHEET NO. 7 OF 9
BY RAC DATE 4-27-81
CHK'D. BY TLW DATE 7-30-81

STAGE DISCHARGE CURVE
W/ FLASHBOARDS IN PLACE



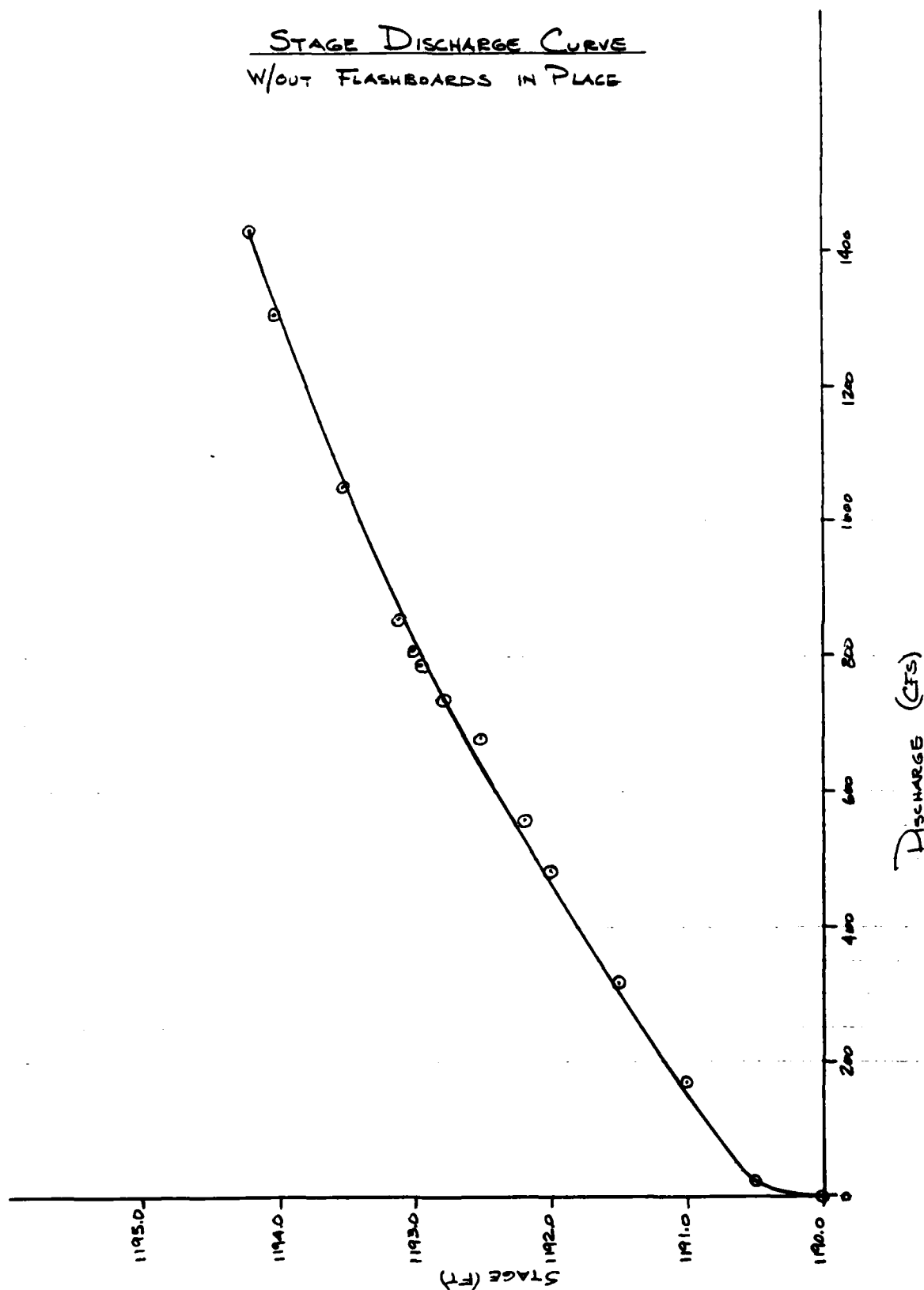
OBJECT CORPS DAMS
DTICGO



FLAHERTY-GIAVARA ASSOCIATES
ENVIRONMENTAL DESIGN CONSULTANTS
ONE COLUMBUS PLAZA, NEW HAVEN, CONN 06510/203/789-1280

SHEET NO. 8 OF 9
BY RAC DATE 4-27-81
CHK'D. BY TLW DATE 7-30-81

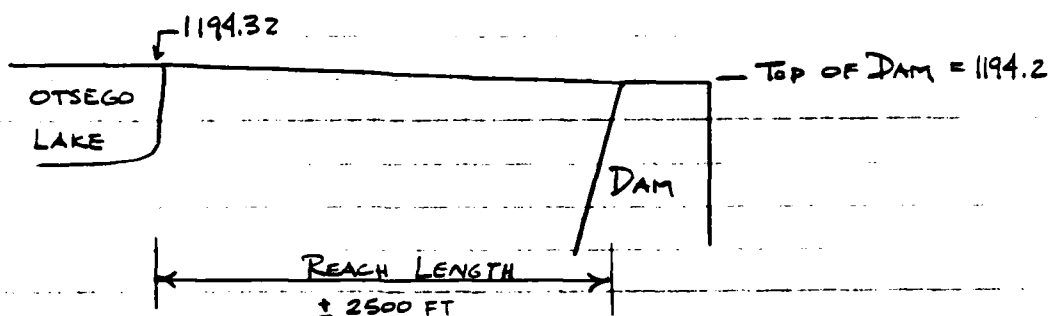
STAGE DISCHARGE CURVE
W/OUT FLASHBOARDS IN PLACE





BACKWATER FROM DAM

RESULTS FROM HEC 2 COMPUTER RUN.



∴ @ Top of Dam (1194.2) additional storage will accumulate in OTSEGO LAKE due to backwater

Top of Dam = 1194.2 $S_A = 4272$
 @ 1220 $S_A = 5402$

$$\frac{1220 - 1194.2}{5402 - 4272} = \frac{1194.32 - 1194.2}{x}$$

$$x = 4272 + 5.3 = 4277.3 \text{ AC}$$

$$\Delta \text{STOR} = \frac{4277.3 + 4272}{2} (0.12) = 513 \text{ AC-FT}$$

@ 1194.2 STOR = 39,300 AC-FT

@ 1194.32 " = 39,813 AC-FT SAY 39,800 AC-FT

∴ STOR @ 1194.2 = 39,800 AC-FT
 DUE TO BACKWATER

BACKWATER ANALYSIS

PAGE 0001

```
*****
** WATER SURFACE PROFILES **
** VERSION OF NOVEMBER 1976 **
** UPDATED APRIL 1980 **
**
** RUN DATE 08/24/81 TIME 10:45:35 **
*****
```

* U.S. ARMY CORPS OF ENGI
* THE HYDROLOGIC ENGINEER
* 609 SECOND STREET, SUIT
* DAVIS, CALIFORNIA 95616
* (916) 440-2105 (FTS) 448-21

08/24/81 10:43:40

PAGE 1

THIS RUN EXECUTED 08/24/81 10:45:41

REC2 RELEASE DATED NOV 76 UP DATED SEPT 1980
EXPERIMENTAL MODS FOR ICE ANALYSIS
ERROR CORR - 01.02,03,04
MODIFICATION - 50.51,52,53,54,99,4.

TT1 NATIONAL DAM INSPECTION PROGRAM, PHASE I REPORT, CORPS OF ENGINEERS, NEW YORK - DISTRICT
 T2 BACKWATER BY DAM INVENTORY NO. NY 361, OTSEGO LAKE DAM, OTSEGO COUNTY, NEW YORK, AUGUST
 T3 PREPARED BY FLANNERY GIOVARRA ASSOCIATES, P.C., ONE COLUMBUS PLAZA, NEW HAVEN, CONNECTICUT

J1	ICHECK	ING	INIV	IDIR	STRT	METRIC	WVINS	G	WSEL	FG
J2	NRDP	IFLOT	PRFVS	XSECV	XSECH	FN	ALLDC	ISW	CHNIM	ITRACE
	-1.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
NC	0.060	0.060	0.040	0.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	1.000	8.000	188.000	362.000	0.000	0.000	0.000	0.000	0.000	0.000
GR	1200.000	0.000	1200.000	50.000	188.000	1190.000	0.000	1184.000	200.000	1184.000
CR	1190.000	362.000	1200.000	400.000	650.000	1220.000	0.000	0.000	0.000	0.000
NC	0.060	0.060	0.040	0.000	0.000	0.000	0.000	0.000	0.000	0.000
X1	2.000	8.000	65.000	185.000	1000.000	1000.000	1000.000	0.000	0.000	0.000
GR	1200.000	0.000	1200.000	50.000	1190.000	0.000	65.000	75.000	1184.400	175.000
CR	1190.000	185.000	1200.000	275.000	1220.000	425.000	0.000	0.000	0.000	0.000

PAGE 0002

[illegible]

08/24/81 10:43:40

PAGE 2

SECNO	DEPTH	CHSEL	CR1WB	WBSELK	EQ	HW	HL	CL08B	BANK ELEV
0	GLOB	GCH	GROB	ALOB	ACH	AROB	VDL	TWA	LEFT/RIGHT
TIME	VLOB	VCH	VROB	XNL	XCH	XNR	WTN	ELNIN	SSTA
SLOPE	XLOBL	XLCH	XLOBR	I1TRAL	IDC	ICONT	CORAR	TOPWID	ENDST

***PROF !**

[illegible]

*SECNO	2.000	9.82	1194.22	0.00	0.00	1194.25	0.02	0.04	0.00	1190.00
2.00	4	4	1399	25	13	1123	80	35	5	1190.00
1428	0.28	1.25	0.31	0.00	0.00	0.040	0.040	0.00	1194.50	58.44
0.23	1000	1000	1000	1000	0.00	0.00	0.00	0.00	1194.50	58.44
0.000059	1000	1000	1000	1000	0.00	0.00	0.00	0.00	1194.50	58.44

*SECNO	3	000	9	48	1174.28	0.00	0.00	1174.31	0.02	0.06	0.00	1170.00
1428	12	1389	27	37	1085	0.00	0.00	0.00	82	63	9	1190.00
0.45	0.32	1.28	0.33	0.06	0.040	0.00	0.00	0.00	0.060	0.00	1184.80	122.71
0.000065	1000	1000	1000	1	0.00	0.00	0.00	0.00	0.00	0.00	175.54	298.45

*SECNO	4	0000	9	32	1194	32	0	00	0	00	1194	34	0	02	0	03	0	00	1190	00
	4	00	57	1314	57	1314	177	1068	177	1068	1194	34	177	177	11	78	11	1190	00	
	0	57	0	123	0	123	0	040	0	040	0	040	0	060	0	000	1185	00	828	09
	0	00004	500	500	500	500	500	500	500	500	500	500	500	0	0	0	283	89	141	25

08/24/81 10:45:40

PAGE 3

THIS RUN EXECUTED 08/24/81 10:45:57

 HEC2 RELEASE DATED NOV 76 UPDATED SEPT 1980
 EXPERIMENTAL MODS FOR ICE ANALYSIS
 ERROR CORR - 01.02.03.04
 MODIFICATION - 50.51.52.53.54.55. 4,

NOTE- ASTERISK (*) AT LEFT OF CROSS-SECTION NUMBER INDICATES MESSAGE IN SUMMARY OF ERRORS LIST

OTSEGO COUNTY, NEW YORK

SUMMARY PRINTOUT TABLE 150

SE	Q	XL	EL D	EL	EL N	Q	CW L	CR S	E	10 S	V	AR
1.000	0.00	0.00	0.00	0.00	1184.00	1428.00	1194.20	0.00	1194.21	0.24	0.82	1838.02
2.000	1000.00	0.00	0.00	0.00	1184.40	1428.00	1194.22	0.00	1194.23	0.39	1.23	1214.33
3.000	1000.00	0.00	0.00	0.00	1184.80	1428.00	1194.28	0.00	1194.31	0.63	1.28	1803.37
4.000	300.00	0.00	0.00	0.00	1183.00	1428.00	1194.32	0.00	1194.34	0.61	1.23	1420.77

08/24/81 10:45:40

PAGE 4

OTSEGO COUNTY, NEW YORK

SUMMARY PRINTOUT TABLE 150

SE	Q	Q	CW L	EL D	EL	EL N	Q	IF S	IF X	IF S	CP D	XL
1.000	1428.00	1194.20	1194.20	0.00	0.00	0.00	0.00	0.00	0.00	0.00	247.72	0.00
2.000	1428.00	1194.22	1194.22	0.00	0.00	0.02	0.00	0.00	0.00	0.00	164.33	1000.00
3.000	1428.00	1194.28	1194.28	0.00	0.00	0.06	0.00	0.00	0.00	0.00	173.34	1000.00
4.000	1428.00	1194.32	1194.32	0.00	0.00	0.03	0.00	0.00	0.00	0.00	283.87	500.00

08/24/81 10:45:40

PAGE 5

SUMMARY OF ERRORS

08/24/81 10:46:02

PAGE 1

THIS RUN EXECUTED 08/24/81 10:46:03

 HEC2 RELEASE DATED NOV 76 UPDATED SEPT 1980
 EXPERIMENTAL MODS FOR ICE ANALYSIS
 ERROR CORR - 01.02.03.04
 MODIFICATION - 30.31.32.33.34.37.4.

HEC-1 FLOOD HYDROGRAPH COMPUTATIONS
(WITH FLASHBOARDS IN PLACE)

FLAHERTY GIAVARA ASSOCIATES, P. C.
FLOOD HYDROGRAPH PACKAGE (HFC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 26 FEB 79

A1 NATIONAL DAM INSPECTION PROGRAM, PHASE I REPORT, CORPS OF ENGINEERS - NEW YORK DISTRICT
A2 DAM INVENTORY NO. NY 361, OTSEGO LAKE DAM (WITH FLASHBOARDS), CHERANOD COUNTY, NEW YORK, APRIL 27, 1981
A3 PREPARED BY FLAHERTY GIAVARA ASSOCIATES, P. C., ONE COLUMBUS PLAZA, NEW HAVEN, CONNECTICUT 06510

1	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
2	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
3	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
4	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
5	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
6	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
7	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
8	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
9	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
10	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
11	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
12	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
13	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
14	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
15	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
16	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
17	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
18	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
19	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
20	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
21	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
22	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
23	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
24	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
25	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
26	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
27	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
28	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
29	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
30	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
31	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
32	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
33	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
34	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
35	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
36	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
37	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
38	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
39	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
40	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
41	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
42	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
43	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
44	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
45	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
46	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
47	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
48	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
49	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
50	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
51	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	
52	1	0.20	0.27	0.28	0.27	0.30	0.30	1.00	

[illegible]

ANALYSIS OF SEQUENCE OF STREAM NETWORK CALCULATIONS

[illegible]

FLOOD HYDROGRAPH PACKAGE (HEC-1)

***** JULY 1978 *****
***** DAM SAFETY VERSION *****
***** LAST MODIFICATION 26 FEB 79 *****

RUN DATE: 8/22/
TIME: 8:23 AM

NATIONAL DAM INSPECTION PROGRAM, PHASE I REPORT, CORPS OF ENGINEERS - NEW YORK DISTRICT
DAM INVENTORY NO. NY 361, DTSEGD LAKE DAM (WITH FLASHBOARDS), CENANGO COUNTY, NEW YORK, APRIL 27, 1981

PREPARED BY FIAHERTY GIAVARA ASSOCIATES, P. C., ONE COLUMBUS PLAZA, NEW HAVEN, CONNECTICUT

NG	NMR	NMIN	IDAY	IHR	IMIN	METRC	IPLT	IPRT	INSTAN
120	0	30	0	0	0	0	2	0	0
		JOPER		NMT	LROPT	TRACE			
		7		0	0	0			

MULTI-PLAN ANALYSES TO BE PERFORMED

MULTI-PLAN ANALYSIS TO BE PERFORMED									
PLAN		NPLAN		NPLAN		NPLAN		NPLAN	
PLAN	NPLAN	PLAN	NPLAN	PLAN	NPLAN	PLAN	NPLAN	PLAN	NPLAN
0.20	0.25	0.26	0.27	0.28	0.29	0.30	0.30	0.30	1.00

市市市市市市市市市市

新華書店經售

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH -	SUBWATERBUSHED NO.					JPRPT	IRNAME	ISTAGE	IAUTH
	1					7			8
	ICOMP	ISECON				6			0
	1STAG					0			0

INTD9	IUN9	TAREA	SNAF	TRSDA	TRSPC	RATIO	IBNDW	IBANE	LOCAL
			0000	27.84	0000	0.00	0	1	0

[illegible]

TRSPC COMPUTED BY THE PROGRAM IS 0.827
0.00 14.

LRPCT	STRMR	DLTKR	RTIOL	ERAIN	STAKS	RTIOK	STRTL	CN8TL	ALBMX	RTIMP
0	0.00	0.00	1.00	0.00	0.00	1.00	1.00	0.10	0.00	0.01

UNIT HYDROGRAPH DATA
tp= 4.61 CP=0.63 NTA= 0

APPROXIMATE CLARK COEFFICIENTS FROM
GIVEN SNYDER CP AND TP ARE
STRTG= -2.00 REACTION= 1.50
GACN= -0.10 INTERVAL B
TC=0.22 AND R= 6.29

UNIT HYDROGRAPH 50 END-OF-PERIOD ORIGINATES, LAG=	4.57 HOURS, CR= 0.63	VOL= 1.00
76. 281	567	2167
2020. 1798	1394	684
606. 537	476	204
142. 160	181	61
54. 48	42	18
	38	
	33	
	30	
	49	
	99	
	126	
	142	
	160	
	176	
	192	
	208	
	224	
	240	
	256	
	272	
	288	
	304	
	320	
	336	
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	368	
	384	
	400	
	416	
	432	
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	560	
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	624	
	640	
	656	
	672	
	688	
	704	
	720	
	736	
	752	
	768	
	784	
	800	
	816	
	832	
	848	
	864	
	880	
	896	
	912	
	928	
	944	
	960	
	976	
	992	
	1008	
	1024	
	1040	
	1056	
	1072	
	1088	
	1104	
	1120	
	1136	
	1152	
	1168	
	1184	
	1200	
	1216	
	1232	
	1248	
	1264	
	1280	
	1296	
	1312	
	1328	
	1344	
	1360	
	1376	
	1392	
	1408	
	1424	
	1440	
	1456	
	1472	
	1488	
	1504	
	1520	
	1536	
	1552	
	1568	
	1584	
	1600	
	1616	
	1632	
	1648	
	1664	
	1680	
	1696	
	1712	
	1728	
	1744	
	1760	
	1776	
	1792	
	1808	
	1824	
	1840	
	1856	
	1872	
	1888	
	1904	
	1920	
	1936	
	1952	
	1968	
	1984	
	2000	
	2016	
	2032	
	2048	
	2064	
	2080	
	2096	
	2112	
	2128	
	2144	
	2160	
	2176	
	2192	
	2208	
	2224	
	2240	
	2256	
	2272	
	2288	
	2304	
	2320	
	2336	

[illegible]

C-21

PAGE 0006

FLAHERTY GIAVARA ASSOCIATES, P.C.

22 00 44
22 00 45
22 00 46
22 00 47
22 00 48
22 00 49
22 00 50
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22 00 101

00102
330103
440104
550105
660106
770107
880108
990109
100110
110111
120112
130113
140114
150115
160116
170117
180118
190119
200120

•END•

C-24

HYDROGRAPH AT STA 111 FOR PLAN 5, RTIO 111

[illegible]

	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL	VOLUME
CFB	50.4	4282	1522	77	9542	9542
CMB	143	121	55	23	208	208
INCHES		1.67	3.01	3.1	3.11	
MM		42.44	76.58	78.94	78.94	
CU FT		3831	3851	3473	3552	
THOUS CU M		2619	4726	4875	4875	

HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 2

[illegible]

FLAHERTY CIAVARA ASSOCIATES, P. C.

HYDROGRAPH AT STA 11 FOR PLAN 1, RTIO 5											
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1

HYDROGRAPH AT STA 11 FOR PLAN 1, RTIO 5											
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1

HYDROGRAPH AT STA 11 FOR PLAN 1, RTIO 5											
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1

HYDROGRAPH AT STA 11 FOR PLAN 1, RTIO 5											
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1

HYDROGRAPH AT STA 11 FOR PLAN 1, RTIO 5											
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
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12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1
12	11	10	9	8	7	6	5	4	3	2	1

	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL	VOLUME
CFS	15034.	12274.	5236.	2166.	25903.	7360.
CMB	426.	348.	148.	61.		15.
INCHES		8.76	14.95	15.46		46.
MM		222.97	379.80	392.74		392.74
AC-FT		6086.	10386.	10740.		10740.
THOUS CU M		7507.	12811.	13247.		13247.

NOTE

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

6

2000.

INFLOW (I),
4000. 4000.

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(0)MO

2. **REMOVED**

#1 MDT
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14000.

6000.

o.

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PRECIP(L) AND EXCESS(X)

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	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL
CFS	3909	3191	1311	563	67573
CMS	111	70	39	16	1913
INCHES		2.28	3.89	4.02	4.02
MM		97.87	98.75	102.11	102.11
AC-FT	1582	2700	2700	2792	2792
				3444	3444

	324.	311.	297.	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL	VOLUME
CF8				4037	3314	1414	589	70174	
CH8				115	94	40	17	1787	
INCHES					2.37	4.04	4.17		4.1
AC-FY				60.04	102.35	106.04	106.0		106.0
				2604	3459	3577	3577		3577

HYDROGRAPH AT STA 1 FOR PLAN 1. RTIO B

	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL VOLUME
CFB	7917	6137	2819	1083	12951
CMS	213	174	51	31	360
INCHES		4.38	7.48	7.73	7.73
MM		111.28	189.90	196.37	196.37
AC-FT		3043	5193	9370	9370
TURNING FU M		3734	5403	6624	6624

	1194.	1108.	1064.	1024.	784.
CFS	PEAK	15034.	5236.	2166.	TOTAL VOLUME
CMS	12274.	12274.	14755.	15816.	259902.
INCHES	426.	346.	176.	15.	7360.
MM	222.57	379.60	10386.	392.74	1548.
AC-FT	5086.	10881.	13247.	10740.	392.74
					10740.
					13247.

```
*****  
*****  
*****  
COMBINE HYDROGRAPHS  
*****  
*****  
COMBINE 2 INFLOW HYDROGRAPHS  
IBTAG 1 ICOMP 2 IECON 0 ITAPE 0 JPLT 0 JPRT 0 INAME 1 ISTAGE 1 IAUTO 0  
SUM OF 2 HYDROGRAPHS AT 1 PLAN 1 RTIO 1  
14. 13. 12.  
9. 7. 6.  
7. 6. 6.  
10. 7. 6.
```

•DVF•

STATION	INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(S)	1000	2000	3000	4000	5000	6000	7000	8000	9000	10000
1											
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71											

18 00 361
17 00 371
16 00 381
15 00 391
14 00 401
13 00 411
12 00 421
11 00 431
10 00 441
09 00 451
08 00 461
07 00 471
06 00 481
05 00 491
04 00 501
03 00 511
02 00 521
01 00 531
00 00 541
00 00 551
00 00 561
00 00 571
00 00 581
00 00 591
00 00 601
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00 00 881
00 00 891
00 00 901
00 00 911
00 00 921
00 00 931

AD-A109 795

FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT F/G 13/13
NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)
JUL 81 H C FLAHERTY DACW51-81-C-0006

F/G 13/13

INVENTORY NUMBER
DACW51-81-C-0006

NL

UNCLASSIFIED

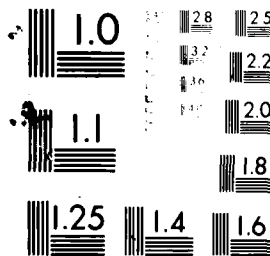
27

Appendix

2 OF 7

AD-

A109795



MICROCOPY RESOLUTION TEST CHART
NBS 1010-A

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23 30 95
00 00 96
00 30 97
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1 30 99
1 00 100
2 00 101
2 30 102
3 00 103
3 30 104
4 00 105
4 30 106
5 00 107
5 30 108
6 00 109
6 30 110
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7 30 112
8 00 113
8 30 114
9 00 115
10 00 116
10 30 117
11 00 118
11 30 119
12 00 120

C-38

OVN

18	17	SUM OF 2 HYDROGRAPHS AT	1	PLAN 1	RTID 2	13	13	13
12	12	14	13	13	14	13	13	13
9	11	11	10	10	10	9	9	9
8	8	8	8	8	7	7	7	7
10	14	23	43	35	6	6	6	6
11	133	170	274	385	486	78	78	78
111	990	1081	1397	1663	2024	395	395	395
4792	3890	7009	9002	9657	9772	2488	2488	2488
8304	7520	6748	5347	4790	4281	7788	7788	7788
2730	2430	2137	1487	1487	1330	3828	3828	3828
933	896	820	1793	1793	1731	1204	1204	1204
						1071	1071	1071
						671	671	671

PEAK
9772
283

CFS
CMS
INCHES
AC-FT
THOUS CU M

6-HOUR
6414
3733
103
374
93 44
7389
9109

72-HOUR
1538
44
3 88
98 54
7423
9403

TOTAL VOLUME
184528
5225
3 88
98 54
7423
9403

OVF

STATION 1

PAGE 0022

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

[illegible]

57. 30 00 58. 30 00 59. 30 00 60. 30 00 61. 30 00 62. 30 00 63. 30 00 64. 30 00 65. 30 00 66. 30 00 67. 30 00 68. 30 00 69. 30 00 70. 30 00 71. 30 00 72. 30 00 73. 30 00 74. 30 00 75. 30 00 76. 30 00 77. 30 00 78. 30 00 79. 30 00 80. 30 00 81. 30 00 82. 30 00 83. 30 00 84. 30 00 85. 30 00 86. 30 00 87. 30 00 88. 30 00 89. 30 00 90. 30 00 91. 30 00 92. 30 00 93. 30 00 94. 30 00 95. 30 00 96. 30 00 97. 30 00 98. 30 00 99. 30 00 00. 30 00 01. 30 00 02. 30 00 03. 30 00 04. 30 00 05. 30 00 06. 30 00 07. 30 00 08. 30 00 09. 30 00 10. 30 00 11. 30 00 12. 30 00 13. 30 00 14. 30 00

9.30119
10.00116
11.00117
12.00118
13.00119
14.00120

DVN

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RTIO 3	
17	18	17	18	17	18
17	18	17	18	17	18
12	13	10	11	10	11
8	9	8	9	8	9
7	8	7	8	7	8
24	25	24	25	24	25
177	178	177	178	177	178
1124	1125	1124	1125	1124	1125
7290	7291	7290	7291	7290	7291
7018	7019	7018	7019	7018	7019
2243	2244	2243	2244	2243	2244
894	895	894	895	894	895
931	932	931	932	931	932
970	971	970	971	970	971

PEAK		6-HOUR		24-HOUR		72-HOUR		TOTAL VOLUME	
CFS	CMH	CFS	CMH	CFS	CMH	CFS	CMH	CFS	CMH
10392	294	9730	270	3872	110	1599	45	191909	5434
249	7	249	7	110	3	43	1	5434	154
INCHES	MM	INCHES	MM	INCHES	MM	INCHES	MM	INCHES	MM
AC-FT	CU M	AC-FT	CU M	AC-FT	CU M	AC-FT	CU M	AC-FT	CU M
THOUS	CU M	THOUS	CU M	THOUS	CU M	THOUS	CU M	THOUS	CU M

DVF

STATION 1

INFLW(1), OUTFLOW(1) AND OBSERVED FLOW(1)

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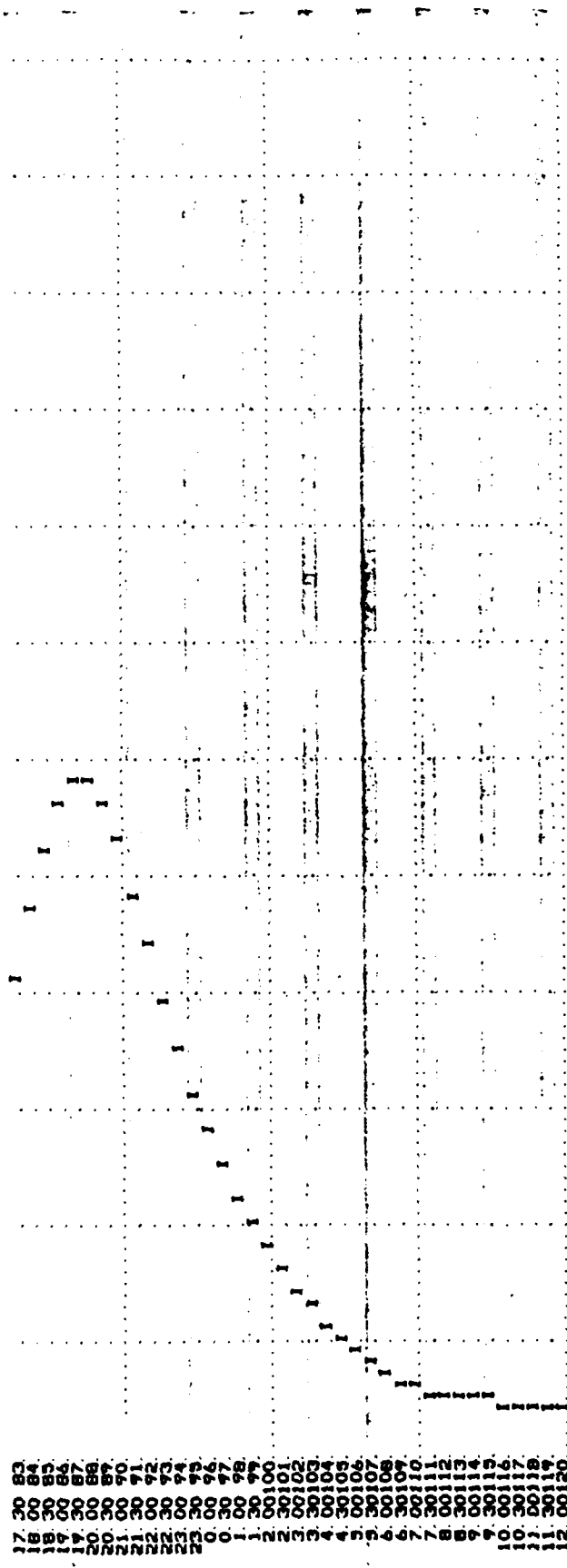
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SUM OF 2 HYDROGRAPHS AT		1	PLAN 1	RTIO 4	
13	18	16	14	13	14
14	17	11	11	10	10
15	12	11	10	10	10
16	9	10	10	11	11
17	9	10	10	11	11
18	9	10	10	11	11
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82	9	10	10	11	11
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111	9	10	10	11	11
112	9	10	10	11	11
113	9	10	10	11	11
114	9	10	10	11	11
115	9	10	10	11	11
116	9	10	10	11	11
117	9	10	10	11	11
118	9	10	10	11	11
119	9	10	10	11	11
120	9	10	10	11	11

12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82



OWN

	21	20	SUM OF 2 HYDROGRAPHS AT	1	FLAN 1	RTIO 7	16	15
17	14	14	19	17	17	16	16	15
18	10	10	13	12	12	11	11	11
19	9	9	10	10	10	9	9	9
20	12	11	10	12	12	12	12	12
21	13	17	39	66	80	74	107	118
22	132	140	249	462	583	713	845	971
23	108	1187	1491	1776	2429	2986	3666	4374
24	974	7048	9697	11588	11991	11586	10863	10863
25	2274	7028	7227	3748	5137	4594	4108	3671
26	1117	1075	2292	1784	1597	1447	1314	1195
27			791	914	878	843	809	777
28			1032					

CFS
 CFS
 INCHES
 AC-FT
 THOUS CU M

PEAK
 11991
 340

6-HOUR
 10096
 284
 2.75
 64.70
 5006
 6175

24-HOUR
 4468
 127
 4.51
 114.32
 8862
 10930

72-HOUR
 1843
 52
 4.66
 118.25
 9159
 11287

TOTAL VOLUME
 221434
 6270
 4.66
 118.25
 9159
 11287

OVF

STATION 1

INFLW(1), OUTFLOW(0) AND OBSERVED FLOW(0)

0 11
 1 12
 2 13
 3 14
 4 15
 5 16
 6 17
 7 18
 8 19
 9 20
 10 21
 11 22
 12 23
 13 24
 14 25
 15 26
 16 27
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 18 29
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 21 32
 22 33
 23 34
 24 35
 25 36
 26 37
 27 38
 28 39
 29 40
 30 41
 31 42
 32 43
 33 44
 34 45

FLAHERTY CIAVARA ASSOCIATES, P. C.

23 00 461
23 30 471
0 30 481
1 30 491
1 30 501
1 30 511
2 30 521
3 30 531
3 30 541
4 30 551
4 30 561
5 30 571
5 30 581
6 30 591
6 30 601
6 30 611
7 30 621
7 30 631
8 30 641
8 30 651
9 30 661
9 30 671
10 30 681
10 30 691
11 30 701
11 30 711
12 30 721
12 30 731
13 30 741
13 30 751
14 30 761
14 30 771
15 30 781
15 30 791
16 30 801
16 30 811
17 30 821
17 30 831
18 30 841
18 30 851
19 30 861
19 30 871
20 30 881
20 30 891
21 30 901
21 30 911
22 30 921
22 30 931
23 30 941
23 30 951
0 30 961
0 30 971
1 30 981
1 30 991
2 30 1001
2 30 1011
3 30 1021
3 30 1031

FLAHERTY GIAVARA ASSOCIATES, P. C.

4 00104
4 30105
5 00106
5 30107
6 00108
6 30109
7 00110
7 30111
8 00112
8 30113
9 00114
9 30115
10 00116
10 30117
11 00118
11 30119
12 00120

OVN

SUM OF 2 HYDROGRAPHS AT

34
23
17
16
19
31
266
1979
11780
15040
4860
1791

33
22
16
18
18
46
340
2161
14089
13495
4314
1720

30
21
14
18
15
84
294
274
1803
1023
3373
1586

27
19
21
15
12
157
1189
4976
1979
7656
2412
1404

26
19
21
12
178
1407
611
17310
2847
2170
1349

23
18
11
21
205
194
1619
7233
19103
9119
9991
1295

PEAK
19789
566
CFS
CHS
INCHES
MM
AC-FT
THOUS CU M

6-HOUR
1687
47
425
107.84
18346
10292

24-HOUR
7446
211
190.87
14769
18217

72-HOUR
3075
87
7.76
197.09
15230
18811

TOTAL VOLUME
369036
18450
7.76
197.09
15230
18811

OVF

STATION 1

INFLW(1), OUTFLOW(1) AND OBSERVED FLOW(1)

0 1
0 30
1 200
2 200
3 200
4 200
5 200
6 200
7 200
8 200

2000

4000

6000

8000

10000

12000

14000

16000

18000

20000

22000

24000

26000

28000

30000

FLAHERTY GIAVARA ASSOCIATES, P. C.

9 30 67
10 30 68
11 30 69
12 30 70
13 30 71
14 30 72
15 30 73
16 30 74
17 30 75
18 30 76
19 30 77
20 30 78
21 30 79
22 30 80
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37 30 95
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41 30 99
42 30 100
43 30 101
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47 30 105
48 30 106
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51 30 109
52 30 110
53 30 111
54 30 112
55 30 113
56 30 114
57 30 115
58 30 116
59 30 117
60 30 118
61 30 119
62 30 120

•DYN•

20 00 88
20 00 89
20 00 90
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20 00 99
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20 00 114
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20 00 117
20 00 118
20 00 119
20 00 120

END

***** SUB-AREA RUNOFF COMPUTATION *****

INFLOW HYDROGRAPH - SUBWATERSED NO. 3
ISTAG 1 ICORP 0 ITAPE 0 JPLT 0 JPR7 0 INAME 1 ISTAGE 0 IAU0 0

HYDRO 1 IUA0 1 TAREA 17.47 SNAP 0.00 TRSDA 17.47 TRSPC 0.00 RATIO 0.000 ISNOW 0 ISAME 1 LOCAL 0

PRECIP DATA
R12 R24
100.00 112.00 119.00

LOSS DATA
R6 R72 R76
86.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.819

LRPT	0	STRK	0.00	DLTK	0.00	RTOL	1.00	ERIN	0.00	STNS	0.00	RTOM	1.00	STRL	1.00	CHSTL	0.10	ALSN	0.00	RTMP	0.01
										UNIT HYDROGRAPH DATA											
										TP= 5.76											
										CP=0.63											
										NTA= 0											

RECESSION DATA
RTIOR= 1.30
EA AND R=10.42 INTERVALS
ORCSN= -0.10
SRTQ= -2.00
COEFFICIENTS FROM
GIVEN SAVED CP AND TP ARE
-7C=12

UNIT	HYDROGRAPH	63	END-OF-PERIOD	ORDINATES,	LAGS	5.72	HOURS,	CPT	0.63	VEL	1.00
32	118	10	382	136	999	864	10.32	1782	1.39	132	12
118	1273	110	1170	1799	948	864	10.32	1782	1.39	132	12
1273	1260	100	1100	1799	948	864	10.32	1782	1.39	132	12
1260	1252	100	1090	1799	948	864	10.32	1782	1.39	132	12
1252	1244	100	1080	1799	948	864	10.32	1782	1.39	132	12
1244	1237	100	1070	1799	948	864	10.32	1782	1.39	132	12
1237	1230	100	1060	1799	948	864	10.32	1782	1.39	132	12
1230	1223	100	1050	1799	948	864	10.32	1782	1.39	132	12
1223	1216	100	1040	1799	948	864	10.32	1782	1.39	132	12
1216	1209	100	1030	1799	948	864	10.32	1782	1.39	132	12
1209	1202	100	1020	1799	948	864	10.32	1782	1.39	132	12
1202	1195	100	1010	1799	948	864	10.32	1782	1.39	132	12
1195	1188	100	1000	1799	948	864	10.32	1782	1.39	132	12
1188	1181	100	990	1799	948	864	10.32	1782	1.39	132	12
1181	1174	100	980	1799	948	864	10.32	1782	1.39	132	12
1174	1167	100	970	1799	948	864	10.32	1782	1.39	132	12
1167	1160	100	960	1799	948	864	10.32	1782	1.39	132	12
1160	1153	100	950	1799	948	864	10.32	1782	1.39	132	12
1153	1146	100	940	1799	948	864	10.32	1782	1.39	132	12
1146	1139	100	930	1799	948	864	10.32	1782	1.39	132	12
1139	1132	100	920	1799	948	864	10.32	1782	1.39	132	12
1132	1125	100	910	1799	948	864	10.32	1782	1.39	132	12
1125	1118	100	900	1799	948	864	10.32	1782	1.39	132	12
1118	1111	100	890	1799	948	864	10.32	1782	1.39	132	12
1111	1104	100	880	1799	948	864	10.32	1782	1.39	132	12
1104	1097	100	870	1799	948	864	10.32	1782	1.39	132	12
1097	1090	100	860	1799	948	864	10.32	1782	1.39	132	12
1090	1083	100	850	1799	948	864	10.32	1782	1.39	132	12
1083	1076	100	840	1799	948	864	10.32	1782	1.39	132	12
1076	1069	100	830	1799	948	864	10.32	1782	1.39	132	12
1069	1062	100	820	1799	948	864	10.32	1782	1.39	132	12
1062	1055	100	810	1799	948	864	10.32	1782	1.39	132	12
1055	1048	100	800	1799	948	864	10.32	1782			

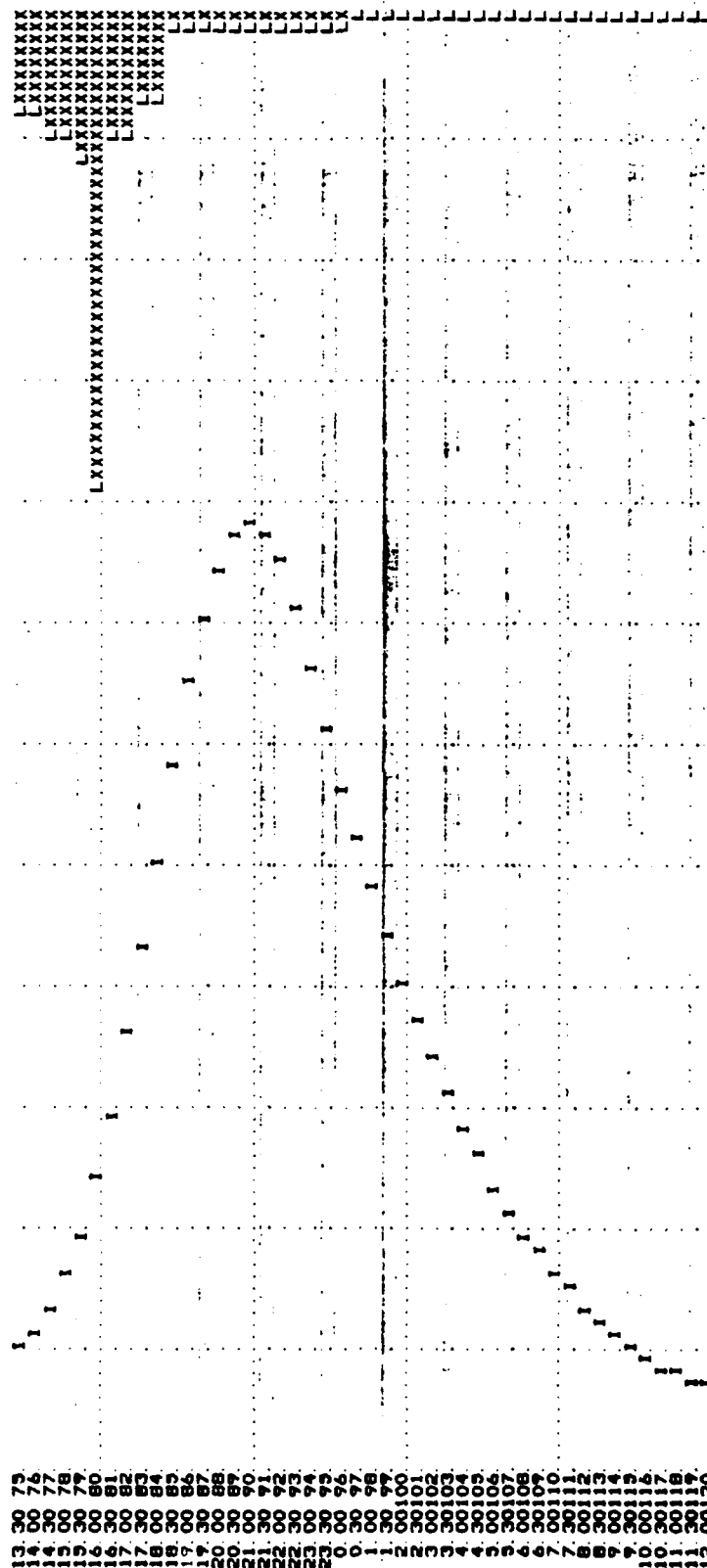
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18.81 19.33 3.47 334014.5

M V3 5000
 THRU 01 M
 AC-FT
 1-34
 MM
 500001
 5000
 5000

*** END ***

[illegible]



13.00 75
14.00 76
15.00 77
16.00 78
17.00 79
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57.00 119
58.00 120

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OVN

AC-FT
THOUS CU M1771
21843501
43183587
44253587
4425

9
6
4
4
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3
4
40
335
1311
1378
1936
4024
1979
1813
1712
784

9
8
6
4
4
4
4
4
39
401
324
2324
3818
1639
1517
388

HYDROGRAPH AT STA

8

1 FOR PLAN 1, RTIO 4

7
5
4
4
4
3
25
227
1038
4143
2354
931
395

6
4
4
4
4
3
25
227
1038
4143
2354
931
395

CFS
CFS
INCHES
AC-FT
THOUS CU M

PEAK
4192
119
3708
105
197
50.16
1839
2268

6-HOUR
1833
52
390
77.16
3636
4484

72-HOUR
751
21
4.00
101.61
3723
4595

TOTAL VOLUME

90152

2223

4.00

101.61

3723

4595

AC-FT
THOUS CU M

7
6
4
4
4
3
4
41
323
1437
4308
2052
813

7
6
4
4
4
3
4
41
323
1437
4308
2052
813

HYDROGRAPH AT STA

8

1 FOR PLAN 1, RTIO 5

7
5
4
4
4
3
26
231
1076
4277
2441
986
410

7
5
4
4
4
3
26
231
1076
4277
2441
986
410

CFS
CFS
INCHES
AC-FT
THOUS CU M

PEAK
4347
123
3844
109
203
52.01
1507
2352

6-HOUR
1901
54
408
102.83
3770
4631

72-HOUR
779
22
4.19
105.37
3863
4765

TOTAL VOLUME

93491

2647

4.19

105.37

3863

4765

7
6
4
4
4
3
4
41
323
1437
4308
2052
813

7
6
4
4
4
3
4
41
323
1437
4308
2052
813

HYDROGRAPH AT STA

8

1 FOR PLAN 1, RTIO 6

7
5
4
4
4
3
26
231
1076
4277
2441
986
410

7
5
4
4
4
3
26
231
1076
4277
2441
986
410

CFS
CFS
INCHES
AC-FT
THOUS CU M

PEAK
4347
123
3844
109
203
52.01
1507
2352

6-HOUR
1901
54
408
102.83
3770
4631

72-HOUR
779
22
4.19
105.37
3863
4765

TOTAL VOLUME

93491

2647

4.19

105.37

3863

4765

PAGE 0050

FLAHERTY GIAVARA ASSOCIATES, P. C.

THOUS CU M	4200	8305	8309
24	2397	2397	2397
23	2397	2397	2397
22	2397	2397	2397
21	2397	2397	2397
20	2397	2397	2397
19	2397	2397	2397
18	2397	2397	2397
17	2397	2397	2397
16	2397	2397	2397
15	2397	2397	2397
14	2397	2397	2397
13	2397	2397	2397
12	2397	2397	2397
11	2397	2397	2397
10	2397	2397	2397
9	2397	2397	2397
8	2397	2397	2397
7	2397	2397	2397
6	2397	2397	2397
5	2397	2397	2397
4	2397	2397	2397
3	2397	2397	2397
2	2397	2397	2397
1	2397	2397	2397
0	2397	2397	2397

THOUS CU M	6-HOUR	24-HOUR	72-HOUR	TOTAL VOLUME
24	15226	13735	2782	33895
23	15226	13735	2782	33895
22	15226	13735	2782	33895
21	15226	13735	2782	33895
20	15226	13735	2782	33895
19	15226	13735	2782	33895
18	15226	13735	2782	33895
17	15226	13735	2782	33895
16	15226	13735	2782	33895
15	15226	13735	2782	33895
14	15226	13735	2782	33895
13	15226	13735	2782	33895
12	15226	13735	2782	33895
11	15226	13735	2782	33895
10	15226	13735	2782	33895
9	15226	13735	2782	33895
8	15226	13735	2782	33895
7	15226	13735	2782	33895
6	15226	13735	2782	33895
5	15226	13735	2782	33895
4	15226	13735	2782	33895
3	15226	13735	2782	33895
2	15226	13735	2782	33895
1	15226	13735	2782	33895
0	15226	13735	2782	33895

DVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(S)
4000 5000 6000

1000 2000 3000 4000 5000 6000 7000 8000 9000 10000 11000 0

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52
0 1 2 3 3 3 3 4 4 5 5 6 6 7 7 8 8 9 9 10 10 11 11 12 12 13 13 14 14 15 15 16 16 17 17 18 18 19 19 20 20 21 21 22 22 23 23 24 24 25 25 26 26 27 27 28 28 29 29 30 30 31 31 32 32 33 33 34 34 35 35 36 36 37 37 38 38 39 39 40 40 41 41 42 42 43 43 44 44 45 45 46 46 47 47 48 48 49 49 50 50 51 51 52 52

7 30111
8 30112
9 30113
10 30114
11 30115
12 30116
13 30117
14 30118
15 30119
16 30120

OVN

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RTIO 2	
24	25	21	22	20	19
18	17	15	14	14	13
13	12	11	10	11	11
11	11	11	10	11	11
14	14	11	10	11	11
15	14	10	10	11	11
17	17	10	10	11	11
117	177	10	10	11	11
1193	1318	10	10	11	11
6233	7382	10	10	11	11
12150	11247	10	10	11	11
4562	4108	10	10	11	11
1659	1355	10	10	11	11

6-70

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RTIO 2	
24	25	21	22	20	19
18	17	15	14	14	13
13	12	11	10	11	11
11	11	11	10	11	11
14	14	11	10	11	11
15	14	10	10	11	11
17	17	10	10	11	11
117	177	10	10	11	11
1193	1318	10	10	11	11
6233	7382	10	10	11	11
12150	11247	10	10	11	11
4562	4108	10	10	11	11
1659	1355	10	10	11	11

OVF

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RTIO 2	
24	25	21	22	20	19
18	17	15	14	14	13
13	12	11	10	11	11
11	11	11	10	11	11
14	14	11	10	11	11
15	14	10	10	11	11
17	17	10	10	11	11
117	177	10	10	11	11
1193	1318	10	10	11	11
6233	7382	10	10	11	11
12150	11247	10	10	11	11
4562	4108	10	10	11	11
1659	1355	10	10	11	11

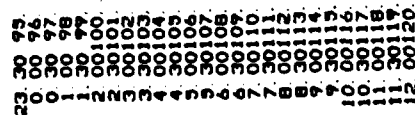
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13 11
14 11
15 11

PAGE 0034

FLAHERTY GIAVARA ASSOCIATES, P. C.

00 161
00 171
00 181
00 191
00 201
00 211
00 221
00 231
00 241
00 251
00 261
00 271
00 281
00 291
00 301
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00 471
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00 721
00 731

18 371
 19 368
 20 360
 21 350
 22 340
 23 330
 24 320
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 26 300
 27 290
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 30 260
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 41 150
 42 140
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 44 120
 45 110
 46 100
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 49 70
 50 60
 51 50
 52 40
 53 30
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 81 0
 82 0
 83 0
 84 0
 85 0
 86 0
 87 0
 88 0
 89 0
 90 0
 91 0
 92 0
 93 0
 94 0



#DYN#

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RHO 4		TOTAL		VOLUME	
		1	2	1	2	1	2	1	2
27	171	23	23	21	21	21	21	21	21
28	171	12	12	13	13	13	13	13	13
29	171	12	12	13	13	13	13	13	13
30	171	12	12	13	13	13	13	13	13
31	171	12	12	13	13	13	13	13	13
32	171	12	12	13	13	13	13	13	13
33	171	12	12	13	13	13	13	13	13
34	171	12	12	13	13	13	13	13	13
35	171	12	12	13	13	13	13	13	13
36	171	12	12	13	13	13	13	13	13
37	171	12	12	13	13	13	13	13	13
38	171	12	12	13	13	13	13	13	13
39	171	12	12	13	13	13	13	13	13
40	171	12	12	13	13	13	13	13	13
41	171	12	12	13	13	13	13	13	13
42	171	12	12	13	13	13	13	13	13
43	171	12	12	13	13	13	13	13	13
44	171	12	12	13	13	13	13	13	13
45	171	12	12	13	13	13	13	13	13
46	171	12	12	13	13	13	13	13	13
47	171	12	12	13	13	13	13	13	13
48	171	12	12	13	13	13	13	13	13
49	171	12	12	13	13	13	13	13	13
50	171	12	12	13	13	13	13	13	13
51	171	12	12	13	13	13	13	13	13
52	171	12	12	13	13	13	13	13	13
53	171	12	12	13	13	13	13	13	13
54	171	12	12	13	13	13	13	13	13
55	171	12	12	13	13	13	13	13	13
56	171	12	12	13	13	13	13	13	13
57	171	12	12	13	13	13	13	13	13
58	171	12	12	13	13	13	13	13	13
59	171	12	12	13	13	13	13	13	13
60	171	12	12	13	13	13	13	13	13
61	171	12	12	13	13	13	13	13	13
62	171	12	12	13	13	13	13	13	13
63	171	12	12	13	13	13	13	13	13
64	171	12	12	13	13	13	13	13	13
65	171	12	12	13	13	13	13	13	13
66	171	12	12	13	13	13	13	13	13
67	171	12	12	13	13	13	13	13	13
68	171	12	12	13	13	13	13	13	13
69	171	12	12	13	13	13	13	13	13
70	171	12	12	13	13	13	13	13	13
71	171	12	12	13	13	13	13	13	13

◆ END ◆

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

PAGE 0039

C-76

55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 00 01 02 03 04 05 06 07 08 09 10 11 12 13 14 15

44-2

10 00116
11 00117
12 00118
13 00119
14 00120

OVN

SUM OF 2 HYDROGRAPHS AT		PLAN 1		RTIO 5	
27	28	29	30	31	32
18	19	17	18	17	18
13	14	13	14	13	14
14	15	14	15	14	15
33	34	32	33	32	33
232	233	231	232	231	232
1826	1827	1824	1825	1824	1825
10260	10261	10258	10259	10258	10259
11516	11517	11514	11515	11514	11515
4137	4138	4134	4135	4134	4135
1634	1635	1631	1632	1631	1632
PEAK	PEAK	PEAK	PEAK	PEAK	PEAK
15342	15343	15339	15340	15339	15340
434	435	432	433	432	433
CFB	CFB	CFB	CFB	CFB	CFB
CMH	CMH	CMH	CMH	CMH	CMH
INCHES	INCHES	INCHES	INCHES	INCHES	INCHES
AC-FT	AC-FT	AC-FT	AC-FT	AC-FT	AC-FT
THOUS CU H	THOUS CU H	THOUS CU H	THOUS CU H	THOUS CU H	THOUS CU H
29	30	29	30	29	30
1337	1338	1334	1335	1334	1335
17004	17005	16999	17000	16999	17000
13608	13609	13604	13605	13604	13605
5109	5110	5105	5106	5105	5106
1858	1859	1854	1855	1854	1855

OVF

STATION 1		INFLW(1); OUTFLW(1) AND OBSERVED FLOW(1)		14000		16000		0		0		0		0	
2000	4000	6000	8000	10000	12000	14000	16000	0	0	0	0	0	0	0	0
0 11	1 11	2 11	3 11	4 11	5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11
20 11	30 11	40 11	50 11	60 11	70 11	80 11	90 11	100 11	110 11	120 11	130 11	140 11	150 11	160 11	170 11
1 11	2 11	3 11	4 11	5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11
2 11	3 11	4 11	5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11
3 11	4 11	5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11
4 11	5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11
5 11	6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11
6 11	7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11
7 11	8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11
8 11	9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11
9 11	10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11
10 11	11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11
11 11	12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11
12 11	13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11
13 11	14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11
14 11	15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11
15 11	16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11
16 11	17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11	31 11
17 11	18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11	31 11	32 11
18 11	19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11	31 11	32 11	33 11
19 11	20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11	31 11	32 11	33 11	34 11
20 11	21 11	22 11	23 11	24 11	25 11	26 11	27 11	28 11	29 11	30 11	31 11	32 11	33 11	34 11	35 11

FLAHERTY GIOVARA ASSOCIATES, P. C.

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54 00 118
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OVN

29	30	SUM OF 2 HYDROGRAPHS AT	PLAN 1	PLAN 2
14	21	27	27	27
15	15	18	15	15
16	12	13	12	12
17	13	14	13	13
18	16	14	16	16
19	24	48	24	24
20	203	341	203	203
21	1529	1891	1529	1529
22	6912	12302	6912	6912
23				
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14094	13047	11928	10818	9781	8833	7973	7198	6500	5867
5292	4766	4284	3845	3444	3081	2779	2523	2291	2082
1924	1804	1693	1589	1493	1404	1321	1256	1206	1159

PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL VOLUME
15890	13611	6283	2591	310882
450	385	178	73	8803
	2.33	4.30	4.43	4.43
INCHES				
	59.18	107.27	112.65	112.65
AC-FT	6749	12462	12846	12846
THOUS CU M	8323	15371	15846	15846

OVF

STATION 1

INFLW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

4000. 6000. 8000. 10000. 12000. 14000. 16000. 0. 0. 0. 0. 0.

0 11 0 30 0 11 0 30 21 10 30 21 11 00 21 11 30 21 12 00 21 12 30 21 13 00 21 13 30 21 14 00 21 14 30 21 15 00 21 15 30 21 16 00 21 16 30 21 17 00 21 17 30 21 18 00 21 18 30 21 19 00 21 19 30 21 20 00 21 20 30 21



| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 7 | | TOTAL VOLUME | |
|-------------------------|----|--------|----|--------|------|--------------|----|
| 1 | 2 | 1 | 2 | 1 | 2 | 1 | 2 |
| 31 | 27 | 24 | 24 | 24 | 24 | 24 | 24 |
| 32 | 18 | 18 | 18 | 18 | 18 | 18 | 18 |
| 33 | 13 | 13 | 13 | 13 | 13 | 13 | 13 |
| 34 | 14 | 14 | 14 | 14 | 14 | 14 | 14 |
| 35 | 15 | 15 | 15 | 15 | 15 | 15 | 15 |
| 36 | 16 | 16 | 16 | 16 | 16 | 16 | 16 |
| 37 | 17 | 17 | 17 | 17 | 17 | 17 | 17 |
| 38 | 18 | 18 | 18 | 18 | 18 | 18 | 18 |
| 39 | 19 | 19 | 19 | 19 | 19 | 19 | 19 |
| 40 | 20 | 20 | 20 | 20 | 20 | 20 | 20 |
| 41 | 21 | 21 | 21 | 21 | 21 | 21 | 21 |
| 42 | 22 | 22 | 22 | 22 | 22 | 22 | 22 |
| 43 | 23 | 23 | 23 | 23 | 23 | 23 | 23 |
| 44 | 24 | 24 | 24 | 24 | 24 | 24 | 24 |
| 45 | 25 | 25 | 25 | 25 | 25 | 25 | 25 |
| 46 | 26 | 26 | 26 | 26 | 26 | 26 | 26 |
| 47 | 27 | 27 | 27 | 27 | 27 | 27 | 27 |
| 48 | 28 | 28 | 28 | 28 | 28 | 28 | 28 |
| 49 | 29 | 29 | 29 | 29 | 29 | 29 | 29 |
| 50 | 30 | 30 | 30 | 30 | 30 | 30 | 30 |
| 51 | 31 | 31 | 31 | 31 | 31 | 31 | 31 |
| 52 | 32 | 32 | 32 | 32 | 32 | 32 | 32 |
| 53 | 33 | 33 | 33 | 33 | 33 | 33 | 33 |
| 54 | 34 | 34 | 34 | 34 | 34 | 34 | 34 |
| 55 | 35 | 35 | 35 | 35 | 35 | 35 | 35 |
| 56 | 36 | 36 | 36 | 36 | 36 | 36 | 36 |
| 57 | 37 | 37 | 37 | 37 | 37 | 37 | 37 |
| 58 | 38 | 38 | 38 | 38 | 38 | 38 | 38 |
| 59 | 39 | 39 | 39 | 39 | 39 | 39 | 39 |
| 60 | 40 | 40 | 40 | 40 | 40 | 40 | 40 |
| 61 | 41 | 41 | 41 | 41 | 41 | 41 | 41 |
| 62 | 42 | 42 | 42 | 42 | 42 | 42 | 42 |
| 63 | 43 | 43 | 43 | 43 | 43 | 43 | 43 |
| 64 | 44 | 44 | 44 | 44 | 44 | 44 | 44 |
| 65 | 45 | 45 | 45 | 45 | 45 | 45 | 45 |
| 66 | 46 | 46 | 46 | 46 | 46 | 46 | 46 |
| 67 | 47 | 47 | 47 | 47 | 47 | 47 | 47 |
| 68 | 48 | 48 | 48 | 48 | 48 | 48 | 48 |
| 69 | 49 | 49 | 49 | 49 | 49 | 49 | 49 |
| 70 | 50 | 50 | 50 | 50 | 50 | 50 | 50 |
| 71 | 51 | 51 | 51 | 51 | 51 | 51 | 51 |
| 72 | 52 | 52 | 52 | 52 | 52 | 52 | 52 |
| 73 | 53 | 53 | 53 | 53 | 53 | 53 | 53 |
| 74 | 54 | 54 | 54 | 54 | 54 | 54 | 54 |
| 75 | 55 | 55 | 55 | 55 | 55 | 55 | 55 |
| 76 | 56 | 56 | 56 | 56 | 56 | 56 | 56 |
| 77 | 57 | 57 | 57 | 57 | 57 | 57 | 57 |
| 78 | 58 | 58 | 58 | 58 | 58 | 58 | 58 |
| 79 | 59 | 59 | 59 | 59 | 59 | 59 | 59 |
| 80 | 60 | 60 | 60 | 60 | 60 | 60 | 60 |
| 81 | 61 | 61 | 61 | 61 | 61 | 61 | 61 |
| 82 | 62 | 62 | 62 | 62 | 62 | 62 | 62 |
| 83 | 63 | 63 | 63 | 63 | 63 | 63 | 63 |
| 84 | 64 | 64 | 64 | 64 | 64 | 64 | 64 |
| 85 | 65 | 65 | 65 | 65 | 65 | 65 | 65 |
| 86 | 66 | 66 | 66 | 66 | 66</ | | |

7 30 63
8 30 64
9 30 65
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13 30 69
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16 30 72
17 30 73
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62 30 118
63 30 119
64 30 120

•DVF•

| | PEAR | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|--------|-------|--------|---------|---------|--------------|
| CFB | 27396 | 23468 | 10832 | 4467 | 536004 |
| CHB | 776 | 649 | 307 | 126 | 15178 |
| INCHES | | 4.02 | 7.42 | 7.65 | |
| MM | | 102.04 | 189.40 | 194.22 | |
| AC-FT | | 121486 | 11637 | 22149 | |
| CU-M | | 14354 | 26302 | 27320 | |
| THOUS | | | | | 27330 |

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(O)

INFLW(I), OUTFLOW(Q) AND OBSERVED FLOW(*)

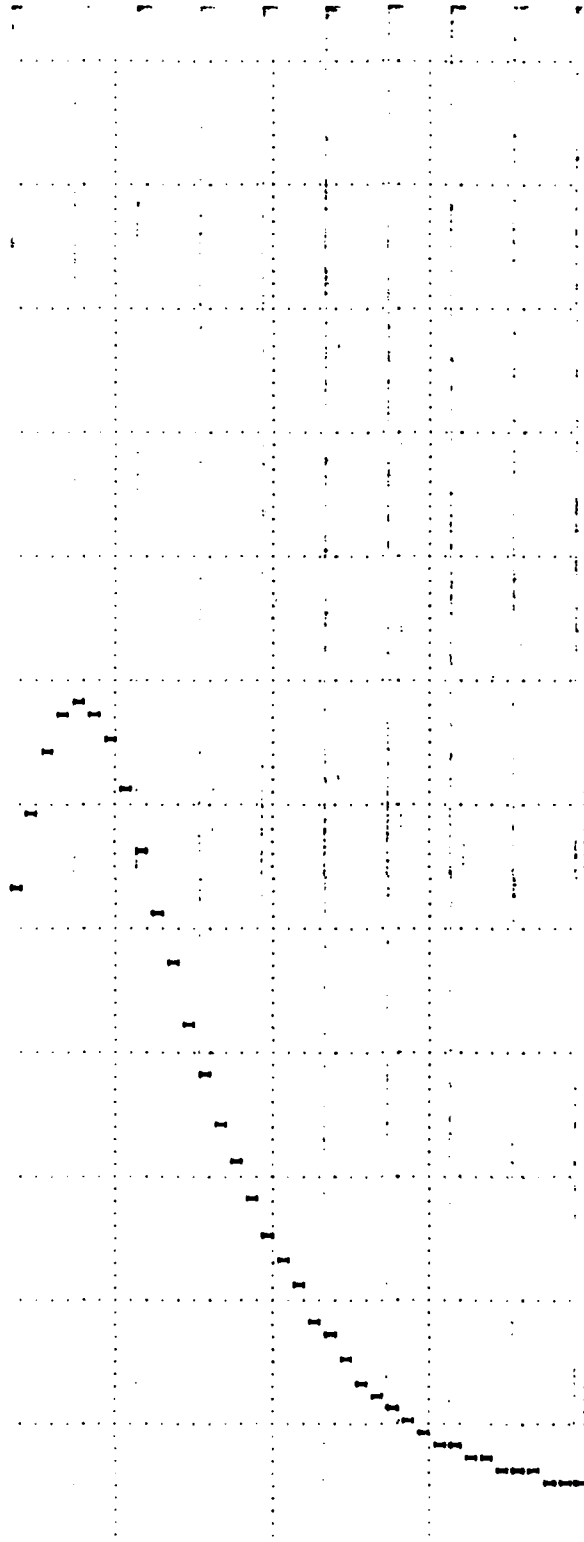
| Time | Inflow (I) | Outflow (Q) | Observed Flow (*) |
|-------|------------|-------------|-------------------|
| 0 | 2000 | 0 | 0 |
| 10000 | 2000 | 2000 | 2000 |
| 28000 | 2000 | 2000 | 2000 |

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FLAHERTY GIOVANA ASSOCIATES, P. C.

261
271
281
291
301
311
321
331
341
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361
371
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421
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681
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701
711
721
731
741
751
761
771
781
791
801
811
821
831
841
851
861
871
881
891
901
911
921
931
941
951
961
971
981
991

18 00 84
19 00 85
19 00 86
19 00 87
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20 01 14
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20 01 17
20 01 18
20 01 19
20 01 20



DVN

| SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 9 | 72 | 74 |
|-------------------------|--------|--------|-------|-------|
| 76 | 89 | 82 | 77 | 74 |
| 66 | 41 | 57 | 55 | 54 |
| 48 | 43 | 43 | 42 | 42 |
| 46 | 51 | 56 | 38 | 38 |
| 42 | 45 | 39 | 37 | 37 |
| 120 | 220 | 344 | 406 | 465 |
| 900 | 1990 | 2509 | 3074 | 3657 |
| 9807 | 8918 | 10772 | 13150 | 16065 |
| 36443 | 91336 | 53993 | 54793 | 53964 |
| 41130 | 30457 | 27494 | 24821 | 22413 |
| 14774 | 11876 | 9581 | 8699 | 7901 |
| 5837 | 5150 | 4557 | 4332 | 4160 |
| 5481 | 14842 | 4557 | 4332 | 4160 |

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME

| 104 | 100 |
|-------|-------|
| 171 | 48 |
| 50 | 47 |
| 43 | 44 |
| 54 | 54 |
| 58 | 83 |
| 588 | 708 |
| 4774 | 5271 |
| 25013 | 30730 |
| 48598 | 44989 |
| 18247 | 16434 |
| 6636 | 6221 |

1072008.
30356.
15.29
388.44
44298.
54641.

8933.
253.
15.29
388.44
44298.
54641.

21663.
613.
14.83
376.81
42971.
53004.

46935.
1329.
8.03
204.08
23274.
28708.

54793.
1552.

CFB
CHB
INCHES
MM
AC-FT
THOUS CU M

DVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

5000. 10000. 15000. 20000. 25000. 30000. 35000. 40000. 45000. 50000. 55000. 0

0.11
1.12
2.13
3.14
4.15
5.16
6.17
7.18
8.19
9.20
10.21
11.22
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32.43
33.44
34.45
35.46

23 00 471
00 481
00 491
1 00 501
2 00 511
2 00 521
3 00 531
3 00 541
4 00 551
5 00 561
5 00 571
5 00 581
5 00 591
6 00 601
7 00 611
7 00 621
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8 00 661
9 00 671
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9 00 691
10 00 701
11 00 711
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11 00 731
11 00 741
11 00 751
11 00 761
11 00 771
11 00 781
11 00 791
11 00 801
11 00 811
11 00 821
11 00 831
11 00 841
11 00 851
11 00 861
11 00 871
11 00 881
11 00 891
11 00 901
11 00 911
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21 30120

OVN

***** SUB-AREA RUNOFF COMPUTATION *****

INFLOW HYDROGRAPH - SUBWATERSHED NO. 4
ISTAG 1 ICOMP 0 IECON 0 ITAPE 0 UPLT 0 UPRY 0 INAME 1 IASTAG 0 IAUTQ 0

HYDROGRAPH DATA
INVDQ 1 IUMQ 1 TAREA 4.77 SNAP 0.00 TRSDA 4.77 TRSPC 0.000 RATIO 0.000 ISNOW 0 ISAME 0 LOCAL 0

PRECIP DATA
SPPE 0.00 PMS 19.30 R6 86.00 100.00 112.00 119.00 R48 R72 R96
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA
LROFT 0 STRKR 0 DLTKR 0 RTIOL 1.00 ERAIN 0.00 STRKS 0.00 RTIOK 1.00 STRTL 1.00 CNSTL 0.10 ALSHX 0.00 RTIMP 0.01

UNIT HYDROGRAPH DATA
TP= 3.87 CP=0.63 NTA= 0

APPROXIMATE CLANK COEFFICIENTS FROM GIVEN BNYDER CP AND TP ARE TC= 8.75 AND R= 7.04 INTERVALS
STRTQ= -2.00 RECESION DATA
GNCBNS= -0.10 RTIOR= 1.50

UNIT HYDROGRAPH 42 END-OF-PERIOD ORDINATES, LAQ= 3.87 HOURS, CP= 0.63 VOL= 1.00
22 384 82 165 289 251 354 435 488 510 494 483
43 334 80 70 61 53 46 40 34 30 128
22 19 17 13 11 10 8 7 6 5

| | 1970 | 1971 | 1972 | 1973 | 1974 | 1975 | 1976 | 1977 | 1978 | 1979 | 1980 | 1981 | 1982 | 1983 | 1984 | 1985 | 1986 | 1987 | 1988 | 1989 | 1990 | 1991 | 1992 | 1993 | 1994 | 1995 | 1996 | 1997 | 1998 | 1999 | 2000 | 2001 | 2002 | 2003 | 2004 | 2005 | 2006 | 2007 | 2008 | 2009 | 2010 | 2011 | 2012 | 2013 | 2014 | 2015 | 2016 | 2017 | 2018 | 2019 | 2020 | 2021 | 2022 | 2023 | 2024 | 2025 | 2026 | 2027 | 2028 | 2029 | 2030 | 2031 | 2032 | 2033 | 2034 | 2035 | 2036 | 2037 | 2038 | 2039 | 2040 | 2041 | 2042 | 2043 | 2044 | 2045 | 2046 | 2047 | 2048 | 2049 | 2050 | 2051 | 2052 | 2053 | 2054 | 2055 | 2056 | 2057 | 2058 | 2059 | 2060 | 2061 | 2062 | 2063 | 2064 | 2065 | 2066 | 2067 | 2068 | 2069 | 2070 | 2071 | 2072 | 2073 | 2074 | 2075 | 2076 | 2077 | 2078 | 2079 | 2080 | 2081 | 2082 | 2083 | 2084 | 2085 | 2086 | 2087 | 2088 | 2089 | 2090 | 2091 | 2092 | 2093 | 2094 | 2095 | 2096 | 2097 | 2098 | 2099 | 2100 | 2101 | 2102 | 2103 | 2104 | 2105 | 2106 | 2107 | 2108 | 2109 | 2110 | 2111 | 2112 | 2113 | 2114 | 2115 | 2116 | 2117 | 2118 | 2119 | 2120 | 2121 | 2122 | 2123 | 2124 | 2125 | 2126 | 2127 | 2128 | 2129 | 2130 | 2131 | 2132 | 2133 | 2134 | 2135 | 2136 | 2137 | 2138 | 2139 | 2140 | 2141 | 2142 | 2143 | 2144 | 2145 | 2146 | 2147 | 2148 | 2149 | 2150 | 2151 | 2152 | 2153 | 2154 | 2155 | 2156 | 2157 | 2158 | 2159 | 2160 | 2161 | 2162 | 2163 | 2164 | 2165 | 2166 | 2167 | 2168 | 2169 | 2170 | 2171 | 2172 | 2173 | 2174 | 2175 | 2176 | 2177 | 2178 | 2179 | 2180 | 2181 | 2182 | 2183 | 2184 | 2185 | 2186 | 2187 | 2188 | 2189 | 2190 | 2191 | 2192 | 2193 | 2194 | 2195 | 2196 | 2197 | 2198 | 2199 | 2200 | 2201 | 2202 | 2203 | 2204 | 2205 | 2206 | 2207 | 2208 | 2209 | 2210 | 2211 | 2212 | 2213 | 2214 | 2215 | 2216 | 2217 | 2218 | 2219 | 2220 | 2221 | 2222 | 2223 | 2224 | 2225 | 2226 | 2227 | 2228 | 2229 | 2230 | 2231 | 2232 | 2233 | 2234 | 2235 | 2236 | 2237 | 2238 | 2239 | 2240 | 2241 | 2242 | 2243 | 2244 | 2245 | 2246 | 2247 | 2248 | 2249 | 2250 | 2251 | 2252 | 2253 | 2254 | 2255 | 2256 | 2257 | 2258 | 2259 | 2260 | 2261 | 2262 | 2263 | 2264 | 2265 | 2266 | 2267 | 2268 | 2269 | 2270 | 2271 | 2272 | 2273 | 2274 | 2275 | 2276 | 2277 | 2278 | 2279 | 2280 | 2281 | 2282 | 2283 | 2284 | 2285 | 2286 | 2287 | 2288 | 2289 | 2290 | 2291 | 2292 | 2293 | 2294 | 2295 | 2296 | 2297 | 2298 | 2299 | 2300 | 2301 | 2302 | 2303 | 2304 | 2305 | 2306 | 2307 | 2308 | 2309 | 2310 | 2311 | 2312 | 2313 | 2314 | 2315 | 2316 | 2317 | 2318 | 2319 | 2320 | 2321 | 2322 | 2323 | 2324 | 2325 | 2326 | 2327 | 2328 | 2329 | 2330 | 2331 | 2332 | 2333 | 2334 | 2335 | 2336 | 2337 | 2338 | 2339 | 2340 | 2341 | 2342 | 2343 | 2344 | 2345 | 2346 | 2347 | 2348 | 2349 | 2350 | 2351 | 2352 | 2353 | 2354 | 2355 | 2356 | 2357 | 2358 | 2359 | 2360 | 2361 | 2362 | 2363 | 2364 | 2365 | 2366 | 2367 | 2368 | 2369 | 2370 | 2371 | 2372 | 2373 | 2374 | 2375 | 2376 | 2377 | 2378 | 2379 | 2380 | 2381 | 2382 | 2383 | 2384 | 2385 | 2386 | 2387 | 2388 | 2389 | 2390 | 2391 | 2392 | 2393 | 2394 | 2395 | 2396 | 2397 | 2398 | 2399 | 2400 | 2401 | 2402 | 2403 | 2404 | 2405 | 2406 | 2407 | 2408 | 2409 | 2410 | 2411 | 2412 | 2413 | 2414 | 2415 | 2416 | 2417 | 2418 | 2419 | 2420 | 2421 | 2422 | 2 |
|--|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|---|
|--|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|---|

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|------|---------|---------|--------|-------------|
| SUBM | 18.37 | 14.93 | 3.45 | 94073. |
| | (467) | (379) | (88) | (2663.89) |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|-------|--------|
| CFS | 5438 | 4439 | 1893 | 783 | | 93912 |
| CMB | 154 | 126 | 54 | 22 | | 2659 |
| INCHES | | 8.66 | 14.76 | 15.26 | | 15.26 |
| MM | | 219.89 | 374.99 | 387.66 | | 387.66 |
| AC-FT | | 2201 | 3754 | 3881 | | 3881 |
| CU M | | 2715 | 4630 | 4787 | | 4787 |

#2ND

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

PRECIP(L) AND EXCESS(X)

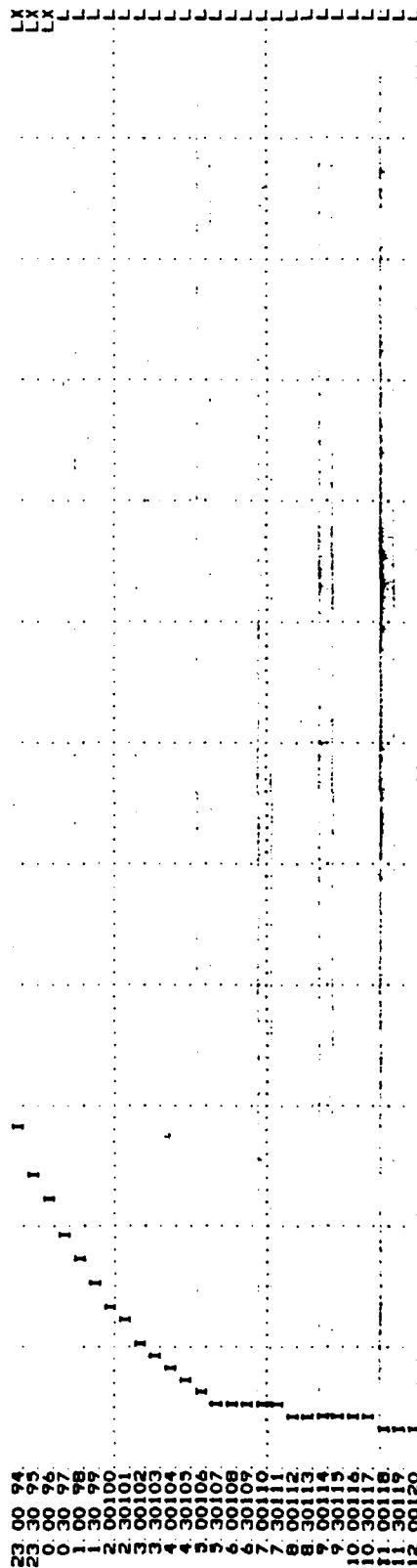
C-93

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PAGE 0077

FLAHERTY GIOVANA ASSOCIATES, P. C.

361
00 30 381
18 30 391
19 30 401
20 30 411
21 30 421
22 30 431
23 30 441
24 30 451
25 30 461
26 30 471
27 30 481
28 30 491
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30 30 511
31 30 521
32 30 531
33 30 541
34 30 551
35 30 561
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49 30 701
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59 30 801
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61 30 821
62 30 831
63 30 841
64 30 851
65 30 861
66 30 871
67 30 881
68 30 891
69 30 901
70 30 911
71 30 921
72 30 931



DVN

| TIME | DISCHARGE (CFS) | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | RTIO 1 | RTIO 2 |
|-------|-----------------|--------|---------|---------|--------------|--------|--------|
| 0000 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0001 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0002 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0003 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0004 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0005 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0006 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0007 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0008 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0009 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0010 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0011 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0012 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0013 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0014 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0015 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0016 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0017 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0018 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0019 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| 0020 | 100 | 100 | 100 | 100 | 100 | 1 | 1 |
| TOTAL | 100 | 100 | 100 | 100 | 100 | 1 | 1 |

THOUS CU H

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO 2

2 1

[illegible][illegible]

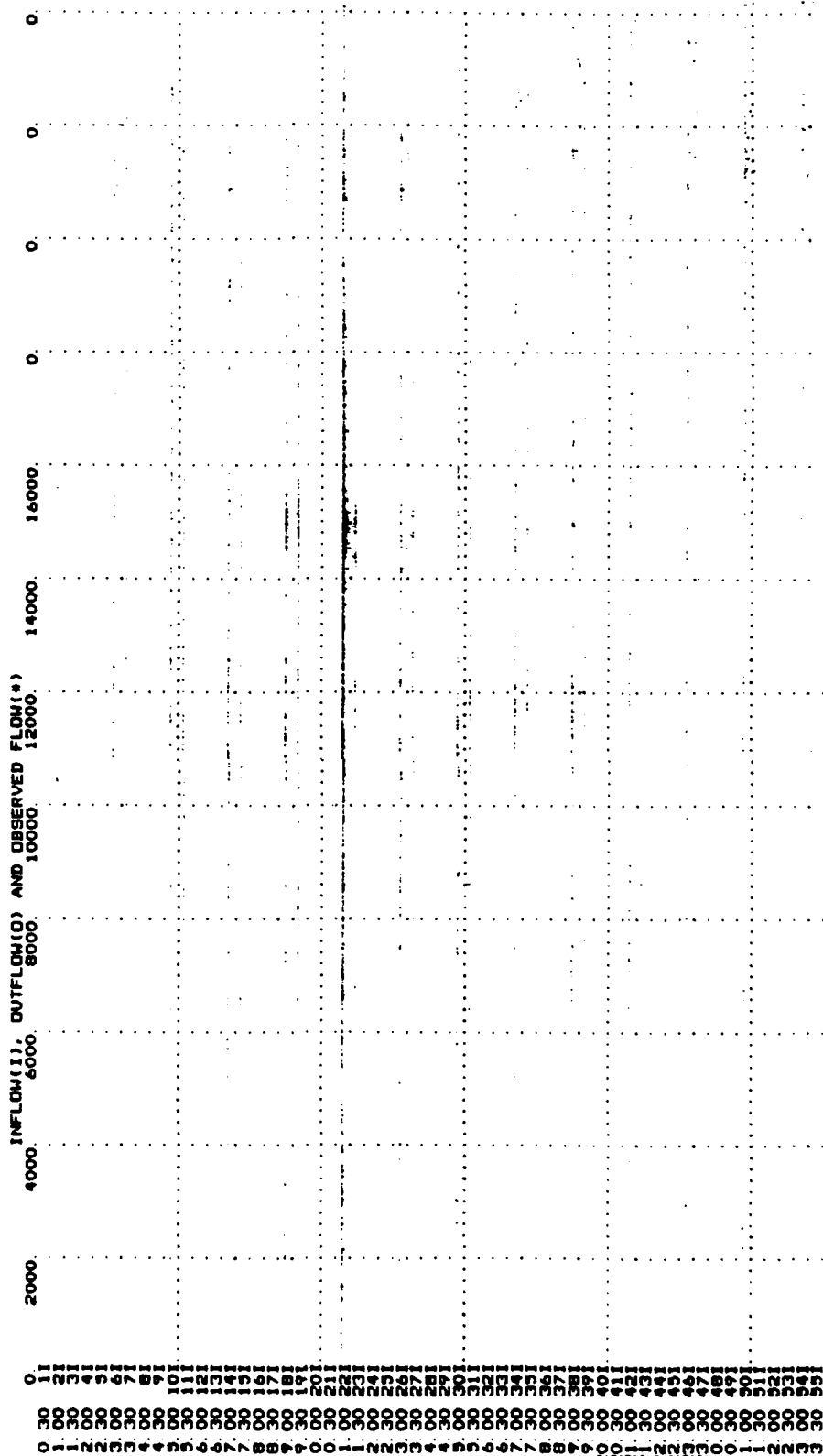
PAGE 0086

FLAHERTY GIAVARA ASSOCIATES, P. C.

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19 30 391
20 30 401
21 30 411
22 30 421
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87 30 1071
88 30 1081
89 30 1091
90 30 1101
91 30 1111
92 30 1121

PAGE 0088

FLAHERTY GIAVARA ASSOCIATES, P. C.



00 561
 4 50 571
 5 50 58
 6 50 59
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 8 50 61
 9 50 62
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 11 50 64
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14 00119
15 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 RTID 4 | |
|-------------------------|----|---------------|----|
| 28 | 26 | 23 | 22 |
| 19 | 18 | 17 | 16 |
| 14 | 13 | 12 | 11 |
| 10 | 9 | 8 | 7 |
| 6 | 5 | 4 | 3 |
| 3 | 2 | 1 | 0 |
| 28 | 26 | 23 | 22 |
| 19 | 18 | 17 | 16 |
| 14 | 13 | 12 | 11 |
| 10 | 9 | 8 | 7 |
| 6 | 5 | 4 | 3 |
| 3 | 2 | 1 | 0 |
| 28 | 26 | 23 | 22 |
| 19 | 18 | 17 | 16 |
| 14 | 13 | 12 | 11 |
| 10 | 9 | 8 | 7 |
| 6 | 5 | 4 | 3 |
| 3 | 2 | 1 | 0 |
| 28 | 26 | 23 | 22 |
| 19 | 18 | 17 | 16 |
| 14 | 13 | 12 | 11 |
| 10 | 9 | 8 | 7 |
| 6 | 5 | 4 | 3 |
| 3 | 2 | 1 | 0 |

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
13843 6360 2623 31477
392 180 74 8914
2 18 4 00 4 13
35 34 101 69 104 86
8869 12619 13008 13008
8467 15560 12045 12045

CFS
CHS
INCHES
AC-FT
THOUS CU M

OVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 0 | 0 | 0 |
|---|------|------|------|-------|-------|-------|-------|-------|----|----|----|
| 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 1 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| 2 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 | 3 |
| 3 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 | 4 |
| 4 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 | 5 |
| 5 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 | 6 |
| 6 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 | 7 |
| 7 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 | 8 |
| 8 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 | 9 |
| 9 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |

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57 00 120

OVN

SUM OF 2 HYDROGRAPHS AT
27 19 14 14 68 478
28 19 14 15 51 364
29 19 14 16 37 277
30 19 14 17 26 218
31 19 14 18 18 180

1 PLAN 1 R110 5
26 17 13 12 106 781
27 17 13 11 125 956
28 17 13 11 143 1136
29 17 13 11 159 1312
30 17 13 11 175 1492
31 17 13 11 191 1673
32 17 13 11 207 1854

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PEAK 16824.
CFS 14356.
CMB 407.
INCHES 2.24
MM 97.39
AC-FT 7119
THOUS CU M 8781

6-HOUR 14356.
24-HOUR 6596.
72-HOUR 2720.
TOTAL VOLUME 326458.
9244.
4.28
108.75
13490.
16640.

OVF

STATION 1
INFLW(1), OUTFLOW(1) AND OBSERVED FLOW(1)
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18 30 15
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21 00 18
22 30 19
23 00 20

OVN

SUM OF 2 HYDROGRAPHS AT

PLAN 1

RTIO 6

| STATION | INFLW (1) | OUTFLOW (2) | AND OBSERVED FLOW (3) |
|---------|-----------|-------------|-----------------------|
| 0 | 0 | 0 | 0 |
| 1 | 0 | 0 | 0 |
| 2 | 0 | 0 | 0 |
| 3 | 0 | 0 | 0 |
| 4 | 0 | 0 | 0 |
| 5 | 0 | 0 | 0 |
| 6 | 0 | 0 | 0 |
| 7 | 0 | 0 | 0 |
| 8 | 0 | 0 | 0 |
| 9 | 0 | 0 | 0 |
| 10 | 0 | 0 | 0 |
| 11 | 0 | 0 | 0 |
| 12 | 0 | 0 | 0 |
| 13 | 0 | 0 | 0 |
| 14 | 0 | 0 | 0 |
| 15 | 0 | 0 | 0 |
| 16 | 0 | 0 | 0 |
| 17 | 0 | 0 | 0 |
| 18 | 0 | 0 | 0 |
| 19 | 0 | 0 | 0 |
| 20 | 0 | 0 | 0 |
| 21 | 0 | 0 | 0 |
| 22 | 0 | 0 | 0 |
| 23 | 0 | 0 | 0 |
| 24 | 0 | 0 | 0 |
| 25 | 0 | 0 | 0 |
| 26 | 0 | 0 | 0 |
| 27 | 0 | 0 | 0 |
| 28 | 0 | 0 | 0 |
| 29 | 0 | 0 | 0 |
| 30 | 0 | 0 | 0 |
| 31 | 0 | 0 | 0 |
| 32 | 0 | 0 | 0 |
| 33 | 0 | 0 | 0 |
| 34 | 0 | 0 | 0 |
| 35 | 0 | 0 | 0 |
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| 37 | 0 | 0 | 0 |
| 38 | 0 | 0 | 0 |
| 39 | 0 | 0 | 0 |
| 40 | 0 | 0 | 0 |
| 41 | 0 | 0 | 0 |
| 42 | 0 | 0 | 0 |
| 43 | 0 | 0 | 0 |
| 44 | 0 | 0 | 0 |
| 45 | 0 | 0 | 0 |
| 46 | 0 | 0 | 0 |
| 47 | 0 | 0 | 0 |
| 48 | 0 | 0 | 0 |
| 49 | 0 | 0 | 0 |
| 50 | 0 | 0 | 0 |
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| 52 | 0 | 0 | 0 |
| 53 | 0 | 0 | 0 |
| 54 | 0 | 0 | 0 |
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| 56 | 0 | 0 | 0 |
| 57 | 0 | 0 | 0 |
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| 70 | 0 | 0 | 0 |
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| 73 | 0 | 0 | 0 |
| 74 | 0 | 0 | 0 |
| 75 | 0 | 0 | 0 |
| 76 | 0 | 0 | 0 |
| 77 | 0 | 0 | 0 |
| 78 | 0 | 0 | 0 |
| 79 | 0 | 0 | 0 |
| 80 | 0 | 0 | 0 |
| 81 | 0 | 0 | 0 |
| 82 | 0 | 0 | 0 |
| 83 | 0 | 0 | 0 |
| 84 | 0 | 0 | 0 |
| 85 | 0 | 0 | 0 |
| 86 | 0 | 0 | 0 |
| 87 | 0 | 0 | 0 |
| 88 | 0 | 0 | 0 |
| 89 | 0 | 0 | 0 |
| 90 | 0 | 0 | 0 |
| 91 | 0 | 0 | 0 |
| 92 | 0 | 0 | 0 |
| 93 | 0 | 0 | 0 |
| 94 | 0 | 0 | 0 |
| 95 | 0 | 0 | 0 |
| 96 | 0 | 0 | 0 |
| 97 | 0 | 0 | 0 |
| 98 | 0 | 0 | 0 |
| 99 | 0 | 0 | 0 |
| 100 | 0 | 0 | 0 |

TOTAL VOLUME

338117
9374
4.43
112.63
13972
17234

OVF

STATION 1

INFLW (1), OUTFLOW (2) AND OBSERVED FLOW (3)

4000 6000 8000 10000 12000 14000 16000 18000

0
0.30
1.00

30 61 1
 7 00 62 1
 8 00 63 1
 9 00 64 1
 10 00 65 1
 11 00 66 1
 12 00 67 1
 13 00 68 1
 14 00 69 1
 15 00 70 1
 16 00 71 1
 17 00 72 1
 18 00 73 1
 19 00 74 1
 20 00 75 1
 21 00 76 1
 22 00 77 1
 23 00 78 1
 24 00 79 1
 25 00 80 1
 26 00 81 1
 27 00 82 1
 28 00 83 1
 29 00 84 1
 30 00 85 1
 31 00 86 1
 32 00 87 1
 33 00 88 1
 34 00 89 1
 35 00 90 1
 36 00 91 1
 37 00 92 1
 38 00 93 1
 39 00 94 1
 40 00 95 1
 41 00 96 1
 42 00 97 1
 43 00 98 1
 44 00 99 1
 45 00 100 1
 46 00 101 1
 47 00 102 1
 48 00 103 1
 49 00 104 1
 50 00 105 1
 51 00 106 1
 52 00 107 1
 53 00 108 1
 54 00 109 1
 55 00 110 1
 56 00 111 1
 57 00 112 1
 58 00 113 1
 59 00 114 1
 60 00 115 1
 61 00 116 1
 62 00 117 1
 63 00 118 1

11. 30119.
12. 00120.

◆NO◆

[illegible]

POWER

[illegible]

PAGE 0099

FLAHERTY GIAVARA ASSOCIATES, P. C.

241
00 23 21
00 23 20 27 1
00 23 20 28 1
00 23 20 30 1
00 23 20 31 1
00 23 20 32 1
00 23 20 33 1
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SUM OF 2 HYDROGRAPHS AT
32 32
33 33
34 34
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1 PLAN 1 RTIO 8
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100 100

PEAK 30042
 CFS 25636
 CHS 726
 INCHES 4.03
 MM 102.47
 AC-FT 12712
 THOUS CU M 15680

24-HOUR 11778
 72-HOUR 4838
 TOTAL VOLUME 382760
 16508
 194.19
 24089
 29714

OVF

STATION 1

| INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*) | | 8000 | 4000 | 0 |
|--|---------|---------|---------|---------|
| 12000 | 16000 | 20000 | 24000 | 32000 |
| 0 11 | 0 11 | 0 11 | 0 11 | 0 11 |
| 1 12 | 1 12 | 1 12 | 1 12 | 1 12 |
| 2 13 | 2 13 | 2 13 | 2 13 | 2 13 |
| 3 14 | 3 14 | 3 14 | 3 14 | 3 14 |
| 4 15 | 4 15 | 4 15 | 4 15 | 4 15 |
| 5 16 | 5 16 | 5 16 | 5 16 | 5 16 |
| 6 17 | 6 17 | 6 17 | 6 17 | 6 17 |
| 7 18 | 7 18 | 7 18 | 7 18 | 7 18 |
| 8 19 | 8 19 | 8 19 | 8 19 | 8 19 |
| 9 20 | 9 20 | 9 20 | 9 20 | 9 20 |
| 10 21 | 10 21 | 10 21 | 10 21 | 10 21 |
| 11 22 | 11 22 | 11 22 | 11 22 | 11 22 |
| 12 23 | 12 23 | 12 23 | 12 23 | 12 23 |
| 13 24 | 13 24 | 13 24 | 13 24 | 13 24 |
| 14 25 | 14 25 | 14 25 | 14 25 | 14 25 |
| 15 26 | 15 26 | 15 26 | 15 26 | 15 26 |
| 16 27 | 16 27 | 16 27 | 16 27 | 16 27 |
| 17 28 | 17 28 | 17 28 | 17 28 | 17 28 |
| 18 29 | 18 29 | 18 29 | 18 29 | 18 29 |
| 19 30 | 19 30 | 19 30 | 19 30 | 19 30 |
| 20 31 | 20 31 | 20 31 | 20 31 | 20 31 |
| 21 32 | 21 32 | 21 32 | 21 32 | 21 32 |
| 22 33 | 22 33 | 22 33 | 22 33 | 22 33 |
| 23 34 | 23 34 | 23 34 | 23 34 | 23 34 |
| 24 35 | 24 35 | 24 35 | 24 35 | 24 35 |
| 25 36 | 25 36 | 25 36 | 25 36 | 25 36 |
| 26 37 | 26 37 | 26 37 | 26 37 | 26 37 |
| 27 38 | 27 38 | 27 38 | 27 38 | 27 38 |
| 28 39 | 28 39 | 28 39 | 28 39 | 28 39 |
| 29 40 | 29 40 | 29 40 | 29 40 | 29 40 |
| 30 41 | 30 41 | 30 41 | 30 41 | 30 41 |
| 31 42 | 31 42 | 31 42 | 31 42 | 31 42 |
| 32 43 | 32 43 | 32 43 | 32 43 | 32 43 |
| 33 44 | 33 44 | 33 44 | 33 44 | 33 44 |
| 34 45 | 34 45 | 34 45 | 34 45 | 34 45 |
| 35 46 | 35 46 | 35 46 | 35 46 | 35 46 |
| 36 47 | 36 47 | 36 47 | 36 47 | 36 47 |
| 37 48 | 37 48 | 37 48 | 37 48 | 37 48 |
| 38 49 | 38 49 | 38 49 | 38 49 | 38 49 |
| 39 50 | 39 50 | 39 50 | 39 50 | 39 50 |
| 40 51 | 40 51 | 40 51 | 40 51 | 40 51 |
| 41 52 | 41 52 | 41 52 | 41 52 | 41 52 |
| 42 53 | 42 53 | 42 53 | 42 53 | 42 53 |
| 43 54 | 43 54 | 43 54 | 43 54 | 43 54 |
| 44 55 | 44 55 | 44 55 | 44 55 | 44 55 |
| 45 56 | 45 56 | 45 56 | 45 56 | 45 56 |
| 46 57 | 46 57 | 46 57 | 46 57 | 46 57 |
| 47 58 | 47 58 | 47 58 | 47 58 | 47 58 |
| 48 59 | 48 59 | 48 59 | 48 59 | 48 59 |
| 49 60 | 49 60 | 49 60 | 49 60 | 49 60 |
| 50 61 | 50 61 | 50 61 | 50 61 | 50 61 |
| 51 62 | 51 62 | 51 62 | 51 62 | 51 62 |
| 52 63 | 52 63 | 52 63 | 52 63 | 52 63 |
| 53 64 | 53 64 | 53 64 | 53 64 | 53 64 |
| 54 65 | 54 65 | 54 65 | 54 65 | 54 65 |
| 55 66 | 55 66 | 55 66 | 55 66 | 55 66 |
| 56 67 | 56 67 | 56 67 | 56 67 | 56 67 |
| 57 68 | 57 68 | 57 68 | 57 68 | 57 68 |
| 58 69 | 58 69 | 58 69 | 58 69 | 58 69 |
| 59 70 | 59 70 | 59 70 | 59 70 | 59 70 |
| 60 71 | 60 71 | 60 71 | 60 71 | 60 71 |
| 61 72 | 61 72 | 61 72 | 61 72 | 61 72 |
| 62 73 | 62 73 | 62 73 | 62 73 | 62 73 |
| 63 74 | 63 74 | 63 74 | 63 74 | 63 74 |
| 64 75 | 64 75 | 64 75 | 64 75 | 64 75 |
| 65 76 | 65 76 | 65 76 | 65 76 | 65 76 |
| 66 77 | 66 77 | 66 77 | 66 77 | 66 77 |
| 67 78 | 67 78 | 67 78 | 67 78 | 67 78 |
| 68 79 | 68 79 | 68 79 | 68 79 | 68 79 |
| 69 80 | 69 80 | 69 80 | 69 80 | 69 80 |
| 70 81 | 70 81 | 70 81 | 70 81 | 70 81 |
| 71 82 | 71 82 | 71 82 | 71 82 | 71 82 |
| 72 83 | 72 83 | 72 83 | 72 83 | 72 83 |
| 73 84 | 73 84 | 73 84 | 73 84 | 73 84 |
| 74 85 | 74 85 | 74 85 | 74 85 | 74 85 |
| 75 86 | 75 86 | 75 86 | 75 86 | 75 86 |
| 76 87 | 76 87 | 76 87 | 76 87 | 76 87 |
| 77 88 | 77 88 | 77 88 | 77 88 | 77 88 |
| 78 89 | 78 89 | 78 89 | 78 89 | 78 89 |
| 79 90 | 79 90 | 79 90 | 79 90 | 79 90 |
| 80 91 | 80 91 | 80 91 | 80 91 | 80 91 |
| 81 92 | 81 92 | 81 92 | 81 92 | 81 92 |
| 82 93 | 82 93 | 82 93 | 82 93 | 82 93 |
| 83 94 | 83 94 | 83 94 | 83 94 | 83 94 |
| 84 95 | 84 95 | 84 95 | 84 95 | 84 95 |
| 85 96 | 85 96 | 85 96 | 85 96 | 85 96 |
| 86 97 | 86 97 | 86 97 | 86 97 | 86 97 |
| 87 98 | 87 98 | 87 98 | 87 98 | 87 98 |
| 88 99 | 88 99 | 88 99 | 88 99 | 88 99 |
| 89 100 | 89 100 | 89 100 | 89 100 | 89 100 |
| 90 101 | 90 101 | 90 101 | 90 101 | 90 101 |
| 91 102 | 91 102 | 91 102 | 91 102 | 91 102 |
| 92 103 | 92 103 | 92 103 | 92 103 | 92 103 |
| 93 104 | 93 104 | 93 104 | 93 104 | 93 104 |
| 94 105 | 94 105 | 94 105 | 94 105 | 94 105 |
| 95 106 | 95 106 | 95 106 | 95 106 | 95 106 |
| 96 107 | 96 107 | 96 107 | 96 107 | 96 107 |
| 97 108 | 97 108 | 97 108 | 97 108 | 97 108 |
| 98 109 | 98 109 | 98 109 | 98 109 | 98 109 |
| 99 110 | 99 110 | 99 110 | 99 110 | 99 110 |
| 100 111 | 100 111 | 100 111 | 100 111 | 100 111 |

3 30103
4 30104
5 30105
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18 30118
19 30119
20 30120



OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | MTD 9 | |
|-------------------------|---------|---------|--------------|--------|---------|
| 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | 6-HOUR | 24-HOUR |
| 109 | 109 | 93 | 86 | 83 | 80 |
| 177 | 177 | 64 | 60 | 58 | 57 |
| 53 | 53 | 47 | 46 | 46 | 46 |
| 47 | 47 | 39 | 43 | 39 | 43 |
| 59 | 59 | 46 | 40 | 40 | 47 |
| 62 | 62 | 44 | 44 | 44 | 47 |
| 77 | 77 | 311 | 447 | 311 | 369 |
| 44 | 44 | 230 | 315 | 230 | 287 |
| 327 | 327 | 782 | 14970 | 782 | 14970 |
| 34130 | 34130 | 5696 | 10085 | 5696 | 10085 |
| 48377 | 48377 | 32610 | 26302 | 32610 | 26302 |
| 17446 | 17446 | 1243 | 9210 | 1243 | 9210 |
| 6436 | 6436 | 5334 | 4911 | 5334 | 4911 |
| | | 5334 | 4911 | 5334 | 4911 |

PEAK
40083
1701
CFS
CMR
INCHES
AC-FT
THOUS CU FT

OVF

0 30
1 30
2 30
3 30
4 30
5 30
6 30
7 30
8 30
9 30
10 30
11 30
12 30
13 30
14 30
15 30
16 30
17 30
18 30
19 30
20 30

STATION 1
INFLOW (1), OUTFLOW (2) AND OBSERVED FLOW (3)
30000 40000 50000 60000

9 00 66
 9 30 67
 10 00 68
 10 30 69
 11 00 70
 11 30 71
 12 00 72
 12 30 73
 13 00 74
 13 30 75
 14 00 76
 14 30 77
 15 00 78
 15 30 79
 16 00 80
 16 30 81
 17 00 82
 17 30 83
 18 00 84
 18 30 85
 19 00 86
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 21 00 90
 21 30 91
 22 00 92
 22 30 93
 23 00 94
 23 30 95
 0 00 96
 0 30 97
 1 00 98
 1 30 99
 2 00 00
 2 30 01
 3 00 02
 3 30 03
 4 00 04
 4 30 05
 5 00 06
 5 30 07
 6 00 08
 6 30 09
 7 00 10
 7 30 11
 8 00 12
 8 30 13
 9 00 14
 9 30 15
 10 00 16
 10 30 17
 11 00 18
 11 30 19
 12 00 20

OVN

***** SUB-AREA RUNOFF COMPUTATION *****

INFLOW HYDROGRAPH - SUBWATERSHED NO. 9

| INVDG | IUNG | TAREA | SNAP | HYDROGRAPH DATA | RATID | ISNOW | ISAME | LDLAL | JPLY | JPT | INAME | ISTAGE | IAUTO |
|-------|------|-------|-------|-----------------|--------|--------|-------|-------|------|-----|-------|--------|-------|
| 1 | 1 | 3.56 | 0.00 | TRSDA TRSPC | 0.000 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 |
| | | | | PRECIP DATA | | | | | | | | | |
| | | SPFE | R6 | R12 | R48 | R72 | R96 | | | | | | |
| | | 0.00 | 86.00 | 100.00 | 112.00 | 119.00 | 0.00 | | | | | | |

TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA

| LRDPT | STMR | DLTKR | RTIOL | ERAIN | STIRKS | RTIOL | STIRL | CNSTL | ALSMX | RTIMP |
|-------|------|-------|-------|-------|--------|-------|-------|-------|-------|-------|
| 0 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.10 | 0.00 | 0.00 |

UNIT HYDROGRAPH DATA NTA= 0

TP= 3.05 CP=0.63

APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 6.78 AND R= 5.41 INTERVALS

UNIT HYDROGRAPH 33 END-OF-PERIOD ORIGINATES, LAG= 3.02 HOURS, CP= 0.63 VOL= 1.00

| MO | DA | HR | MM | PERIOD | RAIN | EXCS | LOSS | END-OF-PERIOD FLOW | COMP | DA | HR | MM | PERIOD | RAIN | EXCS | LOSS | COMP |
|----|----|----|----|--------|------|------|------|--------------------|------|----|----|----|--------|------|------|------|------|
| 1 | 01 | 0 | 30 | 1 | 0.00 | 0.00 | 0.00 | 1.02 | 11 | 02 | 7 | 30 | 41 | 0.18 | 1.13 | 0.00 | 77.3 |
| 1 | 01 | 1 | 30 | 2 | 0.00 | 0.00 | 0.00 | 1.02 | 10 | 02 | 7 | 30 | 42 | 0.18 | 1.13 | 0.00 | 100 |
| 1 | 01 | 2 | 30 | 3 | 0.00 | 0.00 | 0.00 | 1.02 | 10 | 02 | 8 | 30 | 43 | 0.18 | 1.13 | 0.00 | 142 |
| 1 | 01 | 3 | 30 | 4 | 0.00 | 0.00 | 0.00 | 1.02 | 9 | 02 | 8 | 30 | 44 | 0.18 | 1.13 | 0.00 | 205 |
| 1 | 01 | 4 | 30 | 5 | 0.00 | 0.00 | 0.00 | 1.02 | 9 | 02 | 9 | 30 | 45 | 0.18 | 1.13 | 0.00 | 282 |
| 1 | 01 | 5 | 30 | 6 | 0.00 | 0.00 | 0.00 | 1.02 | 8 | 02 | 9 | 30 | 46 | 0.18 | 1.13 | 0.00 | 374 |
| 1 | 01 | 6 | 30 | 7 | 0.00 | 0.00 | 0.00 | 1.02 | 8 | 02 | 10 | 30 | 47 | 0.18 | 1.13 | 0.00 | 444 |
| 1 | 01 | 7 | 30 | 8 | 0.00 | 0.00 | 0.00 | 1.02 | 8 | 02 | 10 | 30 | 48 | 0.18 | 1.13 | 0.00 | 544 |
| 1 | 01 | 8 | 30 | 9 | 0.00 | 0.00 | 0.00 | 1.02 | 8 | 02 | 11 | 30 | 49 | 0.18 | 1.13 | 0.00 | 610 |
| 1 | 01 | 9 | 30 | 10 | 0.00 | 0.00 | 0.00 | 1.02 | 7 | 02 | 11 | 30 | 50 | 0.18 | 1.13 | 0.00 | 665 |
| 1 | 01 | 10 | 30 | 11 | 0.00 | 0.00 | 0.00 | 1.02 | 7 | 02 | 12 | 30 | 51 | 0.18 | 1.13 | 0.00 | 711 |
| 1 | 01 | 11 | 30 | 12 | 0.00 | 0.00 | 0.00 | 1.02 | 7 | 02 | 12 | 30 | 52 | 0.18 | 1.13 | 0.00 | 749 |
| 1 | 01 | 12 | 30 | 13 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 13 | 30 | 53 | 0.18 | 1.13 | 0.00 | 803 |
| 1 | 01 | 13 | 30 | 14 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 13 | 30 | 54 | 0.18 | 1.13 | 0.00 | 812 |
| 1 | 01 | 14 | 30 | 15 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 14 | 30 | 55 | 0.18 | 1.13 | 0.00 | 893 |
| 1 | 01 | 15 | 30 | 16 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 15 | 30 | 56 | 0.18 | 1.13 | 0.00 | 1103 |
| 1 | 01 | 16 | 30 | 17 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 16 | 30 | 57 | 0.18 | 1.13 | 0.00 | 1393 |
| 1 | 01 | 17 | 30 | 18 | 0.00 | 0.00 | 0.00 | 1.02 | 6 | 02 | 17 | 30 | 58 | 0.18 | 1.13 | 0.00 | 1783 |

FLAHERTY CIAVARA ASSOCIATES, P. C.

[illegible]

HYDROGRAPH AT STA 1 FOR PLAN 1. RTIO 8

17 00 341
17 00 351
17 00 361
17 00 371
17 00 381
17 00 391
17 00 401
17 00 411
17 00 421
17 00 431
17 00 441
17 00 451
17 00 461
17 00 471
17 00 481
17 00 491
17 00 501
17 00 511
17 00 521
17 00 531
17 00 541
17 00 551
17 00 561
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17 00 781
17 00 791
17 00 801
17 00 811
17 00 821
17 00 831
17 00 841
17 00 851
17 00 861
17 00 871
17 00 881
17 00 891
17 00 901
17 00 911
17 00 921
17 00 931
17 00 941
17 00 951
17 00 961
17 00 971
17 00 981
17 00 991
17 00 1001

STATION 1

INFLOW(1), OUTFLOW(1) AND OBSERVED FLOW(1)

4000. 6000. 8000. 10000. 12000. 14000. 16000. 18000. 0.

0.11 30.00 0.12 30.00 0.13 30.00 0.14 30.00 0.15 30.00 0.16 30.00 0.17 30.00 0.18 30.00 0.19 30.00 0.20 30.00 0.21 30.00 0.22 30.00 0.23 30.00 0.24 30.00 0.25 30.00 0.26 30.00 0.27 30.00 0.28 30.00 0.29 30.00 0.30 30.00 0.31 30.00 0.32 30.00 0.33 30.00 0.34 30.00 0.35 30.00 0.36 30.00 0.37 30.00 0.38 30.00 0.39 30.00 0.40 30.00 0.41 30.00 0.42 30.00 0.43 30.00 0.44 30.00 0.45 30.00 0.46 30.00 0.47 30.00 0.48 30.00 0.49 30.00 0.50 30.00 0.51 30.00 0.52 30.00 0.53 30.00 0.54 30.00 0.55 30.00 0.56 30.00 0.57 30.00 0.58 30.00 0.59 30.00 0.60 30.00 0.61 30.00 0.62 30.00 0.63 30.00 0.64 30.00 0.65 30.00 0.66 30.00 0.67 30.00 0.68 30.00 0.69 30.00 0.70 30.00 0.71 30.00 0.72 30.00 0.73 30.00 0.74 30.00 0.75 30.00 0.76 30.00 0.77 30.00 0.78 30.00 0.79 30.00 0.80 30.00 0.81 30.00 0.82 30.00 0.83 30.00 0.84 30.00 0.85 30.00 0.86 30.00 0.87 30.00 0.88 30.00 0.89 30.00 0.90 30.00 0.91 30.00 0.92 30.00 0.93 30.00 0.94 30.00 0.95 30.00 0.96 30.00 0.97 30.00 0.98 30.00 0.99 30.00 1.00 30.00

3 30 551
4 30 561
5 30 571
6 30 581
7 30 591
8 30 601
9 30 611
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18 30 701
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24 30 761
25 30 771
26 30 781
27 30 791
28 30 801
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30 30 821
31 30 831
32 30 841
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34 30 861
35 30 871
36 30 881
37 30 891
38 30 901
39 30 911
40 30 921
41 30 931
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43 30 951
44 30 961
45 30 971
46 30 981
47 30 991
48 30 1001
49 30 1011
50 30 1021
51 30 1031
52 30 1041
53 30 1051
54 30 1061
55 30 1071
56 30 1081
57 30 1091
58 30 1101
59 30 1111
60 30 1121

9 00 181
9 00 201
10 00 211
10 00 221
11 00 231
11 00 241
12 00 251
12 00 261
13 00 271
13 00 281
14 00 291
14 00 301
15 00 311
15 00 321
16 00 331
16 00 341
17 00 351
17 00 361
18 00 371
18 00 381
19 00 391
19 00 401
20 00 411
20 00 421
21 00 431
21 00 441
22 00 451
22 00 461
23 00 471
23 00 481
24 00 491
24 00 501
25 00 511
25 00 521
26 00 531
26 00 541
27 00 551
27 00 561
28 00 571
28 00 581
29 00 591
29 00 601
30 00 611
30 00 621
31 00 631
31 00 641
32 00 651
32 00 661
33 00 671
33 00 681
34 00 691
34 00 701
35 00 711
35 00 721
36 00 731
36 00 741
37 00 751

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FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT
NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)
JUL 81 H C FLAHERTY

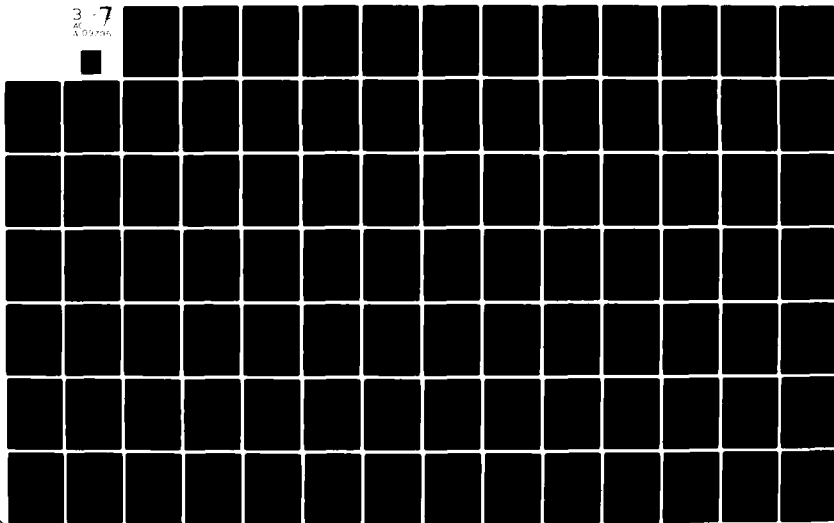
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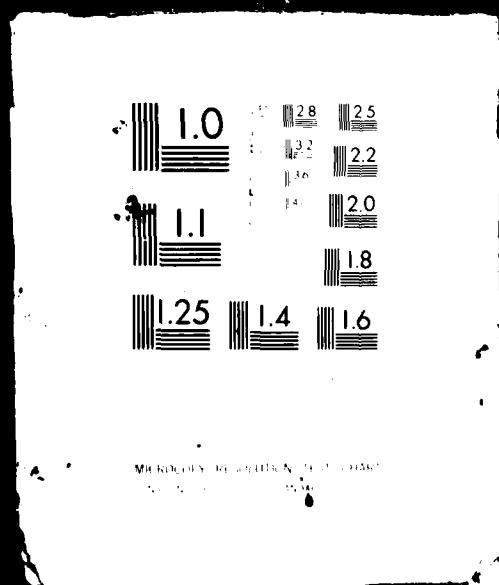
3-7
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3 00700



3 OF 7

AD-

A109795



14 00 76
15 00 76
16 00 80
17 00 81
18 00 83
19 00 84
20 00 85
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22 00 88
23 00 89
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33 01 00
34 01 01
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44 01 11
45 01 12
46 01 13
47 01 14
48 01 15
49 01 16
50 01 17
51 01 18
52 01 19
53 01 20

DN

SUM OF 2 HYDROGRAPHS AT
20 00 80
21 00 81
22 00 83
23 00 84
24 00 85
25 00 87
26 00 88
27 00 89
28 00 90
29 00 92
30 00 93
31 00 94
32 00 95
33 00 96
34 00 97
35 00 98
36 00 99
37 01 00
38 01 01
39 01 02
40 01 03
41 01 04
42 01 05
43 01 06
44 01 07
45 01 08
46 01 09
47 01 10
48 01 11
49 01 12
50 01 13
51 01 14
52 01 15
53 01 16
54 01 17
55 01 18
56 01 19
57 01 20

1 PLAN 1 RTID 4
28 00 80
29 00 81
30 00 83
31 00 84
32 00 85
33 00 87
34 00 88
35 00 89
36 00 90
37 00 92
38 00 93
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41 00 96
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43 00 98
44 00 99
45 01 00
46 01 01
47 01 02
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50 01 05
51 01 06
52 01 07
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54 01 09
55 01 10
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57 01 12
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59 01 14
60 01 15
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63 01 18
64 01 19
65 01 20

25 00 80
26 00 81
27 00 83
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29 00 85
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33 00 90
34 00 92
35 00 93
36 00 94
37 00 95
38 00 96
39 00 97
40 00 98
41 00 99
42 01 00
43 01 01
44 01 02
45 01 03
46 01 04
47 01 05
48 01 06
49 01 07
50 01 08
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53 01 11
54 01 12
55 01 13
56 01 14
57 01 15
58 01 16
59 01 17
60 01 18
61 01 19
62 01 20

| | | | | | | | | | |
|--------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 175 | 237 | 306 | 406 | 538 | 678 | 878 | 1069 | 1261 | 1449 |
| 1616 | 1772 | 1943 | 2184 | 2537 | 3033 | 3698 | 4544 | 5567 | 6924 |
| 8685 | 10659 | 12673 | 14986 | 18207 | 17346 | 17908 | 17897 | 17377 | 16452 |
| 13288 | 14022 | 12724 | 11472 | 10320 | 9279 | 8344 | 7506 | 6753 | 6073 |
| 5456 | 4906 | 4419 | 3767 | 3560 | 3191 | 2890 | 2640 | 2413 | 2207 |
| 2049 | 1927 | 1814 | 1708 | 1610 | 1518 | 1432 | 1364 | 1310 | 1258 |
| TOTAL VOLUME | | | | | | | | | |
| PEAK | | | | | | | | | |
| CFB | | | | | | | | | |
| CMS | | | | | | | | | |
| INCHES | | | | | | | | | |
| MM | | | | | | | | | |
| AC-FT | | | | | | | | | |
| THOUS CU M | | | | | | | | | |
| 6-HOUR | | | | | | | | | |
| 24-HOUR | | | | | | | | | |
| 72-HOUR | | | | | | | | | |
| TOTAL VOLUME | | | | | | | | | |
| 17908 | | | | | | | | | |
| 15296 | | | | | | | | | |
| 433 | | | | | | | | | |
| 2.20 | | | | | | | | | |
| 35.88 | | | | | | | | | |
| 7583 | | | | | | | | | |
| 4355 | | | | | | | | | |
| 6769 | | | | | | | | | |
| 197 | | | | | | | | | |
| 81 | | | | | | | | | |
| 4.14 | | | | | | | | | |
| 103.12 | | | | | | | | | |
| 14266 | | | | | | | | | |
| 17597 | | | | | | | | | |

•OVF•

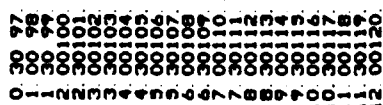
STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(S)

| 2000. | 4000. | 6000. | 8000. | 10000. | 12000. | 14000. | 16000. | 18000. | 0. |
|-------|-------|-------|-------|--------|--------|--------|--------|--------|-------|
| 0.1 | 1.2 | 2.3 | 3.4 | 4.5 | 5.6 | 6.7 | 7.8 | 8.9 | 10.0 |
| 10.1 | 11.2 | 12.3 | 13.4 | 14.5 | 15.6 | 16.7 | 17.8 | 18.9 | 20.0 |
| 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 | 30.0 |
| 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 | 40.0 |
| 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 | 50.0 |
| 60.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 | 60.0 |
| 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 | 70.0 |
| 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 | 80.0 |
| 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 | 90.0 |
| 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 |
| 110.0 | 110.0 | 110.0 | 110.0 | 110.0 | 110.0 | 110.0 | 110.0 | 110.0 | 110.0 |
| 120.0 | 120.0 | 120.0 | 120.0 | 120.0 | 120.0 | 120.0 | 120.0 | 120.0 | 120.0 |
| 130.0 | 130.0 | 130.0 | 130.0 | 130.0 | 130.0 | 130.0 | 130.0 | 130.0 | 130.0 |
| 140.0 | 140.0 | 140.0 | 140.0 | 140.0 | 140.0 | 140.0 | 140.0 | 140.0 | 140.0 |
| 150.0 | 150.0 | 150.0 | 150.0 | 150.0 | 150.0 | 150.0 | 150.0 | 150.0 | 150.0 |
| 160.0 | 160.0 | 160.0 | 160.0 | 160.0 | 160.0 | 160.0 | 160.0 | 160.0 | 160.0 |
| 170.0 | 170.0 | 170.0 | 170.0 | 170.0 | 170.0 | 170.0 | 170.0 | 170.0 | 170.0 |
| 180.0 | 180.0 | 180.0 | 180.0 | 180.0 | 180.0 | 180.0 | 180.0 | 180.0 | 180.0 |
| 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 | 190.0 |
| 200.0 | 200.0 | 200.0 | 200.0 | 200.0 | 200.0 | 200.0 | 200.0 | 200.0 | 200.0 |

FLAHERTY GIAVARA ASSOCIATES, P. C.

[illegible]



◆◆◆

| | SUM OF 2 HYDROGRAPHS AT | | | | 1 PLAN 1 RTID 5 | | | |
|-----|-------------------------|-----|-----|-----|-----------------|-----|-----|-----|
| 33 | 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 |
| 32 | 31 | 30 | 29 | 28 | 27 | 26 | 25 | 24 |
| 31 | 30 | 29 | 28 | 27 | 26 | 25 | 24 | 23 |
| 30 | 29 | 28 | 27 | 26 | 25 | 24 | 23 | 22 |
| 29 | 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 |
| 28 | 27 | 26 | 25 | 24 | 23 | 22 | 21 | 20 |
| 27 | 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 |
| 26 | 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 |
| 25 | 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 |
| 24 | 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 |
| 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 |
| 22 | 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 |
| 21 | 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 |
| 20 | 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 |
| 19 | 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 |
| 18 | 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 |
| 17 | 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 |
| 16 | 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 |
| 15 | 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 |
| 14 | 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 |
| 13 | 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 |
| 12 | 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 |
| 11 | 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 |
| 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 |
| 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 |
| 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | -1 |
| 6 | 5 | 4 | 3 | 2 | 1 | 0 | -1 | -2 |
| 5 | 4 | 3 | 2 | 1 | 0 | -1 | -2 | -3 |
| 4 | 3 | 2 | 1 | 0 | -1 | -2 | -3 | -4 |
| 3 | 2 | 1 | 0 | -1 | -2 | -3 | -4 | -5 |
| 2 | 1 | 0 | -1 | -2 | -3 | -4 | -5 | -6 |
| 1 | 0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 |
| 0 | -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 |
| -1 | -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 |
| -2 | -3 | -4 | -5 | -6 | -7 | -8 | -9 | -10 |
| -3 | -4 | -5 | -6 | -7 | -8 | -9 | -10 | -11 |
| -4 | -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 |
| -5 | -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 |
| -6 | -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 |
| -7 | -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 |
| -8 | -9 | -10 | -11 | -12 | -13 | -14 | -15 | -16 |
| -9 | -10 | -11 | -12 | -13 | -14 | -15 | -16 | -17 |
| -10 | -11 | -12 | -13 | -14 | -15 | -16 | -17 | -18 |
| -11 | -12 | -13 | -14 | -15 | -16 | -17 | -18 | -19 |
| -12 | -13 | -14 | -15 | -16 | -17 | -18 | -19 | -20 |
| -13 | -14 | -15 | -16 | -17 | -18 | -19 | -20 | -21 |
| -14 | -15 | -16 | -17 | -18 | -19 | -20 | -21 | -22 |
| -15 | -16 | -17 | -18 | -19 | -20 | -21 | -22 | -23 |
| -16 | -17 | -18 | -19 | -20 | -21 | -22 | -23 | -24 |
| -17 | -18 | -19 | -20 | -21 | -22 | -23 | -24 | -25 |
| -18 | -19 | -20 | -21 | -22 | -23 | -24 | -25 | -26 |
| -19 | -20 | -21 | -22 | -23 | -24 | -25 | -26 | -27 |
| -20 | -21 | | | | | | | |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------------|--------|--------|---------|---------|---------|--------|
| CFS | 18572. | 15862. | 7227. | 2989. | 358030. | |
| CMB | 526. | 449. | 209. | 84. | 10138. | |
| INCHES | | 2.28 | 4.16 | 4.29 | | |
| PM | | 97.95 | 105.62 | 109.01 | | |
| AC-FY | | 7863. | 14334. | 17793. | | 109.01 |
| THOUS CU M | | 9702. | 17681. | 18249. | | 14793. |
| | | | | | | 18249. |

◆ **AND**

STATION 1

| INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|------------|------------|----------------------|
| 4000. | 6000. | 10000. |
| | | 12000. |

18000. 20000.

Q. O. . . . O.

0.30 0.11

[illegible]

END

| STATION | INFLW(1),
OUTFLOW(2)
AND OBSERVED
FLOW(3) | 2000. | 4000. | 6000. | 8000. | 10000. | 12000. | 14000. | 16000. | 18000. | 20000. | 0. |
|---------|--|-------|-------|-------|-------|--------|--------|--------|--------|--------|--------|----|
| 0.1 | 1 | | | | | | | | | | | |
| 1 | 1 | | | | | | | | | | | |
| 2 | 1 | | | | | | | | | | | |
| 3 | 1 | | | | | | | | | | | |
| 4 | 1 | | | | | | | | | | | |
| 5 | 1 | | | | | | | | | | | |
| 6 | 1 | | | | | | | | | | | |
| 7 | 1 | | | | | | | | | | | |
| 8 | 1 | | | | | | | | | | | |
| 9 | 1 | | | | | | | | | | | |
| 10 | 1 | | | | | | | | | | | |
| 11 | 1 | | | | | | | | | | | |
| 12 | 1 | | | | | | | | | | | |
| 13 | 1 | | | | | | | | | | | |
| 14 | 1 | | | | | | | | | | | |
| 15 | 1 | | | | | | | | | | | |
| 16 | 1 | | | | | | | | | | | |
| 17 | 1 | | | | | | | | | | | |
| 18 | 1 | | | | | | | | | | | |
| 19 | 1 | | | | | | | | | | | |
| 20 | 1 | | | | | | | | | | | |
| 21 | 1 | | | | | | | | | | | |
| 22 | 1 | | | | | | | | | | | |
| 23 | 1 | | | | | | | | | | | |
| 24 | 1 | | | | | | | | | | | |
| 25 | 1 | | | | | | | | | | | |
| 26 | 1 | | | | | | | | | | | |
| 27 | 1 | | | | | | | | | | | |
| 28 | 1 | | | | | | | | | | | |
| 29 | 1 | | | | | | | | | | | |
| 30 | 1 | | | | | | | | | | | |
| 31 | 1 | | | | | | | | | | | |
| 32 | 1 | | | | | | | | | | | |
| 33 | 1 | | | | | | | | | | | |
| 34 | 1 | | | | | | | | | | | |
| 35 | 1 | | | | | | | | | | | |
| 36 | 1 | | | | | | | | | | | |
| 37 | 1 | | | | | | | | | | | |
| 38 | 1 | | | | | | | | | | | |
| 39 | 1 | | | | | | | | | | | |
| 40 | 1 | | | | | | | | | | | |
| 41 | 1 | | | | | | | | | | | |
| 42 | 1 | | | | | | | | | | | |
| 43 | 1 | | | | | | | | | | | |
| 44 | 1 | | | | | | | | | | | |
| 45 | 1 | | | | | | | | | | | |
| 46 | 1 | | | | | | | | | | | |
| 47 | 1 | | | | | | | | | | | |
| 48 | 1 | | | | | | | | | | | |
| 49 | 1 | | | | | | | | | | | |
| 50 | 1 | | | | | | | | | | | |
| 51 | 1 | | | | | | | | | | | |
| 52 | 1 | | | | | | | | | | | |
| 53 | 1 | | | | | | | | | | | |
| 54 | 1 | | | | | | | | | | | |
| 55 | 1 | | | | | | | | | | | |
| 56 | 1 | | | | | | | | | | | |
| 57 | 1 | | | | | | | | | | | |
| 58 | 1 | | | | | | | | | | | |
| 59 | 1 | | | | | | | | | | | |
| 60 | 1 | | | | | | | | | | | |
| 61 | 1 | | | | | | | | | | | |
| 62 | 1 | | | | | | | | | | | |
| 63 | 1 | | | | | | | | | | | |

441
00 451
00 461
00 471
00 481
00 491
00 501
00 511
00 521
00 531
00 541
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00 561
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00 791
00 801
00 811
00 821
00 831
00 841
00 851
00 861
00 871
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00 961
00 971
00 981
00 991
00 1001

FLAHERTY GIOVARA ASSOCIATES, P.C.

3 00102
3 30103
4 00104
4 30105
5 00106
5 30107
6 00108
6 30109
7 00110
7 30111
8 00112
8 30113
9 00114
9 30115
10 00116
10 30117
11 00118
11 30119
12 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO B | |
|-------------------------|------------|--------|---------|---------|--------------|
| 60 | 40 | 51 | 49 | 47 | 45 |
| 42 | 41 | 35 | 34 | 33 | 32 |
| 42 | 39 | 36 | 36 | 33 | 32 |
| 30 | 37 | 27 | 26 | 25 | 25 |
| 30 | 34 | 31 | 32 | 34 | 34 |
| 33 | 31 | 24 | 22 | 21 | 21 |
| 36 | 31 | 179 | 217 | 254 | 288 |
| 361 | 438 | 1272 | 1624 | 1779 | 2334 |
| 2793 | 3598 | 5617 | 6849 | 8414 | 10309 |
| 16083 | 20114 | 33122 | 33164 | 33143 | 33180 |
| 28311 | 27012 | 17184 | 15453 | 13900 | 12506 |
| 10103 | 21245 | 5909 | 5332 | 4888 | 4468 |
| 3793 | 7347 | 2811 | 2653 | 2526 | 2425 |
| | 3163 | | | | |
| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| | 33164 | 28325 | 12702 | 5328 | 632339 |
| | 939 | 802 | 363 | 151 | 18104 |
| | CFS | 4.07 | 7.43 | 7.66 | 7.66 |
| | CMS | 103.49 | 188.60 | 194.66 | 194.66 |
| | INCHES | 14046 | 25597 | 25419 | 25419 |
| | MM | 17325 | 31573 | 32587 | 32587 |
| | AC-FT | | | | |
| | THOUS CU M | | | | |

OVF

0 30
1 00
1 30
2 30
3 00

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

4000 8000 12000 16000 20000 24000 28000 32000 36000

0 11 21 31 41 51

17 00 86
18 30 87
19 00 88
20 30 89
21 00 90
22 30 91
23 00 92
24 30 93
25 00 94
26 30 95
27 00 96
28 30 97
29 00 98
30 30 99
31 00 00
32 30 01
33 00 02
34 30 03
35 00 04
36 30 05
37 00 06
38 30 07
39 00 08
40 30 09
41 00 10
42 30 11
43 00 12
44 30 13
45 00 14
46 30 15
47 00 16
48 30 17
49 00 18
50 30 19
51 00 20
52 30 21

DVN

***** SUB-AREA RUNOFF COMPUTATION *****
INFLOW HYDROGRAPH - SUBWATERBED NO. 6
ISTAG 1 ICOMP 0 IECON 0 ITAPE D JPLT 0 JPR7 0 INAME 1 ISTAGE 0 IAUTO 0
IHQDO 1 IUHQ 1 TAREA 10.33 SNAP 0.00 TRSDA 10.33 TRSPC 0.00 RATIO 0.000 IBNDW 0 ISAME 1 LOCAL 0
HYDROGRAPH DATA
PRECIP DATA
R6 86.00 R12 100.00 R24 112.00 R48 117.00 R72 0.00 R96 0.00
SPFE 0.00 PMS 17.30
TRSPC COMPUTED BY THE PROGRAM IS 0.801

LOSS DATA
 LROPT 0 STRKR 0.00 RTIOL 1.00 STRKS 0.00 RTIOL 1.00 ALSHX 0.00 RTIMP 0.02
 UNIT HYDROGRAPH DATA
 TP= 3.00 CP=0.63 NTA= 0

RECESION DATA
 STRIG= -2.00 GRCSN= -0.10 RTIOR= 1.50
 APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 6.86 AND R= 3.33 INTERVALS

UNIT HYDROGRAPH 32 END-OF-PERIOD ORDINATES, LAG= 2.97 HOURS, CP= 0.63 VOL= 1.00
 90 329 450 481 73 13
 701 329 450 481 73 13
 107 329 450 481 73 13
 16 329 450 481 73 13

| MO | DA | HR | MIN | PERIOD | RAIN | EXCS | LOSS | COMP | END-OF-PERIOD FLOW | MO | DA | HR | MIN | PERIOD | RAIN | EXCS | LOSS | COMP |
|----|----|----|-----|--------|------|------|------|--------|--------------------|----|----|----|-----|--------|------|------|------|--------|
| 1 | 1 | 0 | 30 | 1 | 0.00 | 0.00 | 0.00 | 1.54 | 0.02 | 1 | 1 | 0 | 30 | 1 | 0.00 | 0.00 | 0.00 | 1.54 |
| 1 | 1 | 1 | 30 | 2 | 0.00 | 0.00 | 0.00 | 1.98 | 0.02 | 1 | 1 | 1 | 30 | 2 | 0.00 | 0.00 | 0.00 | 1.98 |
| 1 | 1 | 2 | 30 | 3 | 0.00 | 0.00 | 0.00 | 2.77 | 0.02 | 1 | 1 | 2 | 30 | 3 | 0.00 | 0.00 | 0.00 | 2.77 |
| 1 | 1 | 3 | 30 | 4 | 0.00 | 0.00 | 0.00 | 4.00 | 0.02 | 1 | 1 | 3 | 30 | 4 | 0.00 | 0.00 | 0.00 | 4.00 |
| 1 | 1 | 4 | 30 | 5 | 0.00 | 0.00 | 0.00 | 5.53 | 0.02 | 1 | 1 | 4 | 30 | 5 | 0.00 | 0.00 | 0.00 | 5.53 |
| 1 | 1 | 5 | 30 | 6 | 0.00 | 0.00 | 0.00 | 8.91 | 0.02 | 1 | 1 | 5 | 30 | 6 | 0.00 | 0.00 | 0.00 | 8.91 |
| 1 | 1 | 6 | 30 | 7 | 0.00 | 0.00 | 0.00 | 10.39 | 0.02 | 1 | 1 | 6 | 30 | 7 | 0.00 | 0.00 | 0.00 | 10.39 |
| 1 | 1 | 7 | 30 | 8 | 0.00 | 0.00 | 0.00 | 11.61 | 0.02 | 1 | 1 | 7 | 30 | 8 | 0.00 | 0.00 | 0.00 | 11.61 |
| 1 | 1 | 8 | 30 | 9 | 0.00 | 0.00 | 0.00 | 12.63 | 0.02 | 1 | 1 | 8 | 30 | 9 | 0.00 | 0.00 | 0.00 | 12.63 |
| 1 | 1 | 9 | 30 | 10 | 0.00 | 0.00 | 0.00 | 13.47 | 0.02 | 1 | 1 | 9 | 30 | 10 | 0.00 | 0.00 | 0.00 | 13.47 |
| 1 | 1 | 10 | 30 | 11 | 0.00 | 0.00 | 0.00 | 14.16 | 0.02 | 1 | 1 | 10 | 30 | 11 | 0.00 | 0.00 | 0.00 | 14.16 |
| 1 | 1 | 11 | 30 | 12 | 0.00 | 0.00 | 0.00 | 15.17 | 0.02 | 1 | 1 | 11 | 30 | 12 | 0.00 | 0.00 | 0.00 | 15.17 |
| 1 | 1 | 12 | 30 | 13 | 0.00 | 0.00 | 0.00 | 17.24 | 0.02 | 1 | 1 | 12 | 30 | 13 | 0.00 | 0.00 | 0.00 | 17.24 |
| 1 | 1 | 13 | 30 | 14 | 0.00 | 0.00 | 0.00 | 20.91 | 0.02 | 1 | 1 | 13 | 30 | 14 | 0.00 | 0.00 | 0.00 | 20.91 |
| 1 | 1 | 14 | 30 | 15 | 0.00 | 0.00 | 0.00 | 26.48 | 0.02 | 1 | 1 | 14 | 30 | 15 | 0.00 | 0.00 | 0.00 | 26.48 |
| 1 | 1 | 15 | 30 | 16 | 0.00 | 0.00 | 0.00 | 33.94 | 0.02 | 1 | 1 | 15 | 30 | 16 | 0.00 | 0.00 | 0.00 | 33.94 |
| 1 | 1 | 16 | 30 | 17 | 0.00 | 0.00 | 0.00 | 42.99 | 0.02 | 1 | 1 | 16 | 30 | 17 | 0.00 | 0.00 | 0.00 | 42.99 |
| 1 | 1 | 17 | 30 | 18 | 0.00 | 0.00 | 0.00 | 53.14 | 0.02 | 1 | 1 | 17 | 30 | 18 | 0.00 | 0.00 | 0.00 | 53.14 |
| 1 | 1 | 18 | 30 | 19 | 0.00 | 0.00 | 0.00 | 66.20 | 0.02 | 1 | 1 | 18 | 30 | 19 | 0.00 | 0.00 | 0.00 | 66.20 |
| 1 | 1 | 19 | 30 | 20 | 0.00 | 0.00 | 0.00 | 83.09 | 0.02 | 1 | 1 | 19 | 30 | 20 | 0.00 | 0.00 | 0.00 | 83.09 |
| 1 | 1 | 20 | 30 | 21 | 0.00 | 0.00 | 0.00 | 101.39 | 0.02 | 1 | 1 | 20 | 30 | 21 | 0.00 | 0.00 | 0.00 | 101.39 |
| 1 | 1 | 21 | 30 | 22 | 0.00 | 0.00 | 0.00 | 118.73 | 0.02 | 1 | 1 | 21 | 30 | 22 | 0.00 | 0.00 | 0.00 | 118.73 |
| 1 | 1 | 22 | 30 | 23 | 0.00 | 0.00 | 0.00 | 132.07 | 0.02 | 1 | 1 | 22 | 30 | 23 | 0.00 | 0.00 | 0.00 | 132.07 |
| 1 | 1 | 23 | 30 | 24 | 0.00 | 0.00 | 0.00 | 137.49 | 0.02 | 1 | 1 | 23 | 30 | 24 | 0.00 | 0.00 | 0.00 | 137.49 |
| 1 | 1 | 24 | 30 | 25 | 0.00 | 0.00 | 0.00 | 138.32 | 0.02 | 1 | 1 | 24 | 30 | 25 | 0.00 | 0.00 | 0.00 | 138.32 |
| 1 | 1 | 25 | 30 | 26 | 0.00 | 0.00 | 0.00 | 115.00 | 0.02 | 1 | 1 | 25 | 30 | 26 | 0.00 | 0.00 | 0.00 | 115.00 |
| 1 | 1 | 26 | 30 | 27 | 0.00 | 0.00 | 0.00 | 84.29 | 0.02 | 1 | 1 | 26 | 30 | 27 | 0.00 | 0.00 | 0.00 | 84.29 |
| 1 | 1 | 27 | 30 | 28 | 0.00 | 0.00 | 0.00 | 72.94 | 0.02 | 1 | 1 | 27 | 30 | 28 | 0.00 | 0.00 | 0.00 | 72.94 |
| 1 | 1 | 28 | 30 | 29 | 0.00 | 0.00 | 0.00 | 61.84 | 0.02 | 1 | 1 | 28 | 30 | 29 | 0.00 | 0.00 | 0.00 | 61.84 |
| 1 | 1 | 29 | 30 | 30 | 0.00 | 0.00 | 0.00 | 43.93 | 0.02 | 1 | 1 | 29 | 30 | 30 | 0.00 | 0.00 | 0.00 | 43.93 |
| 1 | 1 | 30 | 30 | 31 | 0.00 | 0.00 | 0.00 | 37.19 | 0.02 | 1 | 1 | 30 | 30 | 31 | 0.00 | 0.00 | 0.00 | 37.19 |
| 1 | 1 | 31 | 30 | 32 | 0.00 | 0.00 | 0.00 | 23.35 | 0.02 | 1 | 1 | 31 | 30 | 32 | 0.00 | 0.00 | 0.00 | 23.35 |

FLAHERTY GIOVANA ASSOCIATES, P. C.

PAGE 0141

14 00 76
15 00 77
16 00 78
17 00 79
18 00 80
19 00 81
20 00 82
21 00 83
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43 00 105
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45 00 107
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52 00 114
53 00 115
54 00 116
55 00 117
56 00 118
57 00 119
58 00 120

DVM

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO 1

40000000 31

40000000 40

40000000 111

40000000 120

40000000 128

40000000 208

40000000 232

40000000 253

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|-------|--------|
| CF8 | 2777 | 2131 | 846 | 351 | | 42179 |
| CHS | 79 | 60 | 24 | 10 | | 1194 |
| INCHES | | 1.92 | 3.05 | 3.17 | | 3.17 |
| MM | | 48.74 | 77.37 | 80.40 | | 80.40 |
| AC-FT | | 1057 | 1678 | 1743 | | 1743 |
| CU-M | | 1503 | 2069 | 2150 | | 2150 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|-------|--------|---------|---------|--------|--------|
| CFB | 3471. | 2664. | 1057. | 439. | 52724. | 1493. |
| CMS | 98. | 75. | 30. | 12. | 3. | 96. |
| INCHES | | 2.40 | 9.673 | 3.96 | 100.50 | 100.50 |
| IN | | 60.93 | 96.73 | 100.50 | 3179. | 2179. |
| AC-FT | | 1321. | 2977. | 3179. | 2687. | 2687. |
| CU-M | | 1.59 | 2.987 | 2.687 | | |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|-------|--------|
| CFS | 3610 | 2770 | 1100 | 457 | 54833 | 1553 |
| CMB | 102 | 78 | 31 | 13 | 153 | 4.11 |
| INCHES | | 2.49 | 3.96 | 4.11 | | |
| MM | | 63.37 | 100.60 | 104.52 | | 104.52 |
| AC-FT | | 1374 | 2181 | 2266 | | 2266 |

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|--------|--------|---------|---------|--------------|
| CFS | 538 | 215 | 879 | 10949 |
| CMS | 642 | 215 | 879 | 2986 |
| INCHES | 197 | 60 | 25 | |
| | 4.80 | 7.62 | 7.91 | |
| INCHES | 121.86 | 193.46 | 200.99 | 200.99 |
| AC-FT | 2642 | 4194 | 4397 | 4397 |
| CU H | 3359 | 5173 | 5375 | 5375 |
| THOUS | | | | |

FLAHERTY GIAVARA ASSOCIATES, P. C.

33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111

8 30 177
9 30 181
10 30 201
11 30 221
12 30 241
13 30 261
14 30 281
15 30 301
16 30 321
17 30 341
18 30 361
19 30 381
20 30 401
21 30 421
22 30 441
23 30 461
24 30 481
25 30 501
26 30 521
27 30 541
28 30 561
29 30 581
30 30 601
31 30 621
32 30 641
33 30 661
34 30 681
35 30 701
36 30 721
37 30 741

PAGE 0150

FLAHERTY GIAVARA ASSOCIATES, P. C.

13 30 72
14 30 77
15 30 77
16 30 80
17 30 81
18 30 83
19 30 85
20 30 87
21 30 90
22 30 92
23 30 94
24 30 96
25 30 97
26 30 98
27 30 99
28 30 100
29 30 101
30 30 102
31 30 103
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33 30 105
34 30 106
35 30 107
36 30 108
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38 30 110
39 30 111
40 30 112
41 30 113
42 30 114
43 30 115
44 30 116
45 30 117
46 30 118
47 30 119
48 30 120

OVN

SUM OF 2 HYDROGRAPHS AT
35 33
36 24
37 17
38 19
39 17
40 20
41 18
42 16

PLAN 1 RTID 3
31 30
32 21
33 16
34 23
35 14
36 15
37 16
38 24
39 13
40 13
41 13
42 13

37 26
38 18
39 17
40 22

36 25
37 18
38 18
39 20

27 17
28 16
29 23
30 16

28 20
29 16
30 23
31 13

| | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 24. | 36. | 53. | 73. | 93. | 119. | 142. | 164. | 183. | 201. |
| 228. | 280. | 367. | 493. | 642. | 840. | 1077. | 1300. | 1516. | 1720. |
| 1704. | 2074. | 2266. | 2332. | 2787. | 3609. | 4444. | 5493. | 6742. | 8389. |
| 10323. | 12900. | 13231. | 17480. | 19217. | 20278. | 20381. | 20224. | 19350. | 18087. |
| 14418. | 15097. | 13601. | 12190. | 10910. | 9767. | 8748. | 7840. | 7028. | 6293. |
| 5631. | 5073. | 4988. | 4143. | 3738. | 3371. | 3048. | 2817. | 2587. | 2379. |
| 2217. | 2087. | 1971. | 1800. | 1737. | 1660. | 1570. | 1496. | 1437. | 1380. |

| | | | | |
|--------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 20581. | 17384. | 7806. | 3227. | 387290. |
| 583. | 492. | 226. | 97. | 107670. |
| | 2.75 | 3.57 | 4.00 | 4.00 |
| | 54.70 | 98.37 | 101.68 | 101.68 |
| | 8610. | 13484. | 16004. | 16004. |
| | 10621. | 19099. | 19740. | 19740. |

STATION

NOV*

| INFLW(1), | OUTFLOW(1) | AND OBSERVED FLOW(1) | STATION |
|-----------|------------|----------------------|---------|
| 2000. | 4000. | 6000. | 8000. |
| 10000. | 12000. | 14000. | 16000. |
| 18000. | 20000. | 22000. | 0. |

| | | | | | | | | | |
|------|------|------|------|------|------|------|------|------|------|
| 0.11 | 0.12 | 0.13 | 0.14 | 0.15 | 0.16 | 0.17 | 0.18 | 0.19 | 0.20 |
| 0.21 | 0.22 | 0.23 | 0.24 | 0.25 | 0.26 | 0.27 | 0.28 | 0.29 | 0.30 |
| 0.31 | 0.32 | 0.33 | 0.34 | 0.35 | 0.36 | 0.37 | 0.38 | 0.39 | 0.40 |
| 0.41 | 0.42 | 0.43 | 0.44 | 0.45 | 0.46 | 0.47 | 0.48 | 0.49 | 0.50 |
| 0.51 | 0.52 | 0.53 | 0.54 | 0.55 | 0.56 | 0.57 | 0.58 | 0.59 | 0.60 |
| 0.61 | 0.62 | 0.63 | 0.64 | 0.65 | 0.66 | 0.67 | 0.68 | 0.69 | 0.70 |
| 0.71 | 0.72 | 0.73 | 0.74 | 0.75 | 0.76 | 0.77 | 0.78 | 0.79 | 0.80 |
| 0.81 | 0.82 | 0.83 | 0.84 | 0.85 | 0.86 | 0.87 | 0.88 | 0.89 | 0.90 |
| 0.91 | 0.92 | 0.93 | 0.94 | 0.95 | 0.96 | 0.97 | 0.98 | 0.99 | 1.00 |

19 00 381
 19 30 39
 20 00 40
 20 30 41
 21 00 42
 21 30 43
 22 00 44
 22 30 45
 23 00 46
 23 30 47
 0 30 48
 1 00 49
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 22 30 92
 23 00 93
 23 30 94
 24 00 95

0 00 76
 1 00 78
 2 00 79
 3 00 80
 4 00 81
 5 00 82
 6 00 83
 7 00 84
 8 00 85
 9 00 86
 10 00 87
 11 00 88
 12 00 89

OVN

37
 26
 19
 18
 21
 37
 290
 2134
 1386
 1386
 1386
 2170

SUM OF 2 HYDROGRAPHS AT

33
 23
 17
 22
 17
 99
 487
 3102
 1738
 1328
 1382
 1824

PLAN 1

32
 22
 17
 23
 16
 123
 3748
 21038
 10143
 3200
 1724

NTIO 4

31
 22
 17
 24
 14
 147
 4415
 21373
 9087
 3187
 1630

TOTAL VOLUME

402183
 11387
 4 16
 103 54
 16617
 20499

STATION 1

CFB
 CMB
 INCHES
 AC-FT
 THOUS CU H

PEAK

21373
 605
 311
 230
 4 02
 102 16
 16074
 19833

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

OVF

STATION 1

CFB
 CMB
 INCHES
 AC-FT
 THOUS CU H

PEAK

21373
 605
 311
 230
 4 02
 102 16
 16074
 19833

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

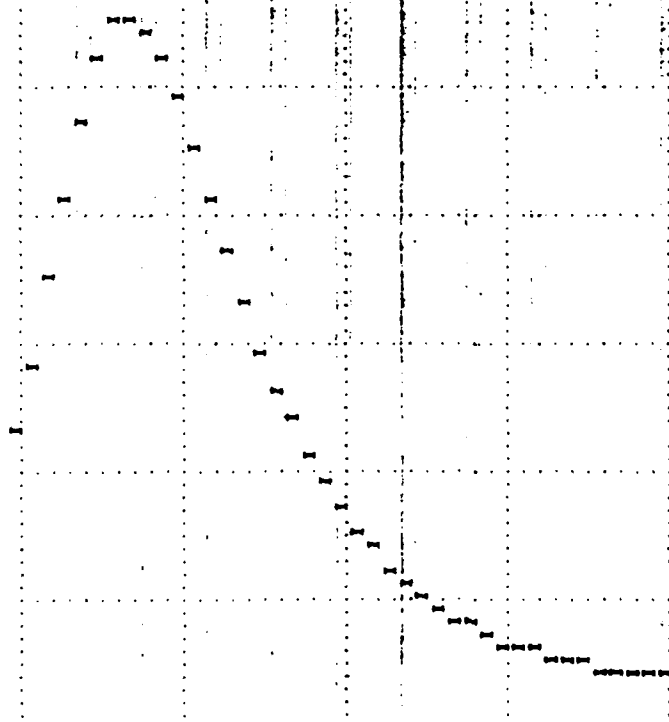
INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

INFLW(1),

OUTFLW(0) AND
 OBSERVED FLOW(1)

16 00 80
17 00 81
18 00 82
19 00 83
20 00 84
21 00 85
22 00 86
23 00 87
24 00 88
25 00 89
26 00 90
27 00 91
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53 00 117
54 00 118
55 00 119
56 00 120



50VNS

42 229
21 21
19 19
27 27
234 234
2126 2126
11736 11736
18536 18536

SUM OF 2 HYDROGRAPHS AT
37 37
26 26
17 17
21 21
31 31
59 59
410 410
2527 2527
17059 17059
15171 15171

PLAN 1
34 34
18 18
23 23
17 17
133 133
426 426
22618 22618
10894 10894

RTID 6
33 33
18 18
26 26
16 16
158 158
1202 1202
4956 4956
22956 22956
9758 9758

32 32
18 18
26 26
14 14
182 182
1447 1447
6127 6127
23538 23538
8745 8745

31 31
22 22
18 18
26 26
13 13
209 209
1671 1671
7520 7520
21583 21583
7839 7839

30 30
21 21
18 18
23 23
16 16
223 223
1918 1918
4357 4357
20174 20174
7022 7022

431
300441
222300451
222300461
222300471
2000481
000491
100501
130511
120521
230531
330541
400551
430561
530571
530581
60059
63060
73061
73062
83063
83064
93065
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100067
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110069
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120072
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150078
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180084
183085
190086
193087
200088
203089
210090
213091
220092
223093
230094
233095
240096
243097
250098
253099
260100

END

C-178

•ONE•

| STATION | 1 |
|------------|---------------------------------|
| INFLOW(I), | OUTFLOW(O) AND OBSERVED FLOW(*) |
| 0. | 4000. |
| | 6000. |
| | 8000. |
| | 10000. |
| | 12000. |
| | 14000. |
| | 16000. |
| | 18000. |
| | 20000. |
| | 22000. |
| | 24000. |

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00 118
00 119
00 120

END

♦♦♦

| STATION | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------|-------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|----------|
| INFLOW(I), | 8000. | 12000. | 16000. | 20000. | 24000. | 28000. | 32000. | 36000. | 40000. | 44000. | 48000. | 52000. | 56000. | 60000. | 64000. | 68000. | 72000. | 76000. | 80000. | 84000. | 88000. | 92000. | 96000. | 100000. | 104000. | 108000. | 112000. | 116000. | 120000. | 124000. | 128000. | 132000. | 136000. | 140000. | 144000. | 148000. | 152000. | 156000. | 160000. | 164000. | 168000. | 172000. | 176000. | 180000. | 184000. | 188000. | 192000. | 196000. | 200000. | 204000. | 208000. | 212000. | 216000. | 220000. | 224000. | 228000. | 232000. | 236000. | 240000. | 244000. | 248000. | 252000. | 256000. | 260000. | 264000. | 268000. | 272000. | 276000. | 280000. | 284000. | 288000. | 292000. | 296000. | 300000. | 304000. | 308000. | 312000. | 316000. | 320000. | 324000. | 328000. | 332000. | 336000. | 340000. | 344000. | 348000. | 352000. | 356000. | 360000. | 364000. | 368000. | 372000. | 376000. | 380000. | 384000. | 388000. | 392000. | 396000. | 400000. | 404000. | 408000. | 412000. | 416000. | 420000. | 424000. | 428000. | 432000. | 436000. | 440000. | 444000. | 448000. | 452000. | 456000. | 460000. | 464000. | 468000. | 472000. | 476000. | 480000. | 484000. | 488000. | 492000. | 496000. | 500000. | 504000. | 508000. | 512000. | 516000. | 520000. | 524000. | 528000. | 532000. | 536000. | 540000. | 544000. | 548000. | 552000. | 556000. | 560000. | 564000. | 568000. | 572000. | 576000. | 580000. | 584000. | 588000. | 592000. | 596000. | 600000. | 604000. | 608000. | 612000. | 616000. | 620000. | 624000. | 628000. | 632000. | 636000. | 640000. | 644000. | 648000. | 652000. | 656000. | 660000. | 664000. | 668000. | 672000. | 676000. | 680000. | 684000. | 688000. | 692000. | 696000. | 700000. | 704000. | 708000. | 712000. | 716000. | 720000. | 724000. | 728000. | 732000. | 736000. | 740000. | 744000. | 748000. | 752000. | 756000. | 760000. | 764000. | 768000. | 772000. | 776000. | 780000. | 784000. | 788000. | 792000. | 796000. | 800000. | 804000. | 808000. | 812000. | 816000. | 820000. | 824000. | 828000. | 832000. | 836000. | 840000. | 844000. | 848000. | 852000. | 856000. | 860000. | 864000. | 868000. | 872000. | 876000. | 880000. | 884000. | 888000. | 892000. | 896000. | 900000. | 904000. | 908000. | 912000. | 916000. | 920000. | 924000. | 928000. | 932000. | 936000. | 940000. | 944000. | 948000. | 952000. | 956000. | 960000. | 964000. | 968000. | 972000. | 976000. | 980000. | 984000. | 988000. | 992000. | 996000. | 1000000. |

PAGE 0165

FLAHERTY GIAVARA ASSOCIATES, P. C.

271
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54 30 119
55 30 120

OVN

| SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 9 | 110 | 106 | 102 |
|-------------------------|--------|--------|-----|-----|-----|
| 133 | 118 | 114 | 110 | 106 | 102 |
| 132 | 118 | 114 | 110 | 106 | 102 |
| 131 | 118 | 114 | 110 | 106 | 102 |
| 130 | 118 | 114 | 110 | 106 | 102 |
| 129 | 118 | 114 | 110 | 106 | 102 |
| 128 | 118 | 114 | 110 | 106 | 102 |
| 127 | 118 | 114 | 110 | 106 | 102 |
| 126 | 118 | 114 | 110 | 106 | 102 |
| 125 | 118 | 114 | 110 | 106 | 102 |
| 124 | 118 | 114 | 110 | 106 | 102 |
| 123 | 118 | 114 | 110 | 106 | 102 |
| 122 | 118 | 114 | 110 | 106 | 102 |
| 121 | 118 | 114 | 110 | 106 | 102 |
| 120 | 118 | 114 | 110 | 106 | 102 |
| 119 | 118 | 114 | 110 | 106 | 102 |
| 118 | 118 | 114 | 110 | 106 | 102 |
| 117 | 118 | 114 | 110 | 106 | 102 |
| 116 | 118 | 114 | 110 | 106 | 102 |
| 115 | 118 | 114 | 110 | 106 | 102 |
| 114 | 118 | 114 | 110 | 106 | 102 |
| 113 | 118 | 114 | 110 | 106 | 102 |
| 112 | 118 | 114 | 110 | 106 | 102 |
| 111 | 118 | 114 | 110 | 106 | 102 |
| 110 | 118 | 114 | 110 | 106 | 102 |
| 109 | 118 | 114 | 110 | 106 | 102 |
| 108 | 118 | 114 | 110 | 106 | 102 |
| 107 | 118 | 114 | 110 | 106 | 102 |
| 106 | 118 | 114 | 110 | 106 | 102 |
| 105 | 118 | 114 | 110 | 106 | 102 |
| 104 | 118 | 114 | 110 | 106 | 102 |
| 103 | 118 | 114 | 110 | 106 | 102 |
| 102 | 118 | 114 | 110 | 106 | 102 |
| 101 | 118 | 114 | 110 | 106 | 102 |
| 100 | 118 | 114 | 110 | 106 | 102 |
| 99 | 118 | 114 | 110 | 106 | 102 |
| 98 | 118 | 114 | 110 | 106 | 102 |
| 97 | 118 | 114 | 110 | 106 | 102 |
| 96 | 118 | 114 | 110 | 106 | 102 |
| 95 | 118 | 114 | 110 | 106 | 102 |
| 94 | 118 | 114 | 110 | 106 | 102 |
| 93 | 118 | 114 | 110 | 106 | 102 |
| 92 | 118 | 114 | 110 | 106 | 102 |
| 91 | 118 | 114 | 110 | 106 | 102 |
| 90 | 118 | 114 | 110 | 106 | 102 |
| 89 | 118 | 114 | 110 | 106 | 102 |
| 88 | 118 | 114 | 110 | 106 | 102 |
| 87 | 118 | 114 | 110 | 106 | 102 |
| 86 | 118 | 114 | 110 | 106 | 102 |
| 85 | 118 | 114 | 110 | 106 | 102 |
| 84 | 118 | 114 | 110 | 106 | 102 |
| 83 | 118 | 114 | 110 | 106 | 102 |
| 82 | 118 | 114 | 110 | 106 | 102 |
| 81 | 118 | 114 | 110 | 106 | 102 |
| 80 | 118 | 114 | 110 | 106 | 102 |
| 79 | 118 | 114 | 110 | 106 | 102 |
| 78 | 118 | 114 | 110 | 106 | 102 |
| 77 | 118 | 114 | 110 | 106 | 102 |
| 76 | 118 | 114 | 110 | 106 | 102 |
| 75 | 118 | 114 | 110 | 106 | 102 |
| 74 | 118 | 114 | 110 | 106 | 102 |
| 73 | 118 | 114 | 110 | 106 | 102 |
| 72 | 118 | 114 | 110 | 106 | 102 |
| 71 | 118 | 114 | 110 | 106 | 102 |
| 70 | 118 | 114 | 110 | 106 | 102 |
| 69 | 118 | 114 | 110 | 106 | 102 |
| 68 | 118 | 114 | 110 | 106 | 102 |
| 67 | 118 | 114 | 110 | 106 | 102 |
| 66 | 118 | 114 | 110 | 106 | 102 |
| 65 | 118 | 114 | 110 | 106 | 102 |
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| 62 | 118 | 114 | 110 | 106 | 102 |
| 61 | 118 | 114 | 110 | 106 | 102 |
| 60 | 118 | 114 | 110 | 106 | 102 |
| 59 | 118 | 114 | 110 | 106 | 102 |
| 58 | 118 | 114 | 110 | 106 | 102 |
| 57 | 118 | 114 | 110 | 106 | 102 |
| 56 | 118 | 114 | 110 | 106 | 102 |
| 55 | 118 | 114 | 110 | 106 | 102 |
| 54 | 118 | 114 | 110 | 106 | 102 |
| 53 | 118 | 114 | 110 | 106 | 102 |
| 52 | 118 | 114 | 110 | 106 | 102 |
| 51 | 118 | 114 | 110 | 106 | 102 |
| 50 | 118 | 114 | 110 | 106 | 102 |
| 49 | 118 | 114 | 110 | 106 | 102 |
| 48 | 118 | 114 | 110 | 106 | 102 |
| 47 | 118 | 114 | 110 | 106 | 102 |
| 46 | 118 | 114 | 110 | 106 | 102 |
| 45 | 118 | 114 | 110 | 106 | 102 |
| 44 | 118 | 114 | 110 | 106 | 102 |
| 43 | 118 | 114 | 110 | 106 | 102 |
| 42 | 118 | 114 | 110 | 106 | 102 |
| 41 | 118 | 114 | 110 | 106 | 102 |
| 40 | 118 | 114 | 110 | 106 | 102 |
| 39 | 118 | 114 | 110 | 106 | 102 |
| 38 | 118 | 114 | 110 | 106 | 102 |
| 37 | 118 | 114 | 110 | 106 | 102 |
| 36 | 118 | 114 | 110 | 106 | 102 |
| 35 | 118 | 114 | 110 | 106 | 102 |
| 34 | 118 | 114 | 110 | 106 | 102 |
| 33 | 118 | 114 | 110 | 106 | 102 |
| 32 | 118 | 114 | 110 | 106 | 102 |
| 31 | 118 | 114 | 110 | 106 | 102 |
| 30 | 118 | 114 | 110 | 106 | 102 |
| 29 | 118 | 114 | 110 | 106 | 102 |
| 28 | 118 | 114 | 110 | 106 | 102 |
| 27 | 118 | 114 | 110 | 106 | 102 |
| 26 | 118 | 114 | 110 | 106 | 102 |
| 25 | 118 | 114 | 110 | 106 | 102 |
| 24 | 118 | 114 | 110 | 106 | 102 |
| 23 | 118 | 114 | 110 | 106 | 102 |
| 22 | 118 | 114 | 110 | 106 | 102 |
| 21 | 118 | 114 | 110 | 106 | 102 |
| 20 | 118 | 114 | 110 | 106 | 102 |
| 19 | 118 | 114 | 110 | 106 | 102 |
| 18 | 118 | 114 | 110 | 106 | 102 |
| 17 | 118 | 114 | 110 | 106 | 102 |
| 16 | 118 | 114 | 110 | 106 | 102 |
| 15 | 118 | 114 | 110 | 106 | 102 |
| 14 | 118 | 114 | 110 | 106 | 102 |
| 13 | 118 | 114 | 110 | 106 | 102 |
| 12 | 118 | 114 | 110 | 106 | 102 |
| 11 | 118 | 114 | 110 | 106 | 102 |
| 10 | 118 | 114 | 110 | 106 | 102 |
| 9 | 118 | 114 | 110 | 106 | 102 |
| 8 | 118 | 114 | 110 | 106 | 102 |
| 7 | 118 | 114 | 110 | 106 | 102 |
| 6 | 118 | 114 | 110 | 106 | 102 |
| 5 | 118 | 114 | 110 | 106 | 102 |
| 4 | 118 | 114 | 110 | 106 | 102 |
| 3 | 118 | 114 | 110 | 106 | 102 |
| 2 | 118 | 114 | 110 | 106 | 102 |
| 1 | 118 | 114 | 110 | 106 | 102 |

CFS 79159 66786 30024 12413 TOTAL VOLUME 1489574

CMS
INCHES
MM
AC-FT
THOUS CU M

2242

1891
8 28
210.40
3317
40849

850
14.90
378.35
5952
73457

352
15.40
391.06
61353
75924

42180
15.40
391.06
61353
75924

OVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| 0 | 10000 | 20000 | 30000 | 40000 | 50000 | 60000 | 70000 | 80000 | 0 |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|---|
| 0 11 | | | | | | | | | 0 |
| 0 30 | | | | | | | | | 0 |
| 0 1 20 | | | | | | | | | 0 |
| 0 2 30 | | | | | | | | | 0 |
| 0 3 30 | | | | | | | | | 0 |
| 0 4 30 | | | | | | | | | 0 |
| 0 5 30 | | | | | | | | | 0 |
| 0 6 30 | | | | | | | | | 0 |
| 0 7 30 | | | | | | | | | 0 |
| 0 8 30 | | | | | | | | | 0 |
| 0 9 30 | | | | | | | | | 0 |
| 0 10 30 | | | | | | | | | 0 |
| 0 11 30 | | | | | | | | | 0 |
| 0 12 30 | | | | | | | | | 0 |
| 0 13 30 | | | | | | | | | 0 |
| 0 14 30 | | | | | | | | | 0 |
| 0 15 30 | | | | | | | | | 0 |
| 0 16 30 | | | | | | | | | 0 |
| 0 17 30 | | | | | | | | | 0 |
| 0 18 30 | | | | | | | | | 0 |
| 0 19 30 | | | | | | | | | 0 |
| 0 20 30 | | | | | | | | | 0 |
| 0 21 30 | | | | | | | | | 0 |
| 0 22 30 | | | | | | | | | 0 |
| 0 23 30 | | | | | | | | | 0 |
| 0 24 30 | | | | | | | | | 0 |
| 0 25 30 | | | | | | | | | 0 |
| 0 26 30 | | | | | | | | | 0 |
| 0 27 30 | | | | | | | | | 0 |
| 0 28 30 | | | | | | | | | 0 |
| 0 29 30 | | | | | | | | | 0 |
| 0 30 30 | | | | | | | | | 0 |
| 0 31 30 | | | | | | | | | 0 |
| 0 32 30 | | | | | | | | | 0 |
| 0 33 30 | | | | | | | | | 0 |
| 0 34 30 | | | | | | | | | 0 |
| 0 35 30 | | | | | | | | | 0 |
| 0 36 30 | | | | | | | | | 0 |
| 0 37 30 | | | | | | | | | 0 |
| 0 38 30 | | | | | | | | | 0 |
| 0 39 30 | | | | | | | | | 0 |
| 0 40 30 | | | | | | | | | 0 |
| 0 41 30 | | | | | | | | | 0 |
| 0 42 30 | | | | | | | | | 0 |
| 0 43 30 | | | | | | | | | 0 |
| 0 44 30 | | | | | | | | | 0 |
| 0 45 30 | | | | | | | | | 0 |
| 0 46 30 | | | | | | | | | 0 |
| 0 47 30 | | | | | | | | | 0 |

00 481
 00 30 501
 01 30 511
 12 30 521
 23 30 531
 33 30 541
 44 30 551
 55 30 561
 66 30 571
 77 30 581
 88 30 591
 99 30 601
 00 30 611
 11 30 621
 22 30 631
 33 30 641
 44 30 651
 55 30 661
 66 30 671
 77 30 681
 88 30 691
 99 30 701
 00 30 711
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 33 30 741
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 55 30 761
 66 30 771
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 88 30 791
 99 30 801
 00 30 811
 11 30 821
 22 30 831
 33 30 841
 44 30 851
 55 30 861
 66 30 871
 77 30 881
 88 30 891
 99 30 901
 00 30 911
 11 30 921
 22 30 931
 33 30 941
 44 30 951
 55 30 961
 66 30 971
 77 30 981
 88 30 991
 99 30 1001
 00 30 1011
 11 30 1021
 22 30 1031
 33 30 1041
 44 30 1051

FLAHERTY GIAVARA ASSOCIATES, P. C.

3 00106
4 00107
5 00108
6 00109
7 00110
8 00111
9 00112
10 00113
11 00114
12 00115
13 00116
14 00117
15 00118
16 00119
17 00120

OVNS

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH - SUBWATERSHED NO. 7 (OTSEGO LAKE)
ICOMP SECON I TAPE JFLT JPRT INAME IBSTAGE IAUFD

HYDQ IUHQ TAREA SNAP TRSDA TRSPC RATIO ISNOW ISAME LOCAL

PRECIP DATA R12 R24 R48 R72 R96
R12 R24 R48 R72 R96

TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA RTICK STRTL CNSTL ALBRI RTIMP
STRTG -2.00 GRCSN -0.10 RTIOR 1.50

UNIT HYDROGRAPH DATA
TP= 0.00 CP=0.63 NTA= 0

RECESSION DATA
STRTG -2.00 GRCSN -0.10 RTIOR 1.50

TC INCREASED TO TRMR OF 0.50
R INCREASED TO MINIMUM OF 0.5
CLARK DID NOT CONVERGE TO GIVEN SNYDER COEFFICIENTS
APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 1.00 AND R= 0.50 INTERVALS

UNIT HYDROGRAPH 2 END-OF-PERIOD ORIGINATES, LAG= 0.39 HOURS, CP= 0.50 VOL= 1.00
4115

MO DA HR MN PERIOD RAIN EXCS LOSS END-OF-PERIOD FLOW MO DA HR MN PERIOD RAIN EXCS LOSS COMP 0

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------------|-------|--------|---------|---------|-------|--------|
| CFS | 20764 | 8915 | 3306 | 1516 | 18191 | 3151 |
| CHB | 588 | 252 | 94 | 43 | | 22 |
| INCHES | | 19.28 | 13.10 | 22.10 | | 361.41 |
| MM | | 330.17 | 489.75 | 561.41 | | 961.41 |
| AC-FT | | 4421 | 6357 | 7517 | | 9517 |
| THOUS CU M | | 9453 | 8088 | 9272 | | 9272 |

STATION : 1

| INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|------------|------------|----------------------|
| 12000. | 16000. | 20000. |
| | | 24000. |

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PRECIP(L) AND EXCESS(X) . 0.
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[illegible]

C-188

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FLAHERTY GIAVARA ASSOCIATES, P. C.

19 00 381
20 00 391
21 00 401
22 00 411
23 00 421
24 00 431
25 00 441
26 00 451
27 00 461
28 00 471
29 00 481
30 00 491
31 00 501
32 00 511
33 00 521
34 00 531
35 00 541
36 00 551
37 00 561
38 00 571
39 00 581
40 00 591
41 00 601
42 00 611
43 00 621
44 00 631
45 00 641
46 00 651
47 00 661
48 00 671
49 00 681
50 00 691
51 00 701
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53 00 721
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69 00 881
70 00 891
71 00 901
72 00 911
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74 00 931
75 00 941
76 00 951

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8 00 112
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9 00 114
9 00 115
10 00 116
10 00 117
11 00 118
11 00 119
12 00 120

40VNS

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 1 | | TOTAL VOLUME | |
|-------------------|------------|----------------------|------------|--------------|------|
| 7 | 8 | 7 | 8 | 7 | 8 |
| 14 | 20 | 20 | 20 | 20 | 20 |
| 20 | 19 | 44 | 76 | 83 | 26 |
| 246 | 96 | 86 | 76 | 17 | 25 |
| 21 | 20 | 19 | 18 | 102 | 56 |
| 102 | 102 | 102 | 102 | 102 | 102 |
| 297 | 297 | 1202 | 1312 | 1639 | 1816 |
| 675 | 1093 | 1202 | 1312 | 1639 | 1816 |
| 1366 | 1202 | 677 | 407 | 375 | 360 |
| 1306 | 1294 | 283 | 271 | 290 | 240 |
| 204 | 196 | 188 | 181 | 167 | 160 |
| 136 | 131 | 126 | 121 | 111 | 107 |
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | |
| 4153 | 1783 | 611 | 303 | 36382 | |
| 118 | 50 | 19 | 7 | 1030 | |
| CFS | CMH | CMH | CMH | 4.42 | |
| INCHES | INCHES | INCHES | INCHES | 112.38 | |
| AC-FT | AC-FT | AC-FT | AC-FT | 1503 | |
| THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M | 1854 | |
| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 2 | | | |
| 7 | 8 | 7 | 8 | | |
| 11 | 11 | 11 | 10 | 10 | 10 |
| 10 | 10 | 23 | 23 | 103 | 129 |
| 24 | 24 | 86 | 93 | 116 | 129 |
| 307 | 307 | 107 | | 131 | |

[illegible]

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|-------|--------|
| CFB | 3171 | 2229 | 827 | 379 | | 45478 |
| CMS | 147 | 63 | 23 | 11 | | 1288 |
| INCHES | | 3.25 | 4.82 | 5.52 | | 5.52 |
| MM | | 82.54 | 122.44 | 140.35 | | 140.35 |
| CU-FT | | 1639 | 1639 | 1877 | | 1877 |
| THOUS | | 1363 | 2022 | 2318 | | 2318 |

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 3 | |
|-------------------|------|----------------------|------|
| 7 | 11 | 11 | 11 |
| 10 | 10 | 26 | 26 |
| 26 | 23 | 58 | 90 |
| 149 | 319 | 125 | 98 |
| 27 | 27 | 125 | 22 |
| 133 | 133 | 132 | 132 |
| 386 | 386 | 386 | 386 |
| 1421 | 1421 | 1705 | 2131 |
| 386 | 903 | 1563 | 508 |
| 1776 | 1776 | 881 | 488 |
| 378 | 383 | 225 | 225 |
| 266 | 255 | 245 | 226 |
| 177 | 170 | 157 | 151 |
| 184 | 184 | 145 | 137 |
| 192 | 192 | 145 | 137 |
| 3288 | 3288 | 217 | 208 |
| 432 | 415 | 232 | 232 |
| 998 | 989 | 225 | 225 |
| 386 | 386 | 2131 | 508 |
| 259 | 259 | 386 | 386 |
| 133 | 133 | 132 | 132 |
| 127 | 127 | 125 | 98 |
| 28 | 28 | 125 | 22 |
| 338 | 338 | 125 | 22 |
| 23 | 23 | 58 | 90 |
| 10 | 10 | 26 | 26 |
| 7 | 7 | 11 | 11 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|-------|--------|
| CFB | 3399 | 318 | 860 | 394 | | 47297 |
| CMB | 153 | 66 | 24 | 11 | | 1339 |
| INCHES | | 3.38 | 5.01 | 5.75 | | 5.75 |
| MM | | 85.84 | 127.33 | 145.97 | | 145.97 |
| AC-FT | | 1149 | 1703 | 1954 | | 1954 |
| CU M | | 1418 | 2103 | 2411 | | 2411 |

[illegible]

MM
AC-FT
THOUS CU M

561.41
7517
9272

61.41
7517.
9272.

489.74
6357.
8088.

COMBINE HYDROGRAPHS

| COMBINE | 2 | INFLW | HYDROGRAPHS | IECON | ITAPE... | JPLT | JPRIT | INAME | ISTAGE | IAUTO |
|---------|---|-------|-------------|-------|----------|------|-------|-------|--------|-------|
| ISTAG | 1 | ICOMP | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 |

[illegible]

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------------|------|--------|---------|---------|-------|--------|
| CF8 | 1523 | 1066 | 641 | 2786 | 33297 | 3.18 |
| CM8 | 459 | 398 | 188 | 79 | 9466 | 3.18 |
| INCHES | | 1.61 | 3.04 | 3.18 | | 60.88 |
| MM | | 40.84 | 77.12 | 80.88 | | 13814 |
| AC-FT | | 6975 | 13172 | 13814 | | 17039 |
| THOUS CU M | | 8604 | 15247 | 17039 | | |

#OVF#

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| | | | | | | | | | | | | | | | |
|----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|-----|----|
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |
| 30 | 00 | 130 | 00 | 230 | 00 | 330 | 00 | 430 | 00 | 530 | 00 | 630 | 00 | 730 | 00 |
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 |

141
 00 171
 8 30 181
 9 30 191
 10 30 201
 11 30 211
 12 30 221
 13 30 231
 14 30 241
 15 30 251
 16 30 261
 17 30 271
 18 30 281
 19 30 291
 20 30 301
 21 30 311
 22 30 321
 23 30 331
 24 30 341
 25 30 351
 26 30 361
 27 30 371
 28 30 381
 29 30 391
 30 30 401
 31 30 411
 32 30 421
 33 30 431
 34 30 441
 35 30 451
 36 30 461
 37 30 471
 38 30 481
 39 30 491
 40 30 501
 41 30 511
 42 30 521
 43 30 531
 44 30 541
 45 30 551
 46 30 561
 47 30 571
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 58 30 681
 59 30 691
 60 30 701
 61 30 711
 62 30 721
 63 30 731
 64 30 741
 65 30 751
 66 30 761
 67 30 771
 68 30 781
 69 30 791
 70 30 801
 71 30 811
 72 30 821
 73 30 831
 74 30 841
 75 30 851
 76 30 861
 77 30 871
 78 30 881
 79 30 891
 80 30 901
 81 30 911
 82 30 921
 83 30 931
 84 30 941
 85 30 951
 86 30 961
 87 30 971
 88 30 981
 89 30 991
 90 30 1001
 91 30 1011
 92 30 1021
 93 30 1031
 94 30 1041
 95 30 1051
 96 30 1061
 97 30 1071
 98 30 1081
 99 30 1091
 100 30 1101

00 74.
13 30 75.
14 00 76.
15 30 77.
16 00 78.
17 30 79.
18 00 80.
19 30 81.
20 00 82.
21 30 83.
22 00 84.
23 30 85.
24 00 86.
25 30 87.
26 00 88.
27 30 89.
28 00 90.
29 30 91.
30 00 92.
31 30 93.
32 00 94.
33 30 95.
34 00 96.
35 30 97.
36 00 98.
37 30 99.
38 00 100.
39 30 101.
40 00 102.
41 30 103.
42 00 104.
43 30 105.
44 00 106.
45 30 107.
46 00 108.
47 30 109.
48 00 110.
49 30 111.
50 00 112.
51 30 113.
52 00 114.
53 30 115.
54 00 116.
55 30 117.
56 00 118.
57 30 119.
58 00 120.

DWN

| SUM OF 2 HYDROGRAPHS AT | 1 PLAN 1 | RTIO 2 | 36 |
|-------------------------|----------|--------|-----|
| 43 | 40 | 39 | 43 |
| 34 | 45 | 45 | 43 |
| 42 | 102 | 110 | 147 |
| 342 | 116 | 176 | 151 |

| | 49. | 47. | 44. | 42. | 40. | 38. | 36. | 34. | 83. | 143. |
|------------|-------|--------|---------|---------|--------------|-------|-------|-------|-------|-------|
| 190 | 162 | 178 | 198 | 219 | 219 | 219 | 264 | 285 | 304 | 321 |
| 468 | 640 | 724 | 847 | 1007 | 1007 | 1198 | 1264 | 1620 | 1828 | 2024 |
| 2004 | 2345 | 3047 | 3820 | 4375 | 4375 | 5110 | 6117 | 7331 | 7857 | 13257 |
| 3020 | 3410 | 4010 | 4810 | 5324 | 5324 | 20007 | 20276 | 19915 | 17037 | 17824 |
| 4374 | 4918 | 5441 | 6289 | 7085 | 7085 | 3730 | 8738 | 7852 | 7038 | 6342 |
| 5691 | 6457 | 7145 | 8227 | 9343 | 9343 | 3467 | 3168 | 2917 | 2698 | 2479 |
| 7371 | 8457 | 9345 | 10752 | 12464 | 12464 | 1747 | 1694 | 1578 | 1515 | 1455 |
| 2316 | 2188 | 2065 | 1952 | 1846 | 1846 | 1747 | 1694 | 1578 | 1515 | 1455 |
| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | | | |
| CFB | 20276 | 17583 | 8501 | 3482 | 417872 | | | | | |
| CHS | 498 | 235 | 99 | | 11832 | | | | | |
| INCHES | 574 | 235 | 99 | | | | | | | |
| MM | 21.01 | 9.41 | 3.90 | | 3.98 | | | | | |
| AC-FT | 51.05 | 96.41 | 101.10 | | 101.10 | | | | | |
| CU-FT | 8719 | 16465 | 17267 | | 17267 | | | | | |
| THOUS CU M | 10754 | 20309 | 21299 | | 21299 | | | | | |

•DVF•

STATION 1

INFLW(1), OUTFLOW(0) AND OBSERVED FLOW(0)

0-112741951789101112131415161718192021222324252627282930313233343536373839404142434445464748495051525354555657585960616263646566676869707172737475767778798081828384858687888990919293949596979899

PAGE 0181

FLAHERTY GIAVARA ASSOCIATES, P. C.

18 30 371
19 30 381
20 30 391
21 30 401
22 30 411
23 30 421
24 30 431
25 30 441
26 30 451
27 30 461
28 30 471
29 30 481
30 30 491
31 30 501
32 30 511
33 30 521
34 30 531
35 30 541
36 30 551
37 30 561
38 30 571
39 30 581
40 30 591
41 30 601
42 30 611
43 30 621
44 30 631
45 30 641
46 30 651
47 30 661
48 30 671
49 30 681
50 30 691
51 30 701
52 30 711
53 30 721
54 30 731
55 30 741
56 30 751
57 30 761
58 30 771
59 30 781
60 30 791
61 30 801
62 30 811
63 30 821
64 30 831
65 30 841
66 30 851
67 30 861
68 30 871
69 30 881
70 30 891
71 30 901
72 30 911
73 30 921
74 30 931
75 30 941

23 30 95
0 00 96
0 30 97
1 00 98
1 30 99
2 00 100
2 30 101
3 00 102
4 00 103
4 30 104
5 00 105
5 30 106
6 00 107
6 30 108
7 00 109
7 30 110
8 00 111
8 30 112
9 00 113
9 30 114
10 00 115
10 30 116
11 00 117
11 30 118
12 00 119
12 30 120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTID 3 | |
|-------------------------|-------|---------|-------|--------------|-------|
| 47 | 43 | 42 | 40 | 39 | 37 |
| 45 | 44 | 47 | 46 | 46 | 45 |
| 36 | 42 | 106 | 115 | 124 | 150 |
| 44 | 43 | 121 | 133 | 137 | 153 |
| 169 | 338 | 149 | 179 | 157 | 193 |
| 51 | 46 | 44 | 37 | 35 | 149 |
| 156 | 185 | 203 | 274 | 296 | 334 |
| 487 | 753 | 881 | 1463 | 1685 | 2105 |
| 169 | 209 | 251 | 274 | 1902 | 2105 |
| 645 | 1048 | 1246 | 1463 | 1902 | 2105 |
| 2272 | 3973 | 5314 | 6362 | 7624 | 13787 |
| 14889 | 19043 | 20807 | 21089 | 20712 | 18537 |
| 15621 | 17067 | 20097 | 21089 | 19819 | 18537 |
| 17050 | 12372 | 11277 | 9087 | 7340 | 6595 |
| 5919 | 4398 | 3606 | 3295 | 2795 | 2579 |
| 2409 | 2148 | 1817 | 1721 | 1576 | 1513 |
| PEAK | | 72-HOUR | | TOTAL VOLUME | |
| 21089 | | 3622 | | 434587 | |
| CFS | | 8633 | | 12304 | |
| CFS | | 244 | | 414 | |
| INCHES | | 3.95 | | 103.13 | |
| AC-FT | | 100.26 | | 17958 | |
| THOUS CU H | | 21122 | | 22151 | |

OVF

STATION 1

INFLW(1), OUTFLOW(0) AND OBSERVED FLOW(9)

FLAHERTY DIAVARA ASSOCIATES, P. C.

[illegible]

58. 1
00 59
30 60
40 61
50 62
60 63
70 64
80 65
90 66
100 67
110 68
120 69
130 70
140 71
150 72
160 73
170 74
180 75
190 76
200 77
210 78
220 79
230 80
240 81
250 82
260 83
270 84
280 85
290 86
300 87
310 88
320 89
330 90
340 91
350 92
360 93
370 94
380 95
390 96
400 97
410 98
420 99
430 100
440 101
450 102
460 103
470 104
480 105
490 106
500 107
510 108
520 109
530 110
540 111
550 112
560 113
570 114
580 115

10. 00116.
10. 30117.
11. 00118.
11. 30119.
12. 00120.

END

[illegible]

ONE *

STATION 1

[illegible]

FLAHERTY GIOVARA ASSOCIATES, P. C.

15 00 80
16 00 81
17 00 82
18 00 83
19 00 84
20 00 85
21 00 86
22 00 87
23 00 88
24 00 89
25 00 90
26 00 91
27 00 92
28 00 93
29 00 94
30 00 95
31 00 96
32 00 97
33 00 98
34 00 99
35 00 100
36 00 101
37 00 102
38 00 103
39 00 104
40 00 105
41 00 106
42 00 107
43 00 108
44 00 109
45 00 110
46 00 111
47 00 112
48 00 113
49 00 114
50 00 115
51 00 116
52 00 117
53 00 118
54 00 119
55 00 120

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | MTIO 5 |
|-------------------------|-------|--------|--------|
| 49 | 46 | 43 | 44 |
| 45 | 33 | 31 | 50 |
| 46 | 80 | 114 | 124 |
| 364 | 143 | 130 | 153 |
| 50 | 47 | 42 | 40 |
| 197 | 244 | 271 | 235 |
| 811 | 1128 | 1342 | 1574 |
| 3413 | 4900 | 3723 | 4831 |
| 18380 | 20508 | 22408 | 22712 |
| 51 | 48 | 42 | 40 |
| 38 | 33 | 49 | 48 |
| 47 | 46 | 133 | 162 |
| 383 | 156 | 61 | 157 |
| 52 | 47 | 92 | 160 |
| 182 | 244 | 319 | 360 |
| 716 | 1128 | 1815 | 2267 |
| 2649 | 4900 | 8211 | 14848 |
| 16034 | 21643 | 21344 | 19962 |

DVN

18362 16708 13077 13540 12143 10898 9786 8794 7903 7103
 6374 5763 5227 4737 4289 3883 3548 3267 3010 2777
 2594 2449 2313 2186 2068 1957 1833 1767 1697 1630

CFB PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
 22712 19692 9297 3900 448016
 643 538 263 110 13253
 INCHES 2.25 4.25 4.46
 37.18 107.77 132.24
 AC-FT 18441 13340
 THOUS CU M 12043 22746 23855

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(=)

4000 9000 12000 15000 20000 24000
 0.11 0.30 1.11 2.11 3.11 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 0.30 1.11 2.11 3.11 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 1.11 2.11 3.11 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 2.11 3.11 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 3.11 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 4.11 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 5.11 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 6.11 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 7.11 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 8.11 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 9.11 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 10.11 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 11.11 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 12.11 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 13.11 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 14.11 15.11 16.11 17.11 18.11 19.11 20.11
 15.11 16.11 17.11 18.11 19.11 20.11
 16.11 17.11 18.11 19.11 20.11
 17.11 18.11 19.11 20.11
 18.11 19.11 20.11
 19.11 20.11
 20.11

FLAHERTY GIOVANA ASSOCIATES, P.C.

00100
00101
00102
00103
00104
00105
00106
00107
00108
00109
00110
00111
00112
00113
00114
00115
00116
00117
00118
00119
00120

DVN

PLAN 1 RTIO 6

SUM OF 2 HYDROGRAPHS AT

| | | | | | | |
|------|------|------|------|------|------|------|
| 50 | 53 | 49 | 48 | 44 | 42 | 41 |
| 40 | 39 | 47 | 46 | 43 | 40 | 39 |
| 48 | 48 | 47 | 46 | 43 | 40 | 39 |
| 184 | 397 | 162 | 148 | 133 | 118 | 103 |
| 187 | 397 | 162 | 148 | 133 | 118 | 103 |
| 175 | 397 | 162 | 148 | 133 | 118 | 103 |
| 343 | 840 | 431 | 403 | 370 | 330 | 300 |
| 252 | 742 | 431 | 403 | 370 | 330 | 300 |
| 1723 | 2744 | 1400 | 1240 | 1013 | 818 | 618 |
| 1607 | 1607 | 1400 | 1240 | 1013 | 818 | 618 |
| 1607 | 1607 | 1400 | 1240 | 1013 | 818 | 618 |
| 1607 | 1607 | 1400 | 1240 | 1013 | 818 | 618 |
| 2887 | 2887 | 2264 | 2142 | 1919 | 1738 | 1588 |

TOTAL VOLUME

| | | |
|--------|-------|--------|
| 484731 | 13726 | 4.62 |
| 13726 | 4.62 | 117.28 |
| 20030 | 24707 | |

6-HOUR

| | | |
|-------|-------|--------|
| 20396 | 927 | 4037 |
| 578 | 273 | 4.62 |
| 2.33 | 11.83 | 117.28 |
| 39.22 | 1509 | 20030 |
| 12475 | 23559 | 24707 |

PEAK

| | | |
|-------|-----|--|
| 23523 | 666 | |
| 666 | | |

CFS

| | | |
|-------|--|--|
| 23523 | | |
|-------|--|--|

INCHES

| | | |
|-------|--|--|
| 23523 | | |
|-------|--|--|

AC-FT

| | | |
|-------|--|--|
| 23523 | | |
|-------|--|--|

THOUS CU M

| | | |
|-------|--|--|
| 23523 | | |
|-------|--|--|

STATION 1

INFLOW(1), OUTFLOW(1) AND OBSERVED FLOW(1)

0.30
1.00
1.30
2.00

4000

8000

12000

16000

20000

24000

28000

32000

36000

40000

44000

48000

7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120

261
0030271
1330281
1430291
1530301
1630311
1730321
1830331
1930341
2030351
2130361
2230371
2330381
2430391
2530401
2630411
2730421
2830431
2930441
3030451
3130461
3230471
3330481
3430491
3530501
3630511
3730521
3830531
3930541
4030551
4130561
4230571
4330581
4430591
4530601
4630611
4730621
4830631
4930641
5030651
5130661
5230671
5330681
5430691
5530701
5630711
5730721
5830731
5930741
6030751
6130761
6230771
6330781
6430791
6530801
6630811
6730821
6830831
6930841
7030851
7130861
7230871
7330881
7430891
7530901
7630911
7730921
7830931
7930941
8030951
8130961
8230971
8330981
8430991
8531001

18 00 84
19 00 85
20 00 86
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27 00 93
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29 00 95
30 00 96
31 00 97
32 00 98
33 00 99
34 00 00
35 00 01
36 00 02
37 00 03
38 00 04
39 00 05
40 00 06
41 00 07
42 00 08
43 00 09
44 00 10
45 00 11
46 00 12
47 00 13
48 00 14
49 00 15
50 00 16
51 00 17
52 00 18
53 00 19
54 00 20

C-212

DYN

| SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 8 | 72-HOUR | 24-HOUR | 6-HOUR | PEAK | TOTAL VOLUME |
|-------------------------|--------|--------|---------|---------|--------|-------|--------------|
| 84 | 80 | 78 | 73 | 73 | 71 | 71 | 2910 |
| 47 | 81 | 89 | 88 | 87 | 86 | 86 | 4048 |
| 83 | 82 | 88 | 88 | 87 | 86 | 86 | 32514 |
| 483 | 204 | 231 | 238 | 243 | 289 | 289 | 12883 |
| 318 | 232 | 152 | 109 | 104 | 102 | 102 | 4759 |
| 388 | 232 | 171 | 157 | 159 | 287 | 287 | 3030 |
| 301 | 453 | 527 | 549 | 408 | 442 | 442 | 3576 |
| 323 | 453 | 527 | 549 | 408 | 442 | 442 | 3576 |
| 1438 | 2396 | 2814 | 3241 | 3457 | 4048 | 4048 | 3030 |
| 1674 | 2396 | 2814 | 3241 | 3457 | 4048 | 4048 | 3030 |
| 7640 | 10220 | 12314 | 14442 | 17507 | 20514 | 20514 | 3030 |
| 36621 | 49014 | 42337 | 39832 | 38113 | 32583 | 32583 | 3030 |
| 24178 | 19480 | 17475 | 15703 | 14116 | 12883 | 12883 | 3030 |
| 8459 | 6734 | 6336 | 5834 | 5376 | 4759 | 4759 | 3030 |
| 3904 | 3494 | 3309 | 3156 | 3030 | 2910 | 2910 | 3030 |
| 4131 | | | | | | | |

835743.
23666.
7.96
202.21
34535
42598

6765.
197.
7.96
202.21
34535
42598

16602.
470.
7.59
192.81
32930.
40618.

35166.
996.
4.02
102.10
17438
21309.

40557.
1148.

CFB
CMS
INCHES
MM
AC-FT
THOUS CU M

DVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

4000 8000 12000 16000 20000 24000 28000 32000 36000 40000 44000 0

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45

23 30 471
0 30 481
1 30 491
2 30 501
3 30 511
4 30 521
5 30 531
6 30 541
7 30 551
8 30 561
9 30 571
10 30 581
11 30 591
12 30 601
13 30 611
14 30 621
15 30 631
16 30 641
17 30 651
18 30 661
19 30 671
20 30 681
21 30 691
22 30 701
23 30 711
24 30 721
25 30 731
26 30 741
27 30 751
28 30 761
29 30 771
30 30 781
31 30 791
32 30 801
33 30 811
34 30 821
35 30 831
36 30 841
37 30 851
38 30 861
39 30 871
40 30 881
41 30 891
42 30 901
43 30 911
44 30 921
45 30 931
46 30 941
47 30 951
48 30 961
49 30 971
50 30 981
51 30 991
52 30 1001
53 30 1011
54 30 1021
55 30 1031
56 30 1041

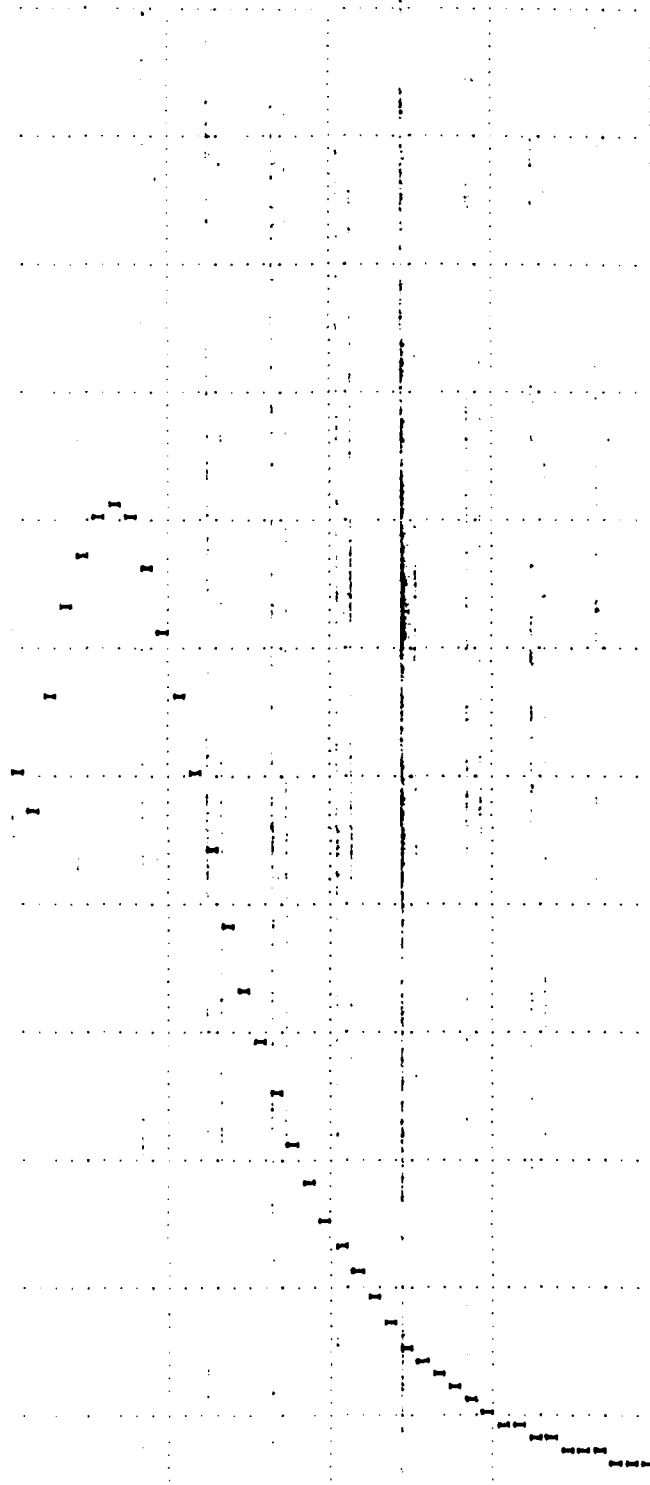
101 00 30 40 50 60 70 80 90 100 110 120 130 140 150 160 170 180 190 200 210 220 230 240 250 260 270 280 290 300 310 320 330 340 350 360 370 380 390 400 410 420 430 440 450 460 470 480 490 500 510 520 530 540 550 560 570 580 590 600 610 620 630 640 650 660 670

10 00 68
10 30 69
11 00 70
11 30 71
12 00 72
12 30 73
13 00 74
13 30 75
14 00 76
14 30 77
15 00 78
15 30 79
16 00 80
16 30 81
17 00 82
17 30 83
18 00 84
18 30 85
19 00 86
19 30 87
20 00 88
20 30 89
21 00 90
21 30 91
22 00 92
22 30 93
23 00 94
23 30 95
24 00 96
24 30 97
25 00 98
25 30 99
26 00 00
26 30 01
27 00 02
27 30 03
28 00 04
28 30 05
29 00 06
29 30 07
30 00 08
30 30 09
31 00 10
31 30 11
32 00 12
32 30 13
33 00 14
33 30 15
34 00 16
34 30 17
35 00 18
35 30 19
36 00 20

DYN

11 30 231
 12 30 241
 13 30 251
 14 30 261
 15 30 271
 16 30 281
 17 30 290
 18 30 300
 19 30 310
 20 30 320
 21 30 330
 22 30 340
 23 30 350
 24 30 361
 25 30 371
 26 30 381
 27 30 391
 28 30 401
 29 30 411
 30 30 421
 31 30 431
 32 30 441
 33 30 451
 34 30 461
 35 30 471
 36 30 481
 37 30 491
 38 30 501
 39 30 510
 40 30 520
 41 30 530
 42 30 540
 43 30 550
 44 30 560
 45 30 570
 46 30 580
 47 30 590
 48 30 600
 49 30 610
 50 30 620
 51 30 630
 52 30 640
 53 30 650
 54 30 660
 55 30 670
 56 30 680
 57 30 690
 58 30 700
 59 30 710
 60 30 720
 61 30 730
 62 30 740
 63 30 750
 64 30 760
 65 30 770
 66 30 780
 67 30 790
 68 30 800

16 30 810
 17 30 820
 18 30 830
 19 30 840
 20 30 850
 21 30 860
 22 30 870
 23 30 880
 24 30 890
 25 30 900
 26 30 910
 27 30 920
 28 30 930
 29 30 940
 30 30 950
 31 30 960
 32 30 970
 33 30 980
 34 30 990
 35 30 1000
 36 30 1010
 37 30 1020
 38 30 1030
 39 30 1040
 40 30 1050
 41 30 1060
 42 30 1070
 43 30 1080
 44 30 1090
 45 30 1100
 46 30 1110
 47 30 1120
 48 30 1130
 49 30 1140
 50 30 1150
 51 30 1160
 52 30 1170
 53 30 1180
 54 30 1190
 55 30 1200



DYN

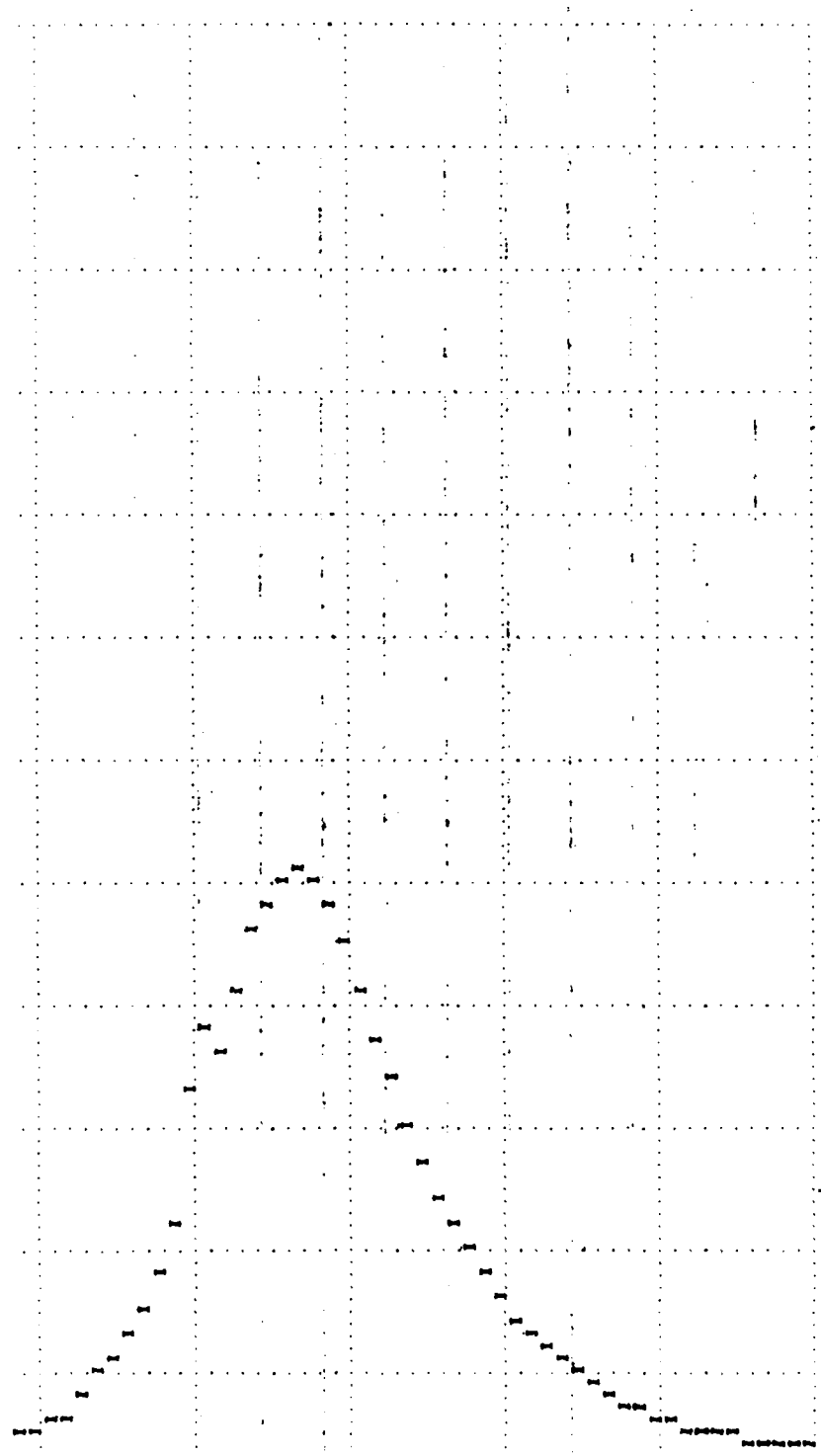
STATION 1, PLAN 1, RATIO 2
 END-OF-PERIOD HYDROGRAPH ORDINATES

OUTFLOW

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 000000000
 000000000
 000000000
 000000000
 000000000
 000000000
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 000000000
 000000000
 000000000
 000000000

FLAHERTY GIAVARA ASSOCIATES, P. C.

10 30 690
11 30 710
12 30 720
13 30 730
14 30 740
15 30 750
16 30 760
17 30 770
18 30 780
19 30 790
20 30 800
21 30 810
22 30 820
23 30 830
24 30 840
25 30 850
26 30 860
27 30 870
28 30 880
29 30 890
30 30 900
31 30 910
32 30 920
33 30 930
34 30 940
35 30 950
36 30 960
37 30 970
38 30 980
39 30 990
40 30 1000
41 30 1010
42 30 1020
43 30 1030
44 30 1040
45 30 1050
46 30 1060
47 30 1070
48 30 1080
49 30 1090
50 30 1100
51 30 1110
52 30 1120
53 30 1130
54 30 1140
55 30 1150
56 30 1160
57 30 1170
58 30 1180
59 30 1190
60 30 1200



STATION 1. PLAN 1. RATIO 3

DNW

| | 4000 | 8000 | 12000 | 16000 | 20000 | 24000 | INFLOW(I) | OUTFLOW(O) | AND OBSERVED FLOW(I*) |
|-----|------|------|-------|-------|-------|-------|-----------|------------|-----------------------|
| 0 | 1 | 1 | 1 | 1 | 1 | 1 | 0 | 0 | 0 |
| 1 | 2 | 2 | 2 | 2 | 2 | 2 | 1 | 1 | 1 |
| 2 | 3 | 3 | 3 | 3 | 3 | 3 | 2 | 2 | 2 |
| 3 | 4 | 4 | 4 | 4 | 4 | 4 | 3 | 3 | 3 |
| 4 | 5 | 5 | 5 | 5 | 5 | 5 | 4 | 4 | 4 |
| 5 | 6 | 6 | 6 | 6 | 6 | 6 | 5 | 5 | 5 |
| 6 | 7 | 7 | 7 | 7 | 7 | 7 | 6 | 6 | 6 |
| 7 | 8 | 8 | 8 | 8 | 8 | 8 | 7 | 7 | 7 |
| 8 | 9 | 9 | 9 | 9 | 9 | 9 | 8 | 8 | 8 |
| 9 | 10 | 10 | 10 | 10 | 10 | 10 | 9 | 9 | 9 |
| 10 | 11 | 11 | 11 | 11 | 11 | 11 | 10 | 10 | 10 |
| 11 | 12 | 12 | 12 | 12 | 12 | 12 | 11 | 11 | 11 |
| 12 | 13 | 13 | 13 | 13 | 13 | 13 | 12 | 12 | 12 |
| 13 | 14 | 14 | 14 | 14 | 14 | 14 | 13 | 13 | 13 |
| 14 | 15 | 15 | 15 | 15 | 15 | 15 | 14 | 14 | 14 |
| 15 | 16 | 16 | 16 | 16 | 16 | 16 | 15 | 15 | 15 |
| 16 | 17 | 17 | 17 | 17 | 17 | 17 | 16 | 16 | 16 |
| 17 | 18 | 18 | 18 | 18 | 18 | 18 | 17 | 17 | 17 |
| 18 | 19 | 19 | 19 | 19 | 19 | 19 | 18 | 18 | 18 |
| 19 | 20 | 20 | 20 | 20 | 20 | 20 | 19 | 19 | 19 |
| 20 | 21 | 21 | 21 | 21 | 21 | 21 | 20 | 20 | 20 |
| 21 | 22 | 22 | 22 | 22 | 22 | 22 | 21 | 21 | 21 |
| 22 | 23 | 23 | 23 | 23 | 23 | 23 | 22 | 22 | 22 |
| 23 | 24 | 24 | 24 | 24 | 24 | 24 | 23 | 23 | 23 |
| 24 | 25 | 25 | 25 | 25 | 25 | 25 | 24 | 24 | 24 |
| 25 | 26 | 26 | 26 | 26 | 26 | 26 | 25 | 25 | 25 |
| 26 | 27 | 27 | 27 | 27 | 27 | 27 | 26 | 26 | 26 |
| 27 | 28 | 28 | 28 | 28 | 28 | 28 | 27 | 27 | 27 |
| 28 | 29 | 29 | 29 | 29 | 29 | 29 | 28 | 28 | 28 |
| 29 | 30 | 30 | 30 | 30 | 30 | 30 | 29 | 29 | 29 |
| 30 | 31 | 31 | 31 | 31 | 31 | 31 | 30 | 30 | 30 |
| 31 | 32 | 32 | 32 | 32 | 32 | 32 | 31 | 31 | 31 |
| 32 | 33 | 33 | 33 | 33 | 33 | 33 | 32 | 32 | 32 |
| 33 | 34 | 34 | 34 | 34 | 34 | 34 | 33 | 33 | 33 |
| 34 | 35 | 35 | 35 | 35 | 35 | 35 | 34 | 34 | 34 |
| 35 | 36 | 36 | 36 | 36 | 36 | 36 | 35 | 35 | 35 |
| 36 | 37 | 37 | 37 | 37 | 37 | 37 | 36 | 36 | 36 |
| 37 | 38 | 38 | 38 | 38 | 38 | 38 | 37 | 37 | 37 |
| 38 | 39 | 39 | 39 | 39 | 39 | 39 | 38 | 38 | 38 |
| 39 | 40 | 40 | 40 | 40 | 40 | 40 | 39 | 39 | 39 |
| 40 | 41 | 41 | 41 | 41 | 41 | 41 | 40 | 40 | 40 |
| 41 | 42 | 42 | 42 | 42 | 42 | 42 | 41 | 41 | 41 |
| 42 | 43 | 43 | 43 | 43 | 43 | 43 | 42 | 42 | 42 |
| 43 | 44 | 44 | 44 | 44 | 44 | 44 | 43 | 43 | 43 |
| 44 | 45 | 45 | 45 | 45 | 45 | 45 | 44 | 44 | 44 |
| 45 | 46 | 46 | 46 | 46 | 46 | 46 | 45 | 45 | 45 |
| 46 | 47 | 47 | 47 | 47 | 47 | 47 | 46 | 46 | 46 |
| 47 | 48 | 48 | 48 | 48 | 48 | 48 | 47 | 47 | 47 |
| 48 | 49 | 49 | 49 | 49 | 49 | 49 | 48 | 48 | 48 |
| 49 | 50 | 50 | 50 | 50 | 50 | 50 | 49 | 49 | 49 |
| 50 | 51 | 51 | 51 | 51 | 51 | 51 | 50 | 50 | 50 |
| 51 | 52 | 52 | 52 | 52 | 52 | 52 | 51 | 51 | 51 |
| 52 | 53 | 53 | 53 | 53 | 53 | 53 | 52 | 52 | 52 |
| 53 | 54 | 54 | 54 | 54 | 54 | 54 | 53 | 53 | 53 |
| 54 | 55 | 55 | 55 | 55 | 55 | 55 | 54 | 54 | 54 |
| 55 | 56 | 56 | 56 | 56 | 56 | 56 | 55 | 55 | 55 |
| 56 | 57 | 57 | 57 | 57 | 57 | 57 | 56 | 56 | 56 |
| 57 | 58 | 58 | 58 | 58 | 58 | 58 | 57 | 57 | 57 |
| 58 | 59 | 59 | 59 | 59 | 59 | 59 | 58 | 58 | 58 |
| 59 | 60 | 60 | 60 | 60 | 60 | 60 | 59 | 59 | 59 |
| 60 | 61 | 61 | 61 | 61 | 61 | 61 | 60 | 60 | 60 |
| 61 | 62 | 62 | 62 | 62 | 62 | 62 | 61 | 61 | 61 |
| 62 | 63 | 63 | 63 | 63 | 63 | 63 | 62 | 62 | 62 |
| 63 | 64 | 64 | 64 | 64 | 64 | 64 | 63 | 63 | 63 |
| 64 | 65 | 65 | 65 | 65 | 65 | 65 | 64 | 64 | 64 |
| 65 | 66 | 66 | 66 | 66 | 66 | 66 | 65 | 65 | 65 |
| 66 | 67 | 67 | 67 | 67 | 67 | 67 | 66 | 66 | 66 |
| 67 | 68 | 68 | 68 | 68 | 68 | 68 | 67 | 67 | 67 |
| 68 | 69 | 69 | 69 | 69 | 69 | 69 | 68 | 68 | 68 |
| 69 | 70 | 70 | 70 | 70 | 70 | 70 | 69 | 69 | 69 |
| 70 | 71 | 71 | 71 | 71 | 71 | 71 | 70 | 70 | 70 |
| 71 | 72 | 72 | 72 | 72 | 72 | 72 | 71 | 71 | 71 |
| 72 | 73 | 73 | 73 | 73 | 73 | 73 | 72 | 72 | 72 |
| 73 | 74 | 74 | 74 | 74 | 74 | 74 | 73 | 73 | 73 |
| 74 | 75 | 75 | 75 | 75 | 75 | 75 | 74 | 74 | 74 |
| 75 | 76 | 76 | 76 | 76 | 76 | 76 | 75 | 75 | 75 |
| 76 | 77 | 77 | 77 | 77 | 77 | 77 | 76 | 76 | 76 |
| 77 | 78 | 78 | 78 | 78 | 78 | 78 | 77 | 77 | 77 |
| 78 | 79 | 79 | 79 | 79 | 79 | 79 | 78 | 78 | 78 |
| 79 | 80 | 80 | 80 | 80 | 80 | 80 | 79 | 79 | 79 |
| 80 | 81 | 81 | 81 | 81 | 81 | 81 | 80 | 80 | 80 |
| 81 | 82 | 82 | 82 | 82 | 82 | 82 | 81 | 81 | 81 |
| 82 | 83 | 83 | 83 | 83 | 83 | 83 | 82 | 82 | 82 |
| 83 | 84 | 84 | 84 | 84 | 84 | 84 | 83 | 83 | 83 |
| 84 | 85 | 85 | 85 | 85 | 85 | 85 | 84 | 84 | 84 |
| 85 | 86 | 86 | 86 | 86 | 86 | 86 | 85 | 85 | 85 |
| 86 | 87 | 87 | 87 | 87 | 87 | 87 | 86 | 86 | 86 |
| 87 | 88 | 88 | 88 | 88 | 88 | 88 | 87 | 87 | 87 |
| 88 | 89 | 89 | 89 | 89 | 89 | 89 | 88 | 88 | 88 |
| 89 | 90 | 90 | 90 | 90 | 90 | 90 | 89 | 89 | 89 |
| 90 | 91 | 91 | 91 | 91 | 91 | 91 | 90 | 90 | 90 |
| 91 | 92 | 92 | 92 | 92 | 92 | 92 | 91 | 91 | 91 |
| 92 | 93 | 93 | 93 | 93 | 93 | 93 | 92 | 92 | 92 |
| 93 | 94 | 94 | 94 | 94 | 94 | 94 | 93 | 93 | 93 |
| 94 | 95 | 95 | 95 | 95 | 95 | 95 | 94 | 94 | 94 |
| 95 | 96 | 96 | 96 | 96 | 96 | 96 | 95 | 95 | 95 |
| 96 | 97 | 97 | 97 | 97 | 97 | 97 | 96 | 96 | 96 |
| 97 | 98 | 98 | 98 | 98 | 98 | 98 | 97 | 97 | 97 |
| 98 | 99 | 99 | 99 | 99 | 99 | 99 | 98 | 98 | 98 |
| 99 | 100 | 100 | 100 | 100 | 100 | 100 | 99 | 99 | 99 |
| 100 | 101 | 101 | 101 | 101 | 101 | 101 | 100 | 100 | 100 |

| | | | |
|----|-------|---|-------|
| 9 | 30115 | 0 | 111 |
| 10 | 00116 | 0 | 11111 |
| 10 | 30117 | 0 | |
| 11 | 00118 | 0 | |
| 11 | 30119 | 0 | |
| 12 | 00120 | 0 | |

#N/A#

STATION 1. PLAN 1. RATIO 4
END-OF-PERIOD HYDROGRAPH ORDINATES

[illegible]

PEAK OUTFLOW IS 636. AT TIME 60.00 HOURS

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
 636 317 127 431
 18 17 4 0.14
 CFS 0.07 0.14 0.14
 CMS 1.77 3.68 3.68
 INCHES 303 629 629
 AC-FT 374 775 775
 THOUS CU H

OVF

STATION 1

| INFLW(1),
8000. 12000. 15000. 20000. 24000. | OUTFLOW(2)
15000. | AND OBSERVED FLOW(3)
24000. | 0. | 0. | 0. | 0. | 0. | 0. | 0. |
|--|----------------------|--------------------------------|----|----|----|----|----|----|----|
| 0.11 | | | | | | | | | |
| 30.00 | | | | | | | | | |
| 1.13 | | | | | | | | | |
| 2.25 | | | | | | | | | |
| 3.37 | | | | | | | | | |
| 4.49 | | | | | | | | | |
| 5.61 | | | | | | | | | |
| 6.73 | | | | | | | | | |
| 7.85 | | | | | | | | | |
| 8.97 | | | | | | | | | |
| 10.09 | | | | | | | | | |
| 11.21 | | | | | | | | | |
| 12.33 | | | | | | | | | |
| 13.45 | | | | | | | | | |
| 14.57 | | | | | | | | | |
| 15.69 | | | | | | | | | |
| 16.81 | | | | | | | | | |
| 17.93 | | | | | | | | | |
| 19.05 | | | | | | | | | |
| 20.17 | | | | | | | | | |
| 21.29 | | | | | | | | | |
| 22.41 | | | | | | | | | |
| 23.53 | | | | | | | | | |
| 24.65 | | | | | | | | | |
| 25.77 | | | | | | | | | |
| 26.89 | | | | | | | | | |
| 28.01 | | | | | | | | | |
| 29.13 | | | | | | | | | |
| 30.25 | | | | | | | | | |
| 31.37 | | | | | | | | | |
| 32.49 | | | | | | | | | |
| 33.61 | | | | | | | | | |
| 34.73 | | | | | | | | | |
| 35.85 | | | | | | | | | |
| 36.97 | | | | | | | | | |
| 38.09 | | | | | | | | | |
| 39.21 | | | | | | | | | |
| 40.33 | | | | | | | | | |
| 41.45 | | | | | | | | | |
| 42.57 | | | | | | | | | |
| 43.69 | | | | | | | | | |
| 44.81 | | | | | | | | | |
| 45.93 | | | | | | | | | |
| 47.05 | | | | | | | | | |
| 48.17 | | | | | | | | | |
| 49.29 | | | | | | | | | |
| 50.41 | | | | | | | | | |
| 51.53 | | | | | | | | | |
| 52.65 | | | | | | | | | |
| 53.77 | | | | | | | | | |
| 54.89 | | | | | | | | | |
| 56.01 | | | | | | | | | |
| 57.13 | | | | | | | | | |
| 58.25 | | | | | | | | | |
| 59.37 | | | | | | | | | |
| 60.49 | | | | | | | | | |
| 61.61 | | | | | | | | | |
| 62.73 | | | | | | | | | |
| 63.85 | | | | | | | | | |
| 64.97 | | | | | | | | | |
| 66.09 | | | | | | | | | |
| 67.21 | | | | | | | | | |
| 68.33 | | | | | | | | | |
| 69.45 | | | | | | | | | |
| 70.57 | | | | | | | | | |
| 71.69 | | | | | | | | | |
| 72.81 | | | | | | | | | |
| 73.93 | | | | | | | | | |
| 75.05 | | | | | | | | | |
| 76.17 | | | | | | | | | |
| 77.29 | | | | | | | | | |
| 78.41 | | | | | | | | | |
| 79.53 | | | | | | | | | |
| 80.65 | | | | | | | | | |
| 81.77 | | | | | | | | | |
| 82.89 | | | | | | | | | |
| 84.01 | | | | | | | | | |
| 85.13 | | | | | | | | | |
| 86.25 | | | | | | | | | |
| 87.37 | | | | | | | | | |
| 88.49 | | | | | | | | | |
| 89.61 | | | | | | | | | |
| 90.73 | | | | | | | | | |
| 91.85 | | | | | | | | | |
| 92.97 | | | | | | | | | |
| 94.09 | | | | | | | | | |
| 95.21 | | | | | | | | | |
| 96.33 | | | | | | | | | |
| 97.45 | | | | | | | | | |
| 98.57 | | | | | | | | | |
| 99.69 | | | | | | | | | |
| 100.81 | | | | | | | | | |

22 30 451
23 30 461
24 30 471
25 30 481
26 30 491
27 30 501
28 30 511
29 30 521
30 30 531
31 30 541
32 30 551
33 30 561
34 30 571
35 30 581
36 30 591
37 30 601
38 30 610
39 30 620
40 30 630
41 30 640
42 30 650
43 30 660
44 30 670
45 30 680
46 30 690
47 30 700
48 30 710
49 30 720
50 30 730
51 30 740
52 30 750
53 30 760
54 30 770
55 30 780
56 30 790
57 30 800
58 30 810
59 30 820
60 30 830
61 30 840
62 30 850
63 30 860
64 30 870
65 30 880
66 30 890
67 30 900
68 30 910
69 30 920
70 30 930
71 30 940
72 30 950
73 30 960
74 30 970
75 30 980
76 30 990
77 30 1000
78 30 1010
79 30 1020
80 30 1030
81 30 1040
82 30 1050
83 30 1060
84 30 1070
85 30 1080
86 30 1090
87 30 1100
88 30 1110
89 30 1120
90 30 1130
91 30 1140
92 30 1150
93 30 1160
94 30 1170
95 30 1180
96 30 1190
97 30 1200
98 30 1210
99 30 1220
100 30 1230
101 30 1240
102 30 1250

16 30 3301
17 00 341
18 00 351
19 00 361
20 00 371
21 00 381
22 00 391
23 00 401
24 00 411
25 00 421
26 00 431
27 00 441
28 00 451
29 00 461
30 00 471
31 00 481
32 00 491
33 00 501
34 00 511
35 00 521
36 00 531
37 00 5401
38 00 5501
39 00 5601
40 00 5701
41 00 5801
42 00 5901
43 00 6001
44 00 6101
45 00 6201
46 00 6301
47 00 6401
48 00 6501
49 00 6601
50 00 6701
51 00 6801
52 00 6901
53 00 7001
54 00 7101
55 00 7201
56 00 7301
57 00 7401
58 00 7501
59 00 7601
60 00 7701
61 00 7801
62 00 7901
63 00 8001
64 00 8101
65 00 8201
66 00 8301
67 00 8401
68 00 8501
69 00 8601
70 00 8701
71 00 8801
72 00 8901
73 00 9001

AD-A109 795

FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT
NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)
JUL 81 H C FLAHERTY
DACW51-81-C-0006

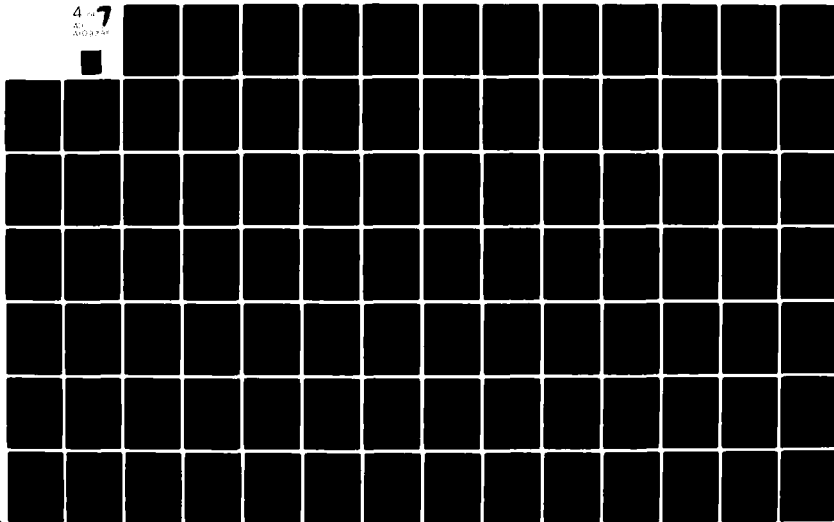
F/G 13/13

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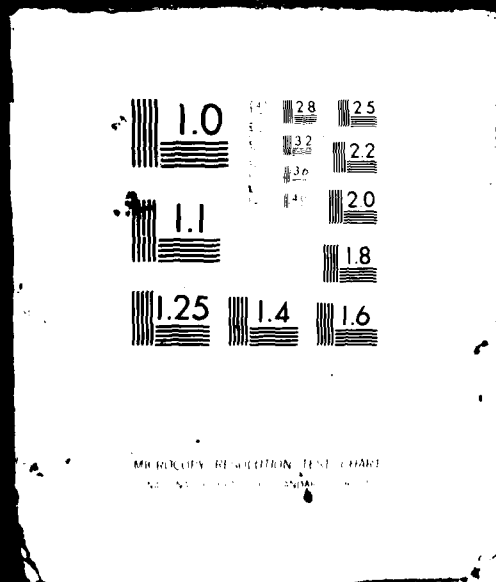
7



4 OF 7

AD-

A109795



PEAK OUTFLOW IS 745. AT TIME 60.00 HOURS

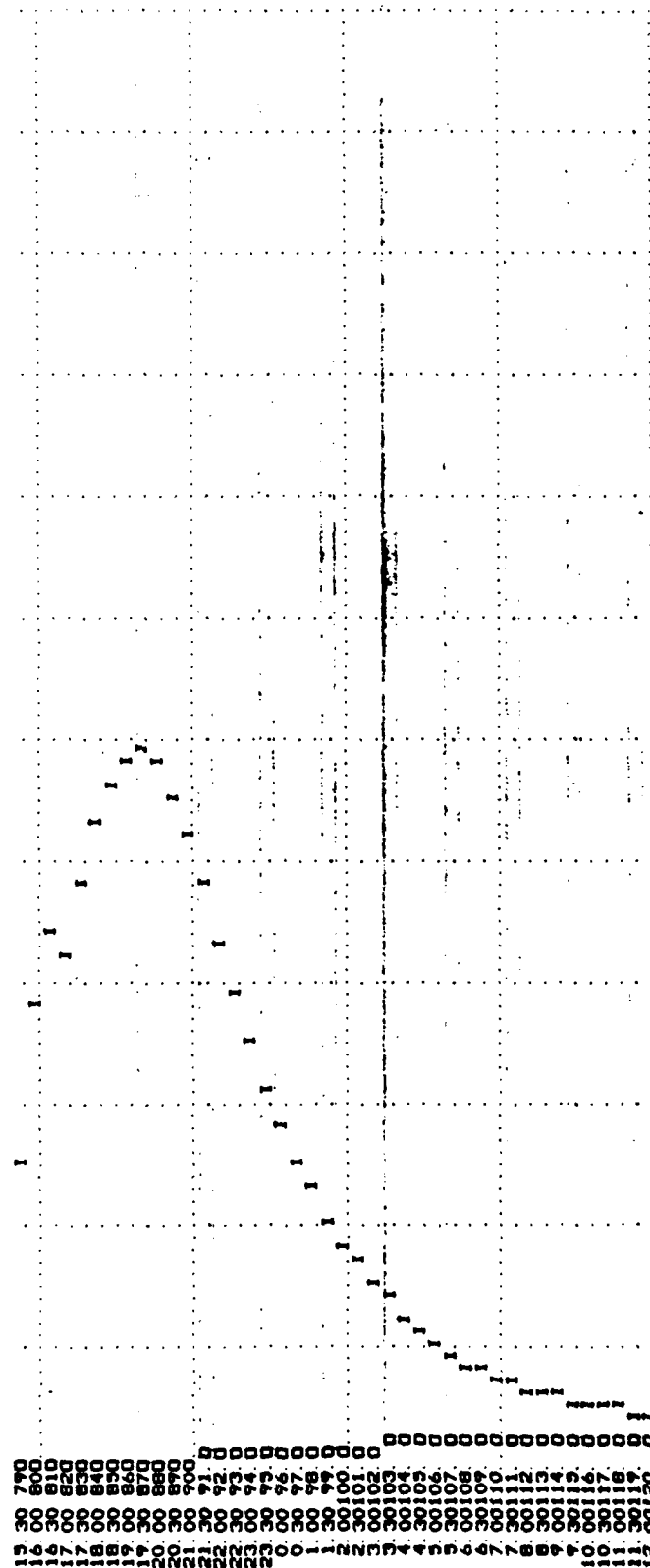
CFB
CMB
INCHES
MM
AC-FT
THOUS CU F

◆OVE◆

STATION 1

| | |
|-------|---|
| | INFLOW(I), "OUTFLOW(I)" AND OBSERVED FLOW(I)" |
| 3000. | 12000 |
| | 16000 |
| | 20000 |
| | 24000 |

[illegible]



STATION 1. PLAN 1. RATIO 7
END-OF-PERIOD HYDROGRAPH ORDINATES

OUTFLOW

0000000
0000000
0000000
0000000
0000000
0000000
0000000
0000000
0000000

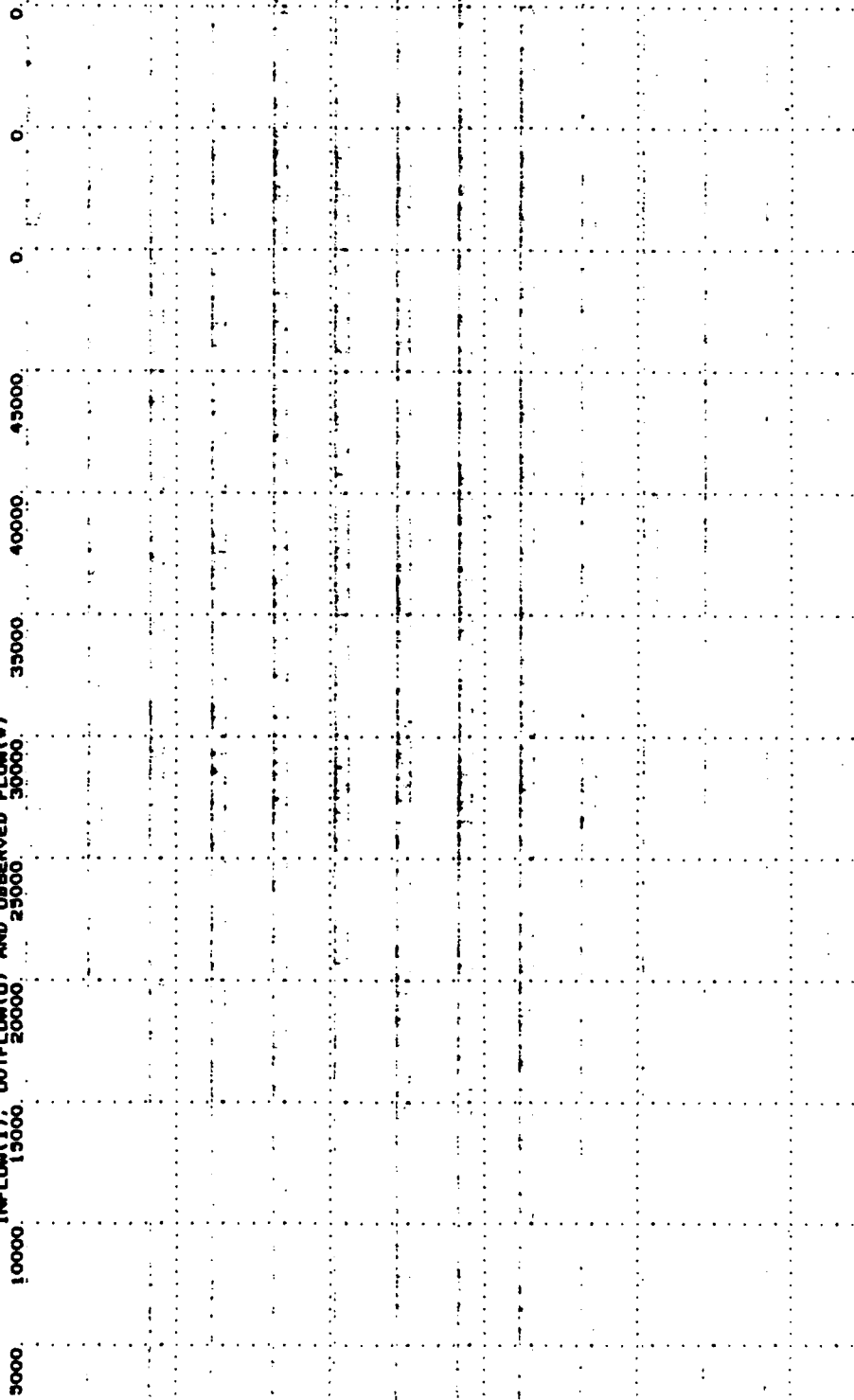
*QVNS

9 30 670
 10 30 680
 11 30 690
 12 30 700
 13 30 710
 14 30 720
 15 30 730
 16 30 740
 17 30 750
 18 30 760
 19 30 770
 20 30 780
 21 30 790
 22 30 800
 23 30 810
 24 30 820
 25 30 830
 26 30 840
 27 30 850
 28 30 860
 29 30 870
 30 30 880
 31 30 890
 32 30 900
 33 30 910
 34 30 920
 35 30 930
 36 30 940
 37 30 950
 38 30 960
 39 30 970
 40 30 980
 41 30 990
 42 30 1000
 43 30 1010
 44 30 1020
 45 30 1030
 46 30 1040
 47 30 1050
 48 30 1060
 49 30 1070
 50 30 1080
 51 30 1090
 52 30 1100
 53 30 1110
 54 30 1120
 55 30 1130
 56 30 1140
 57 30 1150
 58 30 1160
 59 30 1170
 60 30 1180
 61 30 1190
 62 30 1200

STATION

INFLW(1), OUTFLOW(1) AND OBSERVED FLOW(1)

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54



PEAK OUTFLOW IS 11660 AT TIME 34.00 HOURS

| | | | | |
|------------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 11660 | 11578 | 7101 | 2840 | 340840 |
| 330 | 328 | 301 | 80 | 9251 |
| CFS | | | | |
| CMH | 1.32 | 3.23 | 3.23 | 3.23 |
| INCHES | 33.22 | 82.47 | 82.47 | 82.47 |
| MM | 27.81 | 15593 | 15593 | 15593 |
| AC-FT | 7082 | 17373 | 17373 | 17373 |
| THOUS CU M | | | | |

OVF

STATION 1

| | INFLW(I), OUTFLOW(O) AND OBSERVED FLOW(*) | | | | |
|----|---|-------|-------|-------|-------|
| | 0 | 10000 | 20000 | 30000 | 40000 |
| 0 | 11 | | | | |
| 1 | 30 | | | | |
| 2 | 30 | | | | |
| 3 | 30 | | | | |
| 4 | 30 | | | | |
| 5 | 30 | | | | |
| 6 | 30 | | | | |
| 7 | 30 | | | | |
| 8 | 30 | | | | |
| 9 | 30 | | | | |
| 10 | 30 | | | | |
| 11 | 30 | | | | |
| 12 | 30 | | | | |
| 13 | 30 | | | | |
| 14 | 30 | | | | |
| 15 | 30 | | | | |
| 16 | 30 | | | | |
| 17 | 30 | | | | |
| 18 | 30 | | | | |
| 19 | 30 | | | | |
| 20 | 30 | | | | |
| 21 | 30 | | | | |
| 22 | 30 | | | | |
| 23 | 30 | | | | |
| 24 | 30 | | | | |
| 25 | 30 | | | | |
| 26 | 30 | | | | |
| 27 | 30 | | | | |
| 28 | 30 | | | | |
| 29 | 30 | | | | |
| 30 | 30 | | | | |
| 31 | 30 | | | | |
| 32 | 30 | | | | |
| 33 | 30 | | | | |
| 34 | 30 | | | | |
| 35 | 30 | | | | |
| 36 | 30 | | | | |
| 37 | 30 | | | | |
| 38 | 30 | | | | |
| 39 | 30 | | | | |
| 40 | 30 | | | | |
| 41 | 30 | | | | |
| 42 | 30 | | | | |

21 30 00 431
 22 30 00 441
 23 30 00 451
 24 30 00 461
 25 30 00 471
 26 30 00 481
 27 30 00 491
 28 30 00 501
 29 30 00 510
 30 30 00 520
 31 30 00 530
 32 30 00 540
 33 30 00 550
 34 30 00 560
 35 30 00 570
 36 30 00 580
 37 30 00 590
 38 30 00 600
 39 30 00 610
 40 30 00 620
 41 30 00 630
 42 30 00 640
 43 30 00 650
 44 30 00 660
 45 30 00 670
 46 30 00 680
 47 30 00 690
 48 30 00 700
 49 30 00 710
 50 30 00 720
 51 30 00 730
 52 30 00 740
 53 30 00 750
 54 30 00 760
 55 30 00 770
 56 30 00 780
 57 30 00 790
 58 30 00 800
 59 30 00 810
 60 30 00 820
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 67 30 00 890
 68 30 00 900
 69 30 00 910
 70 30 00 920
 71 30 00 930
 72 30 00 940
 73 30 00 950
 74 30 00 960
 75 30 00 970
 76 30 00 980
 77 30 00 990
 78 30 00 1000

2 30101.
3 30102.
4 30103.
5 30104.
6 30105.
7 30106.
8 30107.
9 30108.
10 30109.
11 30110.
12 30111.
13 30112.
14 30113.
15 30114.
16 30115.
17 30116.
18 30117.
19 30118.
20 30119.
21 30120.

DVN

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
AREA IN SQUARE MILES (SQUARE KILOMETERS)

| OPERATION | STATION | AREA | PLAN | RATIO 1
0.20 | RATIO 2
0.25 | RATIO 3
0.26 | RATIO 4
0.27 | RATIO 5
0.28 | RATIO 6
0.29 | RATIO 7
0.30 | RATIO 8
0.30 | RATIO 9
1.00 |
|---------------|---------|-------------------|------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| HYDROGRAPH AT | 1 | 23.84
(61.74) | 1 | 3064
(143.40) | 6330
(179.25) | 6583
(186.42) | 6837
(193.59) | 7090
(200.76) | 7343
(207.93) | 7596
(215.10) | 7850
(222.27) | 8103
(229.44) |
| HYDROGRAPH AT | 1 | 13.03
(33.79) | 1 | 3007
(85.15) | 3759
(106.43) | 3909
(110.69) | 4059
(114.95) | 4210
(119.20) | 4360
(123.46) | 4510
(127.72) | 4660
(131.98) | 4810
(136.24) |
| 2 COMBINED | 1 | 36.87
(95.49) | 1 | 7794
(226.36) | 7792
(226.36) | 10392
(294.26) | 10792
(305.58) | 11191
(316.90) | 11591
(328.22) | 11991
(339.54) | 12391
(350.86) | 12791
(362.18) |
| HYDROGRAPH AT | 1 | 17.47
(45.25) | 1 | 3103
(87.93) | 3881
(109.91) | 4037
(114.31) | 4192
(118.76) | 4347
(123.10) | 4503
(127.50) | 4658
(131.89) | 4813
(136.28) | 4968
(140.67) |
| 2 COMBINED | 1 | 54.34
(140.74) | 1 | 10939
(310.31) | 13678
(387.89) | 14246
(403.41) | 14794
(418.92) | 15342
(434.44) | 15890
(449.95) | 16438
(465.47) | 16986
(480.99) | 17534
(496.51) |
| HYDROGRAPH AT | 1 | 4.77
(12.35) | 1 | 1088
(30.80) | 1360
(38.50) | 1414
(40.04) | 1468
(41.58) | 1523
(43.12) | 1577
(44.66) | 1631
(46.20) | 1685
(47.74) | 1739
(49.28) |

| | | | | | | | | | | | | |
|---------------|---|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|----------|
| 2 COMBINED | 1 | 59.11 | 12017 | 15021 | 15622 | 16223 | 16824 | 17425 | 18025 | 30042 | 60083 | |
| | (| 153.09) | (| 425.35) | (| 442.37) | (| 476.39) | (| 510.42) | (| 1701.41) |
| HYDROGRAPH AT | 1 | 5.56 | 1475 | 1843 | 1917 | 1991 | 2044 | 2138 | 2212 | 3687 | 7373 | |
| | (| 14.40) | (| 52.20) | (| 54.28) | (| 58.46) | (| 62.64) | (| 208.78) |
| 2 COMBINED | 1 | 64.67 | 13263 | 16382 | 17243 | 17908 | 18372 | 19235 | 19878 | 33164 | 66327 | |
| | (| 167.49) | (| 469.54) | (| 488.33) | (| 507.11) | (| 544.67) | (| 1878.18) |
| HYDROGRAPH AT | 1 | 10.33 | 2777 | 3471 | 3610 | 3749 | 3887 | 4026 | 4165 | 6942 | 13883 | |
| | (| 26.75) | (| 98.28) | (| 102.22) | (| 110.08) | (| 114.01) | (| 196.57) |
| 2 COMBINED | 1 | 75.00 | 15832 | 19750 | 20581 | 21373 | 22165 | 22956 | 23748 | 39580 | 79139 | |
| | (| 194.25) | (| 448.51) | (| 560.38) | (| 605.21) | (| 672.46) | (| 2241.53) |
| HYDROGRAPH AT | 1 | 6.38 | 4153 | 5191 | 5399 | 5606 | 5814 | 6022 | 6229 | 10382 | 20764 | |
| | (| 16.52) | (| 117.60) | (| 147.00) | (| 158.76) | (| 176.39) | (| 293.99) |
| 2 COMBINED | 1 | 81.38 | 16223 | 20278 | 21089 | 21901 | 22712 | 23523 | 24334 | 40537 | 81113 | |
| | (| 210.77) | (| 459.38) | (| 574.22) | (| 613.12) | (| 666.09) | (| 1148.44) |
| ROUTED TO | 1 | 81.38 | 318 | 533 | 582 | 636 | 689 | 749 | 837 | 3317 | 11660 | |
| | (| 210.77) | (| 15.09) | (| 16.48) | (| 18.00) | (| 23.69) | (| 93.92) |

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SUMMARY OF DAM SAFETY ANALYSIS

| | | | |
|-----------|---------------|----------------|------------|
| PLAN 1 | INITIAL VALUE | SPILLWAY CREST | TOP OF DAM |
| ELEVATION | 1190.00 | 1191.10 | 1194.20 |
| STORAGE | 20440 | 25225 | 39800 |
| OUTFLOW | | 0 | 758 |

| RATIO OF PPE | MAXIMUM RESERVOIR W.S. ELEV | MAXIMUM DEPTH OVER DAM | MAXIMUM STORAGE AC-FT | MAXIMUM OUTFLOW CFS | DURATION OVER TOP HOURS | TIME OF MAX OUTFLOW HOURS | TIME OF FAILURE HOURS |
|--------------|-----------------------------|------------------------|-----------------------|---------------------|-------------------------|---------------------------|-----------------------|
| 0.20 | 1192.97 | 0.00 | 33917 | 318 | 0.00 | 40.00 | 0.00 |
| 0.25 | 1193.43 | 0.00 | 37091 | 332 | 0.00 | 40.00 | 0.00 |
| 0.30 | 1193.74 | 0.00 | 37707 | 382 | 0.00 | 40.00 | 0.00 |
| 0.35 | 1194.04 | 0.00 | 38370 | 438 | 0.00 | 40.00 | 0.00 |
| 0.40 | 1194.34 | 0.00 | 39023 | 489 | 0.00 | 40.00 | 0.00 |
| 0.45 | 1194.64 | 0.00 | 39677 | 541 | 0.00 | 40.00 | 0.00 |
| 0.50 | 1194.94 | 0.00 | 40329 | 593 | 0.00 | 40.00 | 0.00 |
| 0.55 | 1195.24 | 0.00 | 40982 | 645 | 0.00 | 40.00 | 0.00 |
| 0.60 | 1207.56 | 13.16 | 77046 | 11660 | 18.50 | 54.00 | 0.00 |

 FLOOD HYDROGRAPH PACKAGE (HEC-1)
 DAM SAFETY VERSION JULY 1978
 LAST MODIFICATION 26 FEB 79

HEC-1 FLOOD HYDROGRAPH COMPUTATIONS
(WITHOUT FLASHBOARDS IN PLACE)

FLAHERTY GIAVARA ASSOCIATES, P. C.

FLOOD HYDROGRAPH PACKAGE (HEC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 26 FEB 79

1 A1 NATIONAL DAM INSPECTION PROGRAM, PHASE I REPORT, CORPS OF ENGINEERS - NEW YORK DISTRICT
2 A2 DAM INVENTORY NO. NY 361, OTSEGO LAKE DAM (WITHOUT FLASHBOARDS), CHERANGO COUNTY, NEW YORK, APRIL 27, 1981
3 A3 PREPARED BY FLAHERTY GIAVARA ASSOCIATES, P. C., ONE COLUMBUS PLAZA, NEW HAVEN, CONNECTICUT
4 B 120
5 B1
6 J1
7 J1
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52 K1

| | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
|--|------|------|------|------|------|------|------|------|
| INFLW HYDROGRAPH - SUBWATERISHED NO. 1 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
| INFLW HYDROGRAPH - SUBWATERISHED NO. 2 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
| INFLW HYDROGRAPH - SUBWATERISHED NO. 3 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
| INFLW HYDROGRAPH - SUBWATERISHED NO. 4 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
| INFLW HYDROGRAPH - SUBWATERISHED NO. 5 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |
| INFLW HYDROGRAPH - SUBWATERISHED NO. 6 | 0.27 | 0.30 | 0.31 | 0.32 | 0.33 | 0.34 | 0.50 | 1.00 |

PREPARED BY FLAHERTY GIAVARA ASSOCIATES, P. C., ONE COLUMBUS PLAZA, NEW HAVEN, CONNECTICUT

NG 120 NHR 0 NMIN 30 IDAY 0 JOPER 5
 JOB SPECIFICATION
 IHR 0 IMIN 0 METRC 0
 NMT 0 LROPT 0 TRACE 0
 INSTAN 0

MULTI-PLAN ANALYSES TO BE PERFORMED

RTIOS= 0.20 0.29 0.30 0.31 0.32 0.33 0.34 0.50 1.00
 NPLAN= 1 NRTIO= 9 LRTIO= 1

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH - SUBWATERSHED NO. 1
 ISTAQ 1 ICNTP 0 ITRF 0 IPLI 0 IPRY 1 INAME 1STAGE 0 INUTD 0

HYDO 1 IUNG 1 TAREA 1 SWAP 0.00 TRSBA 23.84 TRSFC 0.00 RATIO 0.000 IENCH 0 ISAME 1 LOCAL 0

PRECIP DATA
 R12 84.00 R24 112.00 R48 119.00 R72 0.00 R96 0.00
 TRSPC COMPUTED BY THE PROGRAM IS 0.829

LOSS DATA
 LROPT 0 STRKR 0 DLTKR 0 RTIOL 1.00 ERAIN 0.00 STRMS 0.00 RTIOM 1.00 CNSTL 0.10 ALSHX 0.00 RTIMP 0.01

TP= 4.61 UNIT HYDROGRAPH DATA NTA= 0
 CP=0.63

APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC=10.22 AND N= 8.29 INTERVALS
 RECESSION DATA
 STRIQ= -2.00 GRCEM= -0.10 RTIOM= 1.50
 N= 10.22

UNIT HYDROGRAPH 50 END-OF-PERIOD ORDINATES, LAG= 4.57 HOURS, CP= 0.63 VOL= 1.00

| MO | DA | HR | MM | PERIOD | RAIN | EXCS | LOSS | COMP | LOSS | COMP |
|-----|------|------|------|--------|------|------|------|------|------|------|
| 74 | 2030 | 1798 | 1594 | 1412 | 422 | 126 | 38 | 42 | 2167 | 281 |
| 606 | 181 | 140 | 48 | 42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 181 | 140 | 48 | 42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 34 | 42 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

END-OF-PERIOD FLOW

| MO | DA | HR | MM | PERIOD | RAIN | EXCS | LOSS | COMP | LOSS | COMP |
|------|------|------|------|--------|------|------|------|------|------|------|
| 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 |
| 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 |
| 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 |
| 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 | 1001 |

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5 00104
6 00105
7 00106
8 00107
9 00108
10 00109
11 00110
12 00111
13 00112
14 00113
15 00114
16 00115
17 00116
18 00117
19 00118
20 00119
21 00120

OVN

C-255

HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 1

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------|--------|---------|---------|--------------|
| 9064 | 4282 | 1932 | 797 | 95612 |
| 143 | 121 | 55 | 23 | 2709 |
| | 1.67 | 3.01 | 3.11 | |
| | 42.44 | 76.58 | 78.99 | |
| | 2124 | 3831 | 3952 | |
| | 2619 | 4726 | 4875 | |

CFS
CMS
INCHES
MM
AC-FT
THOUS CU M

HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 2

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------|--------|---------|---------|--------------|
| 9064 | 4282 | 1932 | 797 | 95612 |
| 143 | 121 | 55 | 23 | 2709 |
| | 1.67 | 3.01 | 3.11 | |
| | 42.44 | 76.58 | 78.99 | |
| | 2124 | 3831 | 3952 | |
| | 2619 | 4726 | 4875 | |

CFS
CMS
INCHES
MM
AC-FT
THOUS CU M

C-256

FLAHERTY GIARARA ASSOCIATES, P. C.

| 843. | 810. | 777. | 747. | 717. | 688. | 661. | 635. | 610. | 585. |
|------|------|------------|--------|---------|---------|--------------|------|------|------|
| | | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | |
| | | 8609. | 7280. | 3284. | 1355. | 162991. | | | |
| | | 244. | 208. | 93. | 38. | 4604. | | | |
| | | | 2.84 | 3.13 | 5.29 | 5.29 | | | |
| | | | 72.15 | 130.18 | 134.29 | 134.29 | | | |
| | | | 3610. | 6313. | 6719. | 6719. | | | |
| | | | 4953. | 8034. | 8287. | 8287. | | | |
| | | THOUS CU M | | | | | | | |

| 843. | 810. | 777. | 747. | 717. | 688. | 661. | 635. | 610. | 585. |
|------|------|------------|--------|---------|---------|--------------|------|------|------|
| | | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | |
| | | 12680. | 10706. | 4829. | 1973. | 239105. | | | |
| | | 358. | 303. | 137. | 56. | 6771. | | | |
| | | | 4.19 | 7.24 | 7.77 | 7.77 | | | |
| | | | 106.11 | 191.85 | 197.48 | 197.48 | | | |
| | | | 5309. | 9578. | 9880. | 9880. | | | |
| | | | 6548. | 11815. | 12187. | 12187. | | | |
| | | THOUS CU M | | | | | | | |

C-258

| 843. | 810. | 777. | 747. | 717. | 688. | 661. | 635. | 610. | 585. |
|------|------|------------|--------|---------|---------|--------------|------|------|------|
| | | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | |
| | | 12680. | 10706. | 4829. | 1973. | 239105. | | | |
| | | 358. | 303. | 137. | 56. | 6771. | | | |
| | | | 4.19 | 7.24 | 7.77 | 7.77 | | | |
| | | | 106.11 | 191.85 | 197.48 | 197.48 | | | |
| | | | 5309. | 9578. | 9880. | 9880. | | | |
| | | | 6548. | 11815. | 12187. | 12187. | | | |
| | | THOUS CU M | | | | | | | |

| 843. | 810. | 777. | 747. | 717. | 688. | 661. | 635. | 610. | 585. |
|------|------|------------|--------|---------|---------|--------------|------|------|------|
| | | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | |
| | | 12680. | 10706. | 4829. | 1973. | 239105. | | | |
| | | 358. | 303. | 137. | 56. | 6771. | | | |
| | | | 4.19 | 7.24 | 7.77 | 7.77 | | | |
| | | | 106.11 | 191.85 | 197.48 | 197.48 | | | |
| | | | 5309. | 9578. | 9880. | 9880. | | | |
| | | | 6548. | 11815. | 12187. | 12187. | | | |
| | | THOUS CU M | | | | | | | |

FLAHERTY DIAVARA ASSOCIATES, P C.

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH - SUBWATERSHED NO. 2
ISTAG ICOMP IECON ITAPE JPLT JPRY INAME ISTAGE IAUTO

HYDQ I IUMQ IAREA IUMQ SNAP TRSDA TRBPC RATIO ISNOM ISAVE LOCAL

PRECIP DATA
R12 R24 R48 R72 R96
R6 R12 R24 R48 R72 R96

TRBPC COMPUTED BY THE PROGRAM IS 0.007

LOSS DATA
LROFT STRKR DLTAR RTIOL ERAIN STRKS RTIOK STRTL CNSTL ALSMX RTIMP

UNIT HYDROGRAPH DATA
TP= 3.87 CP=0.43 NTA= 0

RECESSION DATA
STRIO= -2.00 GRCSN= -0.10 RTIOK= 1.50
APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 8.75 AND R= 7.04 INTERVALS

UNIT HYDROGRAPH 42 END-OF-PERIOD ORDINATES. LAG= 3.87 HOURS. CP= 0.43 VOL= 1.00
61 1050 223 911 220 53 13
450 705 228 1187 1332 447 388 292 292 171 46

| MO | DA | HR | MN | PERIOD | RAIN | EXCS | LOSS | END-OF-PERIOD FLOW | COMP | MO | DA | HR | MN | PERIOD | RAIN | EXCS | LOSS | COMP |
|----|----|----|----|--------|------|------|------|--------------------|------|----|----|----|----|--------|------|------|------|-------|
| 1 | 1 | 0 | 30 | 1 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 0 | 30 | 1 | 0.00 | 0.00 | 0.00 | 161 |
| 1 | 1 | 1 | 30 | 2 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 1 | 30 | 2 | 0.00 | 0.00 | 0.00 | 177 |
| 1 | 1 | 2 | 30 | 3 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 2 | 30 | 3 | 0.00 | 0.00 | 0.00 | 238 |
| 1 | 1 | 3 | 30 | 4 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 3 | 30 | 4 | 0.00 | 0.00 | 0.00 | 349 |
| 1 | 1 | 4 | 30 | 5 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 4 | 30 | 5 | 0.00 | 0.00 | 0.00 | 471 |
| 1 | 1 | 5 | 30 | 6 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 5 | 30 | 6 | 0.00 | 0.00 | 0.00 | 518 |
| 1 | 1 | 6 | 30 | 7 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 6 | 30 | 7 | 0.00 | 0.00 | 0.00 | 752 |
| 1 | 1 | 7 | 30 | 8 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 7 | 30 | 8 | 0.00 | 0.00 | 0.00 | 1117 |
| 1 | 1 | 8 | 30 | 9 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 8 | 30 | 9 | 0.00 | 0.00 | 0.00 | 1392 |
| 1 | 1 | 9 | 30 | 10 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 9 | 30 | 10 | 0.00 | 0.00 | 0.00 | 1504 |
| 1 | 1 | 10 | 30 | 11 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 10 | 30 | 11 | 0.00 | 0.00 | 0.00 | 1630 |
| 1 | 1 | 11 | 30 | 12 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 11 | 30 | 12 | 0.00 | 0.00 | 0.00 | 1824 |
| 1 | 1 | 12 | 30 | 13 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 12 | 30 | 13 | 0.00 | 0.00 | 0.00 | 2123 |
| 1 | 1 | 13 | 30 | 14 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 13 | 30 | 14 | 0.00 | 0.00 | 0.00 | 23563 |
| 1 | 1 | 14 | 30 | 15 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 14 | 30 | 15 | 0.00 | 0.00 | 0.00 | 2933 |
| 1 | 1 | 15 | 30 | 16 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 15 | 30 | 16 | 0.00 | 0.00 | 0.00 | 3933 |
| 1 | 1 | 16 | 30 | 17 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 16 | 30 | 17 | 0.00 | 0.00 | 0.00 | 4860 |
| 1 | 1 | 17 | 30 | 18 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 17 | 30 | 18 | 0.00 | 0.00 | 0.00 | 6090 |
| 1 | 1 | 18 | 30 | 19 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 18 | 30 | 19 | 0.00 | 0.00 | 0.00 | |
| 1 | 1 | 19 | 30 | 20 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 19 | 30 | 20 | 0.00 | 0.00 | 0.00 | |
| 1 | 1 | 20 | 30 | 21 | 0.00 | 0.00 | 0.00 | 1.02 | 24 | 1 | 1 | 20 | 30 | 21 | 0.00 | 0.00 | 0.00 | |

[illegible]

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|-------|--------|---------|---------|-------|--------|
| CFS | 15034 | 13274 | 5236 | 2166 | 25903 | 7360 |
| CMS | 426 | 348 | 148 | 61 | 516 | 1546 |
| INCHES | | 876 | 1495 | 1546 | | 39274 |
| MM | | 379.80 | 379.80 | 392.74 | | 10740 |
| CU-FT | | 6086 | 10386 | 12811 | | 13247 |
| THOUS | | 7507 | | | | |

◆◆◆◆◆

STATION 11

| INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|------------|------------|----------------------|
| 1000. | 6000. | 8000. |
| | | 10000. |
| | | 12000. |

14000. : 16000.

•

PRECIP(L) AND EXCESS(X)

FLAHERTY GIAVARA ASSOCIATES, P. C.

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99

PAGE 0014

[illegible]

LC-262

10 00116
10 00117
11 00118
11 00119
12 00120

DYN

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301
1881
1984
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240

326
2228
1744
490
231

100
170
369
2551
1934
1422
222

14
42
423
2809
1351
1370
213

121
131
1313
2111
1191
121
204

121
131
1313
2111
1191
121
204

CFS
CMS
INCHES
AC-FY
THOUS CU M

PEAK
3007
85

2455
170
175
1217
1501

24-HOUR
1047
30
299
75.96
2077
2562

72-HOUR
432
12
309
78.25
2148
2649

TOTAL VOLUME
51981
1473
3109
78.25
2148
2649

C-263

CFS
CMS
INCHES
AC-FY
THOUS CU M

PEAK
4340
123

3359
101
254
44.55
1793
2177

24-HOUR
1518
43
43
110.14
3012
3715

72-HOUR
628
18
4.48
113.90
3113
3842

TOTAL VOLUME
75372
2134
4.48
113.90
3113
3842

C-263

CFS
CMS
INCHES
AC-FY
THOUS CU M

PEAK
4340
123

3359
101
254
44.55
1793
2177

24-HOUR
1518
43
43
110.14
3012
3715

72-HOUR
628
18
4.48
113.90
3113
3842

TOTAL VOLUME
75372
2134
4.48
113.90
3113
3842

C-263

[illegible]

| | PEAK | 8-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|--------|--------|
| CFS | 4510 | 3682 | 1571 | 650 | 77971 | 2208 |
| CMS | 128 | 104 | 44 | 18 | 2208 | 4.64 |
| INCHES | | 6.67 | 4.49 | 4.64 | 117.82 | 3222 |
| MM | | 66.77 | 113.94 | 117.82 | 3222 | 3774 |
| AC-FT | | 1826 | 3116 | 3222 | 3774 | |

HYDROGRAPH AT STA 1 FOR PLAN 1, RTID 4[illegible]

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|--------|------|--------|---------|---------|--------------|
| GRS | 4661 | 3803 | 1623 | 671 | 80370 |
| CMB | 132 | 108 | 46 | 19 | 2281 |
| INCHES | | 2.72 | 4.64 | 4.77 | 4.77 |
| MM | | 69.00 | 117.74 | 121.75 | 121.75 |
| AC-FT | | 1837 | 3230 | 3387 | 3387 |
| CU-M | | 2327 | 3371 | 4107 | 4107 |

HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 5[illegible]

[illegible]

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|-------|--------|---------|---------|---------|--------|
| CPS | 7517. | 6137. | 2618. | 1083. | 187751. | |
| CHS | 213. | 174. | 74. | 31. | 3680. | |
| INCHES | | 4.38 | 7.48 | 7.73 | | |
| MM | | 111.28 | 189.90 | 196.37 | | |
| AC-FT | | 3043. | 3193. | 3370. | | |
| AC-M | | 7794. | 8405. | 8624. | | |
| | | | | | | 196.37 |
| | | | | | | 5370. |
| | | | | | | 8624. |

| HYDROGRAPH AT STA | 1 FOR PLAN | 11 | RTIO | 9 |
|-------------------|------------|----|------|-----|
| 24 | 21 | 21 | 104 | 187 |
| 25 | 22 | 22 | 104 | 187 |
| 26 | 23 | 23 | 104 | 187 |
| 27 | 24 | 24 | 104 | 187 |
| 28 | 25 | 25 | 104 | 187 |
| 29 | 26 | 26 | 104 | 187 |
| 30 | 27 | 27 | 104 | 187 |
| 31 | 28 | 28 | 104 | 187 |
| 32 | 29 | 29 | 104 | 187 |
| 33 | 30 | 30 | 104 | 187 |
| 34 | 31 | 31 | 104 | 187 |
| 35 | 32 | 32 | 104 | 187 |
| 36 | 33 | 33 | 104 | 187 |
| 37 | 34 | 34 | 104 | 187 |
| 38 | 35 | 35 | 104 | 187 |
| 39 | 36 | 36 | 104 | 187 |
| 40 | 37 | 37 | 104 | 187 |
| 41 | 38 | 38 | 104 | 187 |
| 42 | 39 | 39 | 104 | 187 |
| 43 | 40 | 40 | 104 | 187 |
| 44 | 41 | 41 | 104 | 187 |
| 45 | 42 | 42 | 104 | 187 |
| 46 | 43 | 43 | 104 | 187 |
| 47 | 44 | 44 | 104 | 187 |
| 48 | 45 | 45 | 104 | 187 |
| 49 | 46 | 46 | 104 | 187 |
| 50 | 47 | 47 | 104 | 187 |
| 51 | 48 | 48 | 104 | 187 |
| 52 | 49 | 49 | 104 | 187 |
| 53 | 50 | 50 | 104 | 187 |
| 54 | 51 | 51 | 104 | 187 |
| 55 | 52 | 52 | 104 | 187 |
| 56 | 53 | 53 | 104 | 187 |
| 57 | 54 | 54 | 104 | 187 |
| 58 | 55 | 55 | 104 | 187 |
| 59 | 56 | 56 | 104 | 187 |
| 60 | 57 | 57 | 104 | 187 |
| 61 | 58 | 58 | 104 | 187 |
| 62 | 59 | 59 | 104 | 187 |
| 63 | 60 | 60 | 104 | 187 |
| 64 | 61 | 61 | 104 | 187 |
| 65 | 62 | 62 | 104 | 187 |
| 66 | 63 | 63 | 104 | 187 |
| 67 | 64 | 64 | 104 | 187 |
| 68 | 65 | 65 | 104 | 187 |
| 69 | 66 | 66 | 104 | 187 |
| 70 | 67 | 67 | 104 | 187 |
| 71 | 68 | 68 | 104 | 187 |
| 72 | 69 | 69 | 104 | 187 |
| 73 | 70 | 70 | 104 | 187 |
| 74 | 71 | 71 | 104 | 187 |
| 75 | 72 | 72 | 104 | 187 |
| 76 | 73 | 73 | 104 | 187 |
| 77 | 74 | 74 | 104 | 187 |
| 78 | 75 | 75 | 104 | 187 |
| 79 | 76 | 76 | 104 | 187 |
| 80 | 77 | 77 | 104 | 187 |
| 81 | 78 | 78 | 104 | 187 |
| 82 | 79 | 79 | 104 | 187 |
| 83 | 80 | 80 | 104 | 187 |
| 84 | 81 | 81 | 104 | 187 |
| 85 | 82 | 82 | 104 | 187 |
| 86 | 83 | 83 | 104 | 187 |
| 87 | 84 | 84 | 104 | 187 |
| 88 | 85 | 85 | 104 | 187 |
| 89 | 86 | 86 | 104 | 187 |
| 90 | 87 | 87 | 104 | 187 |
| 91 | 88 | 88 | 104 | 187 |
| 92 | 89 | 89 | 104 | 187 |
| 93 | 90 | 90 | 104 | 187 |
| 94 | 91 | 91 | 104 | 187 |
| 95 | 92 | 92 | 104 | 187 |
| 96 | 93 | 93 | 104 | 187 |
| 97 | 94 | 94 | 104 | 187 |
| 98 | 95 | 95 | 104 | 187 |
| 99 | 96 | 96 | 104 | 187 |
| 100 | 97 | 97 | 104 | 187 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | TOTAL VOLUME |
|--------|-------|--------|---------|---------|--------|--------------|
| CFS | 19034 | 12274 | 5238 | 2166 | 35902 | 35902 |
| CMS | 426 | 349 | 148 | 61 | 7360 | 7360 |
| INCHES | | 8 | 14.95 | 15.46 | 15.46 | 15.46 |
| MM | | 222 | 379.80 | 392.74 | 392.74 | 392.74 |
| AC.FT | | 6086 | 10386 | 10740 | 10740 | 10740 |
| AC.FT | | 7507 | 12811 | 13247 | 13247 | 13247 |

南京城市圈发展研究

武吉知馬新加坡新加坡

100

1

COMPACT HYDROGRAPH

| DATE | TIME | NAME | STAGE | UNIT |
|------------------------------|------|------|-------|------|
| COMBINE 2 INFLOW HYDROGRAPHS | | | | |

[illegible]

#QVF#

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(F)

[illegible]

PAGE 0020

FLAHERTY GIAVARA ASSOCIATES, P. C.

361
371
381
391
401
411
421
431
441
451
461
471
481
491
501
511
521
531
541
551
561
571
581
591
601
611
621
631
641
651
661
671
681
691
701
711
721
731
741
751
761
771
781
791
801
811
821
831
841
851
861
871
881
891
901
911
921
931
941
951
961
971
981
991

FLAHERTY GIOVANA ASSOCIATES, P. C.

23 00 94.
23 30 93.
0 30 96.
0 30 97.
1 30 98.
1 30 99.
2 00 100.
2 30 101.
3 30 102.
4 30 103.
4 30 104.
4 30 105.
5 30 106.
5 30 107.
6 30 108.
6 30 109.
7 30 110.
7 30 111.
8 30 112.
8 30 113.
9 30 114.
9 30 115.
10 00 116.
10 30 117.
11 00 118.
11 30 119.
12 00 120.

DNV

21
14
10
9
11
12
130
1030
2539
9432
3165
1082

20
13
10
9
11
18
134
1148
6833
8723
2819
1039

SUM OF 2 HYDROGRAPHS AT
19 18
13 12
9 11
10 9
27 38
177 260
1234 1402
8131 9374
7827 6886
2902 6923
998 938

PEAK
11591
328

CFS
CMS
INCHES
MM
AC-FT
THOUS CU M

6-HOUR
9760
2764
244
6255
4840
5970

24-HOUR
4319
122
456
110.71
8566
10566

72-HOUR
1784
450
114.31
8843
10910

TOTAL VOLUME
214053
6041
450
114.31
8843
10910

STATION 1

DNV

4 30 571
5 30 581
6 30 591
7 30 601
8 30 611
9 30 621
10 30 631
11 30 641
12 30 651
13 30 661
14 30 671
15 30 681
16 30 691
17 30 701
18 30 711
19 30 721
20 30 731
21 30 741
22 30 751
23 30 761
24 30 771
25 30 781
26 30 791
27 30 801
28 30 811
29 30 821
30 30 831
31 30 841
32 30 851
33 30 861
34 30 871
35 30 881
36 30 891
37 30 901
38 30 911
39 30 921
40 30 931
41 30 941
42 30 951
43 30 961
44 30 971
45 30 981
46 30 991
47 30 1001
48 30 1011
49 30 1021
50 30 1031
51 30 1041
52 30 1051
53 30 1061
54 30 1071
55 30 1081
56 30 1091
57 30 1101
58 30 1111
59 30 1121
60 30 1131
61 30 1141

FLAHERTY GIOVARA ASSOCIATES, P. C.

9 30113
10 30116
11 30117
12 30118
13 30119
14 30120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 3 | |
|-------------------------|------|--------|-------|--------|-------|
| 20 | 21 | 17 | 18 | 16 | 15 |
| 13 | 14 | 12 | 13 | 11 | 10 |
| 10 | 11 | 9 | 10 | 9 | 8 |
| 10 | 10 | 12 | 11 | 12 | 12 |
| 11 | 11 | 10 | 10 | 7 | 7 |
| 28 | 12 | 80 | 66 | 94 | 107 |
| 249 | 133 | 383 | 462 | 713 | 845 |
| 1491 | 1086 | 2427 | 1774 | 2786 | 3666 |
| 9697 | 5730 | 11991 | 11388 | 11985 | 10863 |
| 7327 | 9964 | 5137 | 3748 | 4394 | 3671 |
| 2387 | 3276 | 1597 | 1784 | 1447 | 1193 |
| 1032 | 1119 | 8767 | 914 | 1443 | 1777 |
| 1073 | | 8767 | 914 | 1443 | 1777 |

CFB
CHS
INCHES
AC-FT
THOUS CU M

PEAK
11991
340
2895
470
5006
6175

24-HOUR
4468
127
451
11452
8862
10930

72-HOUR
1843
32
466
11825
9130
11287

TOTAL VOLUME
221434
6270
466
11825
9130
11287

OVF

STATION 1
INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(O*)
4000 6000 8000 10000 12000

0.11
1.1
2.1
3.1
4.1
5.1
6.1
7.1
8.1
9.1
10.1
11.1
12.1
13.1
14.1
15.1
16.1
17.1
18.1
19.1

PAGE 0028

FLAHERTY GIAVARA ASSOCIATES, P. C.

4111
4211
4311
4411
4511
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4711
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9011
9111
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9311
9411
9511
9611
9711
9811

FLAHERTY GIAVARA ASSOCIATES, P. C.

1 30.99
2 30.100
3 30.101
4 30.102
5 30.103
6 30.104
7 30.105
8 30.106
9 30.107
10 30.108
11 30.109
12 30.110
13 30.111
14 30.112
15 30.113
16 30.114
17 30.115
18 30.116
19 30.117
20 30.118
21 30.119
22 30.120

OVN

C-277

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 5 | | | |
|-------------------------|------------|------------|--------------|------------|------------|------------|--------------|
| 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 10769 | 4766 | 1788 | 236124 | 17 | 12 | 17 | 12 |
| 305 | 138 | 56 | 6488 | 12 | 12 | 12 | 12 |
| 2.72 | 4.81 | 4.97 | 4.97 | 12 | 12 | 12 | 12 |
| 69.02 | 122.14 | 129.14 | 129.14 | 12 | 12 | 12 | 12 |
| 5340 | 9432 | 7760 | 9760 | 12 | 12 | 12 | 12 |
| 6587 | 11659 | 12039 | 12039 | 12 | 12 | 12 | 12 |
| PEAK | PEAK | PEAK | PEAK | PEAK | PEAK | PEAK | PEAK |
| 12790 | 4766 | 1788 | 236124 | 17 | 12 | 17 | 12 |
| 362 | 138 | 56 | 6488 | 12 | 12 | 12 | 12 |
| CFS | CFS | CFS | CFS | CFS | CFS | CFS | CFS |
| INCHES | INCHES | INCHES | INCHES | INCHES | INCHES | INCHES | INCHES |
| MM | MM | MM | MM | MM | MM | MM | MM |
| AC-FT | AC-FT | AC-FT | AC-FT | AC-FT | AC-FT | AC-FT | AC-FT |
| THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M | THOUS CU M |

OVF

STATION 1

| INFLOW(1), OUTFLOW(0) AND OBSERVED FLOW(1) | | 14000 | | 0 | | 0 | |
|--|----|-------|---|---|---|---|---|
| 0 | 30 | 11 | 0 | 0 | 0 | 0 | 0 |
| 0 | 30 | 21 | 0 | 0 | 0 | 0 | 0 |
| 1 | 30 | 31 | 0 | 0 | 0 | 0 | 0 |

62
00 63
7 30 64
8 30 65
9 30 66
10 30 67
11 30 68
12 30 69
13 30 70
14 30 71
15 30 72
16 30 73
17 30 74
18 30 75
19 30 76
20 30 77
21 30 78
22 30 79
23 30 80
24 30 81
25 30 82
26 30 83
27 30 84
28 30 85
29 30 86
30 30 87
31 30 88
32 30 89
33 30 90
34 30 91
35 30 92
36 30 93
37 30 94
38 30 95
39 30 96
40 30 97
41 30 98
42 30 99
43 30 00
44 30 01
45 30 02
46 30 03
47 30 04
48 30 05
49 30 06
50 30 07
51 30 08
52 30 09
53 30 10
54 30 11
55 30 12
56 30 13
57 30 14
58 30 15
59 30 16
60 30 17
61 30 18
62 30 19

FLAHERTY OIIVARA ASSOCIATES, P. C.

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|
| 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 | 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 | 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 | 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 | 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 | 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 | 100 |
|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|-----|

17 30 83
18 30 84
19 30 85
20 30 86
21 30 87
22 30 88
23 30 89
24 30 90
25 30 91
26 30 92
27 30 93
28 30 94
29 30 95
30 30 96
31 30 97
32 30 98
33 30 99
34 30 100
35 30 101
36 30 102
37 30 103
38 30 104
39 30 105
40 30 106
41 30 107
42 30 108
43 30 109
44 30 110
45 30 111
46 30 112
47 30 113
48 30 114
49 30 115
50 30 116
51 30 117
52 30 118
53 30 119
54 30 120

DNV

| 24. | 23. | SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 7 | 18 | 17 |
|-----|-----|-------------------------|--------|--------|----|----|
| 12 | 16 | 22 | 20 | 12 | 18 | 17 |
| 13 | 11 | 19 | 10 | 10 | 12 | 12 |
| 14 | 11 | 11 | 10 | 10 | 10 | 10 |
| 15 | 11 | 12 | 10 | 10 | 10 | 10 |
| 16 | 11 | 11 | 10 | 10 | 10 | 10 |
| 17 | 11 | 11 | 10 | 10 | 10 | 10 |
| 18 | 11 | 11 | 10 | 10 | 10 | 10 |
| 19 | 11 | 11 | 10 | 10 | 10 | 10 |
| 20 | 11 | 11 | 10 | 10 | 10 | 10 |
| 21 | 11 | 11 | 10 | 10 | 10 | 10 |
| 22 | 11 | 11 | 10 | 10 | 10 | 10 |
| 23 | 11 | 11 | 10 | 10 | 10 | 10 |
| 24 | 11 | 11 | 10 | 10 | 10 | 10 |
| 25 | 11 | 11 | 10 | 10 | 10 | 10 |
| 26 | 11 | 11 | 10 | 10 | 10 | 10 |
| 27 | 11 | 11 | 10 | 10 | 10 | 10 |
| 28 | 11 | 11 | 10 | 10 | 10 | 10 |
| 29 | 11 | 11 | 10 | 10 | 10 | 10 |
| 30 | 11 | 11 | 10 | 10 | 10 | 10 |
| 31 | 11 | 11 | 10 | 10 | 10 | 10 |
| 32 | 11 | 11 | 10 | 10 | 10 | 10 |
| 33 | 11 | 11 | 10 | 10 | 10 | 10 |
| 34 | 11 | 11 | 10 | 10 | 10 | 10 |
| 35 | 11 | 11 | 10 | 10 | 10 | 10 |
| 36 | 11 | 11 | 10 | 10 | 10 | 10 |
| 37 | 11 | 11 | 10 | 10 | 10 | 10 |
| 38 | 11 | 11 | 10 | 10 | 10 | 10 |
| 39 | 11 | 11 | 10 | 10 | 10 | 10 |
| 40 | 11 | 11 | 10 | 10 | 10 | 10 |
| 41 | 11 | 11 | 10 | 10 | 10 | 10 |
| 42 | 11 | 11 | 10 | 10 | 10 | 10 |
| 43 | 11 | 11 | 10 | 10 | 10 | 10 |
| 44 | 11 | 11 | 10 | 10 | 10 | 10 |
| 45 | 11 | 11 | 10 | 10 | 10 | 10 |
| 46 | 11 | 11 | 10 | 10 | 10 | 10 |
| 47 | 11 | 11 | 10 | 10 | 10 | 10 |
| 48 | 11 | 11 | 10 | 10 | 10 | 10 |
| 49 | 11 | 11 | 10 | 10 | 10 | 10 |
| 50 | 11 | 11 | 10 | 10 | 10 | 10 |
| 51 | 11 | 11 | 10 | 10 | 10 | 10 |
| 52 | 11 | 11 | 10 | 10 | 10 | 10 |
| 53 | 11 | 11 | 10 | 10 | 10 | 10 |
| 54 | 11 | 11 | 10 | 10 | 10 | 10 |
| 55 | 11 | 11 | 10 | 10 | 10 | 10 |
| 56 | 11 | 11 | 10 | 10 | 10 | 10 |
| 57 | 11 | 11 | 10 | 10 | 10 | 10 |
| 58 | 11 | 11 | 10 | 10 | 10 | 10 |
| 59 | 11 | 11 | 10 | 10 | 10 | 10 |
| 60 | 11 | 11 | 10 | 10 | 10 | 10 |
| 61 | 11 | 11 | 10 | 10 | 10 | 10 |
| 62 | 11 | 11 | 10 | 10 | 10 | 10 |
| 63 | 11 | 11 | 10 | 10 | 10 | 10 |
| 64 | 11 | 11 | 10 | 10 | 10 | 10 |
| 65 | 11 | 11 | 10 | 10 | 10 | 10 |
| 66 | 11 | 11 | 10 | 10 | 10 | 10 |
| 67 | 11 | 11 | 10 | 10 | 10 | 10 |
| 68 | 11 | 11 | 10 | 10 | 10 | 10 |
| 69 | 11 | 11 | 10 | 10 | 10 | 10 |
| 70 | 11 | 11 | 10 | 10 | 10 | 10 |
| 71 | 11 | 11 | 10 | 10 | 10 | 10 |
| 72 | 11 | 11 | 10 | 10 | 10 | 10 |
| 73 | 11 | 11 | 10 | 10 | 10 | 10 |
| 74 | 11 | 11 | 10 | 10 | 10 | 10 |
| 75 | 11 | 11 | 10 | 10 | 10 | 10 |
| 76 | 11 | 11 | 10 | 10 | 10 | 10 |
| 77 | 11 | 11 | 10 | 10 | 10 | 10 |
| 78 | 11 | 11 | 10 | 10 | 10 | 10 |
| 79 | 11 | 11 | 10 | 10 | 10 | 10 |
| 80 | 11 | 11 | 10 | 10 | 10 | 10 |
| 81 | 11 | 11 | 10 | 10 | 10 | 10 |
| 82 | 11 | 11 | 10 | 10 | 10 | 10 |
| 83 | 11 | 11 | 10 | 10 | 10 | 10 |
| 84 | 11 | 11 | 10 | 10 | 10 | 10 |
| 85 | 11 | 11 | 10 | 10 | 10 | 10 |
| 86 | 11 | 11 | 10 | 10 | 10 | 10 |
| 87 | 11 | 11 | 10 | 10 | 10 | 10 |
| 88 | 11 | 11 | 10 | 10 | 10 | 10 |
| 89 | 11 | 11 | 10 | 10 | 10 | 10 |
| 90 | 11 | 11 | 10 | 10 | 10 | 10 |
| 91 | 11 | 11 | 10 | 10 | 10 | 10 |
| 92 | 11 | 11 | 10 | 10 | 10 | 10 |
| 93 | 11 | 11 | 10 | 10 | 10 | 10 |
| 94 | 11 | 11 | 10 | 10 | 10 | 10 |
| 95 | 11 | 11 | 10 | 10 | 10 | 10 |
| 96 | 11 | 11 | 10 | 10 | 10 | 10 |
| 97 | 11 | 11 | 10 | 10 | 10 | 10 |
| 98 | 11 | 11 | 10 | 10 | 10 | 10 |
| 99 | 11 | 11 | 10 | 10 | 10 | 10 |
| 100 | 11 | 11 | 10 | 10 | 10 | 10 |
| 101 | 11 | 11 | 10 | 10 | 10 | 10 |
| 102 | 11 | 11 | 10 | 10 | 10 | 10 |
| 103 | 11 | 11 | 10 | 10 | 10 | 10 |
| 104 | 11 | 11 | 10 | 10 | 10 | 10 |
| 105 | 11 | 11 | 10 | 10 | 10 | 10 |
| 106 | 11 | 11 | 10 | 10 | 10 | 10 |
| 107 | 11 | 11 | 10 | 10 | 10 | 10 |
| 108 | 11 | 11 | 10 | 10 | 10 | 10 |
| 109 | 11 | 11 | 10 | 10 | 10 | 10 |
| 110 | 11 | 11 | 10 | 10 | 10 | 10 |
| 111 | 11 | 11 | 10 | 10 | 10 | 10 |
| 112 | 11 | 11 | 10 | 10 | 10 | 10 |
| 113 | 11 | 11 | 10 | 10 | 10 | 10 |
| 114 | 11 | 11 | 10 | 10 | 10 | 10 |
| 115 | 11 | 11 | 10 | 10 | 10 | 10 |
| 116 | 11 | 11 | 10 | 10 | 10 | 10 |
| 117 | 11 | 11 | 10 | 10 | 10 | 10 |
| 118 | 11 | 11 | 10 | 10 | 10 | 10 |
| 119 | 11 | 11 | 10 | 10 | 10 | 10 |
| 120 | 11 | 11 | 10 | 10 | 10 | 10 |

CFS
 CFS
 INCHES
 AC-FT
 THOUS CU YD

PEAK
 13589
 385

6-HOUR
 11443
 324
 289
 73.33
 5474
 4999

24-HOUR
 5063
 143
 511
 127.79
 10043
 12388

72-HOUR
 2091
 57
 528
 134.02
 10370
 12791

TOTAL VOLUME
 250958
 7104
 528
 134.02
 10370
 12791

DNF

STATION 1

INFLW(1), OUTFLW(1) AND OBSERVED FLOW(1)

4000. 2000. 8000. 10000. 12000. 14000. 0. 0. 0. 0. 0.

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• DVF •

C-288

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C-298

SDVNS

***** SUB-AREA RUNOFF COMPUTATION *****

INFLOW HYDROGRAPH - SUBWATERSHED NO. 3
ISTAG 1 ICOMP 0 IECON 0 ITAPE 0 JPLT 0 JPRT 0 INAME 1 ISTAGE 0 IAUFD 0

IHYDQ 1 IUNG 1 TAREA 17.47 SNAP 0.00 HYDROGRAPH DATA
TRSDA 17.47 TRSPC 0.00 RATIO 0.000 ISNOW 0 ISAME 1 LDCAL 0

SPFE 0.00 PHS 17.30 R6 86.00 R12 100.00 R24 112.00 R48 119.00 R72 0.00 R96 0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.819

LOSS DATA

| LRDPT | STRKR | DLTKR | RTIOL | ERAIN | STAKS | RTICK | STATL | CNSTL | ALSNX | RTIMP |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 0.10 | 0.00 | 0.01 |

UNIT HYDROGRAPH DATA
TP= 9.76 CP=0.63 NTA= 0

APPROXIMATE CLARK COEFFICIENTS FROM
GIVEN SNYDER CP STR10=-2.00 RTIOR= 1.50
AND TP ARE GRCSN=-0.10 TC=12.86 AND N=10.42 INTERVALS
RECESSION DATA

| UNIT HYDROGRAPH | 43 | END-OF-PERIOD | ORDINATES, LAOS | 5.72 | HOURS, CP | 0.43 | VDL | 1.00 |
|-----------------|-----|---------------|-----------------|------|-----------|------|------|------|
| 1218 | 20 | 1218 | 1218 | 84 | 1013 | 1218 | 1218 | 1218 |
| 1215 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1212 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1209 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1206 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1203 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1200 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1197 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1194 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1191 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1188 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1185 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1182 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1179 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1176 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1173 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1170 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1167 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1164 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1161 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1158 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1155 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1152 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1149 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1146 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1143 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1140 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1137 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1134 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1131 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1128 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1125 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1122 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1119 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1116 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1113 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1110 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1107 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1104 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1101 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1098 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1095 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1092 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1089 | 146 | 146 | 146 | 84 | 1013 | 146 | 146 | 146 |
| 1086 | 146 | 146 | 146 | 84 | 1013 | 146 | | |

[illegible]

#DVF*

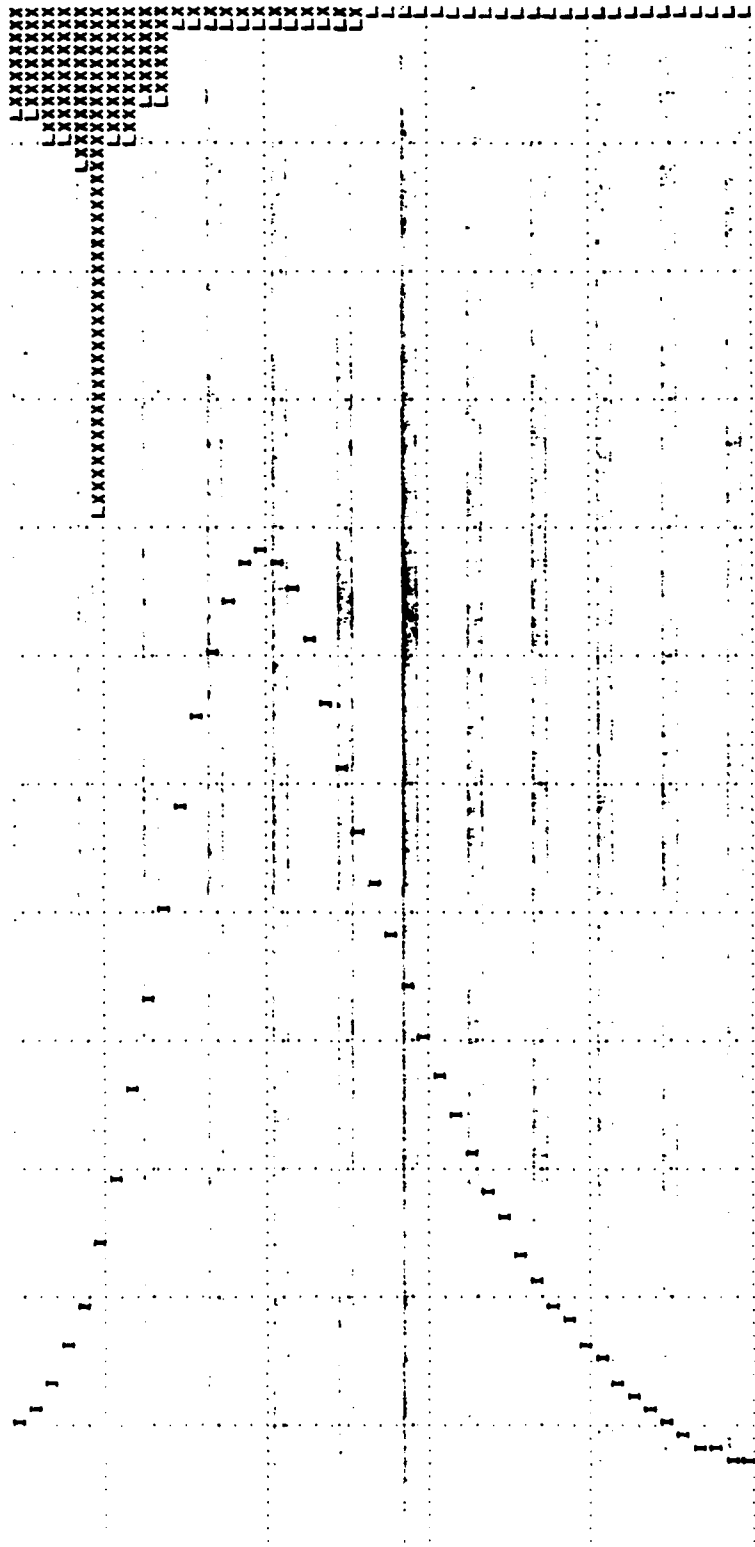
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FLAHERTY GIAVARA ASSOCIATES, P. C.

PAGE 0045

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DWN

HYDROGRAPH AT STA

7. 6.4 3.3 3.3 3.4

1 FOR PLAN 1, RTIO 1

6.4 3.3 3.3 3.3 10. 12. 15. 18. 22.

[illegible]

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| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 5 | | | | | | | | TOTAL VOLUME | |
|-------------------|---|----------------------|---|---|---|---|---|---|---|--------------|--|
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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| 10 | 9 | 8 | 7 | 6 | 5 | 4 | 3 | 2 | 1 | 0 | |
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FLAHERTY GIAVARA ASSOCIATES, P. C.

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OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | MTID 2 | |
|-------------------------|-------|--------|--------|--------|--------|
| 29 | 30 | 25 | 26 | 23 | 24 |
| 20 | 21 | 17 | 18 | 16 | 17 |
| 14 | 15 | 13 | 14 | 12 | 13 |
| 13 | 14 | 12 | 13 | 11 | 12 |
| 16 | 17 | 15 | 16 | 14 | 15 |
| 24 | 25 | 22 | 23 | 21 | 22 |
| 203 | 21 | 18 | 19 | 17 | 18 |
| 1329 | 1384 | 1286 | 1371 | 1286 | 1371 |
| 8912 | 9324 | 8843 | 9258 | 8843 | 9258 |
| 13047 | 14094 | 12781 | 13796 | 12781 | 13796 |
| 4764 | 5292 | 3444 | 3845 | 3444 | 3845 |
| 1804 | 1924 | 1493 | 1589 | 1493 | 1589 |
| PEAK | 15890 | 13411 | 14833 | 13411 | 14833 |
| CFB | 450 | 385 | 473 | 385 | 473 |
| CMB | 233 | 233 | 233 | 233 | 233 |
| INCHES | 27.18 | 107.27 | 128.65 | 107.27 | 128.65 |
| AC-FT | 6747 | 12462 | 15846 | 12462 | 15846 |
| THOUS CU YD | 8325 | 15371 | 19846 | 15371 | 19846 |

C-301

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STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(I+O)

| 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 0 | 0 | 0 | 0 |
|------|------|------|------|-------|-------|-------|-------|---|---|---|---|
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OVN

SUM OF 2 HYDROGRAPHS AT
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21 20
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PLAN 1 RTIO 3
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FLAHERTY GIOVARA ASSOCIATES, P. C.

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17 17
17 17
28 28
220 220
1834 1834
9526 9526
13747 13747
3094 3094
1929 1929

SUM OF 2 HYDROGRAPHS AT
20 20
20 20
14 14
14 14
14 14
14 14
37 37
279 279
1809 1809
13557 13557
12750 12750
4580 4580
1807 1807

1 PLAN 1 RT10.3
27 27
10 10
14 14
13 13
13 13
87 87
617 617
2764 2764
15976 15976
9442 9442
3294 3294
1501 1501

23 23
17 17
13 13
10 10
11 11
126 126
453 453
4076 4076
16986 16986
7695 7695
2697 2697
1343 1343

24 24
13 13
10 10
11 11
114 114
1134 1134
1780 1780
18729 18729
6748 6748
2449 2449
1290 1290

6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
14350 6716 2769 33233
481 190 78 910
2 49 4 60 4 74
63 27 116 81 120 42
7215 13321 13732 16939
8899 16431 16939

CFB
CFB
INCHES
AC-FT
THOUS CU H

DVE

STATION 1
INFLW(1), OUTFLOW(0) AND OBSERVED FLOW(1)

| | 2000. | 4000. | 6000. | 8000. | 10000. | 12000. | 14000. | 16000. | 18000. | 0. | 0. | 0. | 0. |
|----|-------|-------|-------|-------|--------|--------|--------|--------|--------|----|----|----|----|
| 0 | 11 | | | | | | | | | | | | |
| 1 | 23 | | | | | | | | | | | | |
| 2 | 31 | | | | | | | | | | | | |
| 3 | 44 | | | | | | | | | | | | |
| 4 | 51 | | | | | | | | | | | | |
| 5 | 61 | | | | | | | | | | | | |
| 6 | 71 | | | | | | | | | | | | |
| 7 | 81 | | | | | | | | | | | | |
| 8 | 91 | | | | | | | | | | | | |
| 9 | 10 | | | | | | | | | | | | |
| 10 | 11 | | | | | | | | | | | | |
| 11 | 12 | | | | | | | | | | | | |
| 12 | 13 | | | | | | | | | | | | |
| 13 | 14 | | | | | | | | | | | | |
| 14 | 15 | | | | | | | | | | | | |
| 15 | 16 | | | | | | | | | | | | |
| 16 | 17 | | | | | | | | | | | | |
| 17 | 18 | | | | | | | | | | | | |
| 18 | 19 | | | | | | | | | | | | |
| 19 | 20 | | | | | | | | | | | | |
| 20 | 21 | | | | | | | | | | | | |
| 21 | 22 | | | | | | | | | | | | |
| 22 | 23 | | | | | | | | | | | | |
| 23 | 24 | | | | | | | | | | | | |
| 24 | 25 | | | | | | | | | | | | |
| 25 | 26 | | | | | | | | | | | | |
| 26 | 27 | | | | | | | | | | | | |
| 27 | 28 | | | | | | | | | | | | |
| 28 | 29 | | | | | | | | | | | | |
| 29 | 30 | | | | | | | | | | | | |
| 30 | 31 | | | | | | | | | | | | |
| 31 | 32 | | | | | | | | | | | | |
| 32 | 33 | | | | | | | | | | | | |
| 33 | 34 | | | | | | | | | | | | |
| 34 | 35 | | | | | | | | | | | | |
| 35 | 36 | | | | | | | | | | | | |
| 36 | 37 | | | | | | | | | | | | |
| 37 | 38 | | | | | | | | | | | | |
| 38 | 39 | | | | | | | | | | | | |
| 39 | 40 | | | | | | | | | | | | |
| 40 | 41 | | | | | | | | | | | | |
| 41 | 42 | | | | | | | | | | | | |
| 42 | 43 | | | | | | | | | | | | |
| 43 | 44 | | | | | | | | | | | | |
| 44 | 45 | | | | | | | | | | | | |
| 45 | 46 | | | | | | | | | | | | |
| 46 | 47 | | | | | | | | | | | | |
| 47 | 48 | | | | | | | | | | | | |
| 48 | 49 | | | | | | | | | | | | |
| 49 | 50 | | | | | | | | | | | | |
| 50 | 51 | | | | | | | | | | | | |
| 51 | 52 | | | | | | | | | | | | |
| 52 | 53 | | | | | | | | | | | | |
| 53 | 54 | | | | | | | | | | | | |
| 54 | 55 | | | | | | | | | | | | |
| 55 | 56 | | | | | | | | | | | | |
| 56 | 57 | | | | | | | | | | | | |
| 57 | 58 | | | | | | | | | | | | |
| 58 | 59 | | | | | | | | | | | | |
| 59 | 60 | | | | | | | | | | | | |
| 60 | 61 | | | | | | | | | | | | |
| 61 | 62 | | | | | | | | | | | | |
| 62 | 63 | | | | | | | | | | | | |
| 63 | 64 | | | | | | | | | | | | |
| 64 | 65 | | | | | | | | | | | | |
| 65 | 66 | | | | | | | | | | | | |
| 66 | 67 | | | | | | | | | | | | |
| 67 | 68 | | | | | | | | | | | | |
| 68 | 69 | | | | | | | | | | | | |
| 69 | 70 | | | | | | | | | | | | |
| 70 | 71 | | | | | | | | | | | | |
| 71 | 72 | | | | | | | | | | | | |
| 72 | 73 | | | | | | | | | | | | |
| 73 | 74 | | | | | | | | | | | | |
| 74 | 75 | | | | | | | | | | | | |
| 75 | 76 | | | | | | | | | | | | |
| 76 | 77 | | | | | | | | | | | | |
| 77 | 78 | | | | | | | | | | | | |
| 78 | 79 | | | | | | | | | | | | |
| 79 | 80 | | | | | | | | | | | | |
| 80 | 81 | | | | | | | | | | | | |
| 81 | 82 | | | | | | | | | | | | |
| 82 | 83 | | | | | | | | | | | | |
| 83 | 84 | | | | | | | | | | | | |
| 84 | 85 | | | | | | | | | | | | |
| 85 | 86 | | | | | | | | | | | | |
| 86 | 87 | | | | | | | | | | | | |
| 87 | 88 | | | | | | | | | | | | |
| 88 | 89 | | | | | | | | | | | | |
| 89 | 90 | | | | | | | | | | | | |
| 90 | 91 | | | | | | | | | | | | |
| 91 | 92 | | | | | | | | | | | | |
| 92 | 93 | | | | | | | | | | | | |
| 93 | 94 | | | | | | | | | | | | |
| 94 | 95 | | | | | | | | | | | | |
| 95 | 96 | | | | | | | | | | | | |
| 96 | 97 | | | | | | | | | | | | |
| 97 | 98 | | | | | | | | | | | | |
| 98 | 99 | | | | | | | | | | | | |
| 99 | 100 | | | | | | | | | | | | |

FLAHERTY CIAVARA ASSOCIATES, P. C.

55 00 30 58
56 00 30 59
57 00 30 60
58 00 30 61
59 00 30 62
60 00 30 63
61 00 30 64
62 00 30 65
63 00 30 66
64 00 30 67
65 00 30 68
66 00 30 69
67 00 30 70
68 00 30 71
69 00 30 72
70 00 30 73
71 00 30 74
72 00 30 75
73 00 30 76
74 00 30 77
75 00 30 78
76 00 30 79
77 00 30 80
78 00 30 81
79 00 30 82
80 00 30 83
81 00 30 84
82 00 30 85
83 00 30 86
84 00 30 87
85 00 30 88
86 00 30 89
87 00 30 90
88 00 30 91
89 00 30 92
90 00 30 93
91 00 30 94
92 00 30 95
93 00 30 96
94 00 30 97
95 00 30 98
96 00 30 99
97 00 00 00
98 00 00 01
99 00 00 02
00 00 00 03
01 00 00 04
02 00 00 05
03 00 00 06
04 00 00 07
05 00 00 08
06 00 00 09
07 00 00 10
08 00 00 11
09 00 00 12
10 00 00 13
11 00 00 14
12 00 00 15

16037 14846 13573 12311 11130 10031 9073 8191 7396 6677
5022 4875 4675 4375 3919 3506 3162 2871 2607 2369
2190 1926 1809 1809 1699 1598 1504 1430 1373 1318

PEAK 18052 15487 7149 2948 35373
CFS 437 202 83 10917
CMBS 2.65 4.70 5.05
INCHES 67.35 124.35 128.18
AC-FT 7680 14181 14618
THOUS CU M 9474 17491 18031

6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
15487 7149 2948 35373
437 202 83 10917
2.65 4.70 5.05
67.35 124.35 128.18
7680 14181 14618
9474 17491 18031

DVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(S)

2000 4000 6000 8000 10000 12000 14000 16000 18000 20000 0

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41

21 00 421
 21 00 431
 22 00 441
 22 00 451
 22 00 461
 22 00 471
 22 00 481
 22 00 491
 22 00 501
 22 00 511
 22 00 521
 22 00 531
 22 00 541
 22 00 551
 22 00 561
 22 00 571
 22 00 581
 22 00 591
 22 00 601
 22 00 611
 22 00 621
 22 00 631
 22 00 641
 22 00 651
 22 00 661
 22 00 671
 22 00 681
 22 00 691
 22 00 701
 22 00 711
 22 00 721
 22 00 731
 22 00 741
 22 00 751
 22 00 761
 22 00 771
 22 00 781
 22 00 791
 22 00 801
 22 00 811
 22 00 821
 22 00 831
 22 00 841
 22 00 851
 22 00 861
 22 00 871
 22 00 881
 22 00 891
 22 00 901
 22 00 911
 22 00 921
 22 00 931
 22 00 941
 22 00 951
 22 00 961
 22 00 971
 22 00 981
 22 00 991

FLAHERTY GIAVARA ASSOCIATES, P.C.

2 00100
3 00101
4 00102
5 00103
6 00104
7 00105
8 00106
9 00107
10 00108
11 00109
12 00110
13 00111
14 00112
15 00113
16 00114
17 00115
18 00116
19 00117
20 00118
21 00119
22 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 7 | |
|-------------------------|----|--------|----|--------|-----|
| 24 | 25 | 26 | 27 | 28 | 29 |
| 24 | 25 | 26 | 27 | 28 | 29 |
| 25 | 26 | 27 | 28 | 29 | 30 |
| 26 | 27 | 28 | 29 | 30 | 31 |
| 27 | 28 | 29 | 30 | 31 | 32 |
| 28 | 29 | 30 | 31 | 32 | 33 |
| 29 | 30 | 31 | 32 | 33 | 34 |
| 30 | 31 | 32 | 33 | 34 | 35 |
| 31 | 32 | 33 | 34 | 35 | 36 |
| 32 | 33 | 34 | 35 | 36 | 37 |
| 33 | 34 | 35 | 36 | 37 | 38 |
| 34 | 35 | 36 | 37 | 38 | 39 |
| 35 | 36 | 37 | 38 | 39 | 40 |
| 36 | 37 | 38 | 39 | 40 | 41 |
| 37 | 38 | 39 | 40 | 41 | 42 |
| 38 | 39 | 40 | 41 | 42 | 43 |
| 39 | 40 | 41 | 42 | 43 | 44 |
| 40 | 41 | 42 | 43 | 44 | 45 |
| 41 | 42 | 43 | 44 | 45 | 46 |
| 42 | 43 | 44 | 45 | 46 | 47 |
| 43 | 44 | 45 | 46 | 47 | 48 |
| 44 | 45 | 46 | 47 | 48 | 49 |
| 45 | 46 | 47 | 48 | 49 | 50 |
| 46 | 47 | 48 | 49 | 50 | 51 |
| 47 | 48 | 49 | 50 | 51 | 52 |
| 48 | 49 | 50 | 51 | 52 | 53 |
| 49 | 50 | 51 | 52 | 53 | 54 |
| 50 | 51 | 52 | 53 | 54 | 55 |
| 51 | 52 | 53 | 54 | 55 | 56 |
| 52 | 53 | 54 | 55 | 56 | 57 |
| 53 | 54 | 55 | 56 | 57 | 58 |
| 54 | 55 | 56 | 57 | 58 | 59 |
| 55 | 56 | 57 | 58 | 59 | 60 |
| 56 | 57 | 58 | 59 | 60 | 61 |
| 57 | 58 | 59 | 60 | 61 | 62 |
| 58 | 59 | 60 | 61 | 62 | 63 |
| 59 | 60 | 61 | 62 | 63 | 64 |
| 60 | 61 | 62 | 63 | 64 | 65 |
| 61 | 62 | 63 | 64 | 65 | 66 |
| 62 | 63 | 64 | 65 | 66 | 67 |
| 63 | 64 | 65 | 66 | 67 | 68 |
| 64 | 65 | 66 | 67 | 68 | 69 |
| 65 | 66 | 67 | 68 | 69 | 70 |
| 66 | 67 | 68 | 69 | 70 | 71 |
| 67 | 68 | 69 | 70 | 71 | 72 |
| 68 | 69 | 70 | 71 | 72 | 73 |
| 69 | 70 | 71 | 72 | 73 | 74 |
| 70 | 71 | 72 | 73 | 74 | 75 |
| 71 | 72 | 73 | 74 | 75 | 76 |
| 72 | 73 | 74 | 75 | 76 | 77 |
| 73 | 74 | 75 | 76 | 77 | 78 |
| 74 | 75 | 76 | 77 | 78 | 79 |
| 75 | 76 | 77 | 78 | 79 | 80 |
| 76 | 77 | 78 | 79 | 80 | 81 |
| 77 | 78 | 79 | 80 | 81 | 82 |
| 78 | 79 | 80 | 81 | 82 | 83 |
| 79 | 80 | 81 | 82 | 83 | 84 |
| 80 | 81 | 82 | 83 | 84 | 85 |
| 81 | 82 | 83 | 84 | 85 | 86 |
| 82 | 83 | 84 | 85 | 86 | 87 |
| 83 | 84 | 85 | 86 | 87 | 88 |
| 84 | 85 | 86 | 87 | 88 | 89 |
| 85 | 86 | 87 | 88 | 89 | 90 |
| 86 | 87 | 88 | 89 | 90 | 91 |
| 87 | 88 | 89 | 90 | 91 | 92 |
| 88 | 89 | 90 | 91 | 92 | 93 |
| 89 | 90 | 91 | 92 | 93 | 94 |
| 90 | 91 | 92 | 93 | 94 | 95 |
| 91 | 92 | 93 | 94 | 95 | 96 |
| 92 | 93 | 94 | 95 | 96 | 97 |
| 93 | 94 | 95 | 96 | 97 | 98 |
| 94 | 95 | 96 | 97 | 98 | 99 |
| 95 | 96 | 97 | 98 | 99 | 100 |

| PEAK | 5-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------|--------|---------|---------|--------------|
| 1850 | 15758 | 7366 | 3037 | 34483 |
| 528 | 452 | 209 | 86 | 10321 |
| | 2.73 | 5.04 | 2.20 | 10.17 |
| | 49.39 | 128.11 | 132.07 | 309.57 |
| | 7913 | 14610 | 13061 | 25584 |
| | 9761 | 18021 | 18578 | 36660 |

THOUS CU H

STATION 1

INFLW (1) OUTFLOW (2) AND OBSERVED FLOW (3)

4000 8000 12000 16000 20000

0 30 1.00 1.30 2

OVF

FLAHERTY GIAVARA ASSOCIATES, P. C.

7 30 63
8 30 64
9 30 65
10 30 66
11 30 67
12 30 68
13 30 69
14 30 70
15 30 71
16 30 72
17 30 73
18 30 74
19 30 75
20 30 76
21 30 77
22 30 78
23 30 79
24 30 80
25 30 81
26 30 82
27 30 83
28 30 84
29 30 85
30 30 86
31 30 87
32 30 88
33 30 89
34 30 90
35 30 91
36 30 92
37 30 93
38 30 94
39 30 95
40 30 96
41 30 97
42 30 98
43 30 99
44 30 100
45 30 101
46 30 102
47 30 103
48 30 104
49 30 105
50 30 106
51 30 107
52 30 108
53 30 109
54 30 110
55 30 111
56 30 112
57 30 113
58 30 114
59 30 115
60 30 116
61 30 117
62 30 118
63 30 119
64 30 120

FLAHERTY GIAVARA ASSOCIATES, P. C.

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 8 | |
|-------------------------|-------|--------|-------|--------|-------|
| 50. | 48. | 43. | 41. | 40. | 38. |
| 32 | 33 | 30 | 29 | 28 | 27 |
| 22 | 24 | 22 | 22 | 21 | 21 |
| 22 | 23 | 27 | 28 | 29 | 29 |
| 28 | 24 | 21 | 20 | 18 | 18 |
| 29 | 83 | 140 | 172 | 203 | 232 |
| 42 | 60 | 99 | 134 | 153 | 182 |
| 334 | 588 | 449 | 536 | 602 | 697 |
| 2634 | 3744 | 4439 | 5366 | 6032 | 6977 |
| 12304 | 21310 | 23768 | 26997 | 27394 | 25868 |
| 23299 | 18643 | 1747 | 12411 | 11202 | 10116 |
| 7124 | 1528 | 15239 | 4791 | 4350 | 3350 |
| 3318 | 2740 | 2321 | 2278 | 2080 | 1977 |

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|-------|--------|---------|---------|--------------|
| 27376 | 23468 | 10832 | 4987 | 53608 |
| 776 | 665 | 307 | 126 | 15178 |
| | 4.02 | 7.42 | 126 | 197.65 |
| | 102.04 | 186.40 | 194.22 | 22147 |
| | 11637 | 21486 | 22147 | 27320 |
| | 14354 | 26502 | 27320 | |

OVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| 4000. | 8000. | 12000. | 16000. | 20000. | 24000. | 28000. | 0. | 0. | 0. | 0. | 0. |
|-------|-------|--------|--------|--------|--------|--------|----|----|----|----|----|
|-------|-------|--------|--------|--------|--------|--------|----|----|----|----|----|

| | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------|-----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| 0.11 | 121 | 34 | 51 | 71 | 89 | 101 | 112 | 123 | 134 | 145 | 156 | 167 | 178 | 189 | 191 | 201 | 211 | 222 | 233 | 244 | 255 | 266 | 277 | 288 | 299 | 300 |
|------|-----|----|----|----|----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|

13 00 261
13 00 271
14 00 281
15 00 291
16 00 301
17 00 311
18 00 321
19 00 331
20 00 341
21 00 351
22 00 361
23 00 371
24 00 381
25 00 391
26 00 401
27 00 411
28 00 421
29 00 431
30 00 441
31 00 451
32 00 461
33 00 471
34 00 481
35 00 491
36 00 501
37 00 511
38 00 521
39 00 531
40 00 541
41 00 551
42 00 561
43 00 571
44 00 581
45 00 591
46 00 601
47 00 611
48 00 621
49 00 631
50 00 641
51 00 651
52 00 661
53 00 671
54 00 681
55 00 691
56 00 701
57 00 711
58 00 721
59 00 731
60 00 741
61 00 751
62 00 761
63 00 771
64 00 781
65 00 791
66 00 801
67 00 811
68 00 821
69 00 831
70 00 841
71 00 851
72 00 861
73 00 871
74 00 881
75 00 891
76 00 901
77 00 911
78 00 921
79 00 931
80 00 941
81 00 951
82 00 961
83 00 971
84 00 981
85 00 991

18 00 84.
18 30 85.
19 00 86.
19 30 87.
20 00 88.
20 30 89.
21 00 90.
21 30 91.
22 00 92.
22 30 93.
23 00 94.
23 30 95.
00 00 96.
00 30 97.
01 00 98.
01 30 99.
02 00 100.
02 30 101.
03 00 102.
03 30 103.
04 00 104.
04 30 105.
05 00 106.
05 30 107.
06 00 108.
06 30 109.
07 00 110.
07 30 111.
08 00 112.
08 30 113.
09 00 114.
09 30 115.
10 00 116.
10 30 117.
11 00 118.
11 30 119.
12 00 120.

C-319

DVN

| SUM OF 2 HYDROGRAPHS AT | 1 | PLAN 1 | RTIO 9 | 74 | 74 | 74 |
|-------------------------|-------|--------|--------|-------|-------|-------|
| 76 | 67 | 56 | 82 | 74 | 74 | 74 |
| 66 | 61 | 59 | 57 | 54 | 54 | 52 |
| 48 | 45 | 44 | 43 | 42 | 42 | 42 |
| 46 | 43 | 44 | 56 | 58 | 58 | 58 |
| 49 | 51 | 54 | 39 | 37 | 37 | 37 |
| 47 | 45 | 42 | 34 | 37 | 37 | 37 |
| 166 | 220 | 281 | 344 | 465 | 465 | 465 |
| 1175 | 1540 | 1990 | 2509 | 3074 | 3657 | 319 |
| 6522 | 7529 | 8918 | 10772 | 13150 | 16065 | 4232 |
| 42421 | 47574 | 51536 | 57993 | 64793 | 71764 | 19955 |
| 37305 | 33726 | 30457 | 27494 | 24821 | 22413 | 21237 |
| 13257 | 11876 | 10423 | 9381 | 8499 | 7701 | 20332 |
| 5481 | 5150 | 4842 | 4557 | 4332 | 4160 | 7180 |
| 5837 | | | | | | 3995 |

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME

104 100
71 68
50 47
43 44
54 54
58 83
588 708
4774 5271
25013 30730
48598 44989
18247 16434
6636 6221

23 30 477
00 481
00 491
1 501
2 511
3 521
3 531
3 541
4 551
4 561
5 571
5 581
6 591
6 601
7 611
7 621
8 631
8 641
9 651
9 661
00 671
00 681
00 691
00 701
00 711
00 721
00 731
00 741
00 751
00 761
00 771
00 781
00 791
00 801
00 811
00 821
00 831
00 841
00 851
00 861
00 871
00 881
00 891
00 901
00 911
00 921
00 931
00 941
00 951
00 961
00 971
00 981
00 991
00 1001
00 1011
00 1021
00 1031
00 1041

4.30109.
5.00106.
6.00107.
7.00108.
8.00109.
9.00110.
10.00111.
11.00112.
12.00113.
13.00114.
14.00115.
15.00116.
16.00117.
17.00118.
18.00119.
19.00120.



OVN

***** SUB-AREA RUNOFF COMPUTATION *****

INFLOW HYDROGRAPH - SUBWATERSHED NO. 4
ISTAG 1 ICOMP 0 ITAPE 0 UPLT 0 UPRT 0 INAME 1 ISTAGE 0 IAUTO 0

HYDQ 1 IUMP 1 TAREA 4.77 SNAP 0.00 TRSDA TRSFC RATIO ISNOW ISAME LOCAL 0

PRECIP DATA
R12 R24 R48 R72 R96
R48 112.00 119.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA
LRDPT 0 STRKR 0.00 DLTKR 0.00 RTIOL 1.00 ERAIN 0.00 STRKS 0.00 RTIOK 1.00 STRTL 1.00 CNSTL 0.10 ALSX 0.00 RTIMP 0.01

TP= 3.87 CP=0.83 NTA= 0

APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 8.75 AND R= 7.04 INTERVALS

UNIT HYDROGRAPH 42 END-OF-PERIOD ORDINATES, LAG= 3.87 HOURS, CP= 0.63 VOL= 1.00
32 384 82 165 289 251 334 488 493
334 334 80 170 289 251 334 488 493
22 22 19 17 13 11 46 34 38
5 5 5 5 5 5 5 5 5

XX

[illegible]

[illegible]

FLAHERTY GIAVARA ASSOCIATES, P. C.

CFS
CMS
INCHES
AC-FT
THOUS CU M

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 3 | | TOTAL VOLUME | |
|-------------------|--------|----------------------|---------|--------------|---------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | 24-HOUR | 72-HOUR |
| 1740 | 1421 | 605 | 250 | 3052 | |
| 17 | 40 | 172 | 4 88 | 172 | 88 |
| | 70.36 | 120.00 | 124.05 | 124.05 | |
| | 704 | 1201 | 1242 | 1242 | |
| | 869 | 1482 | 1532 | 1532 | |

CFS
CMS
INCHES
AC-FT
THOUS CU M

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 6 | | TOTAL VOLUME | |
|-------------------|--------|----------------------|---------|--------------|---------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | 24-HOUR | 72-HOUR |
| 1795 | 1465 | 625 | 259 | 3092 | |
| 51 | 41 | 18 | 3 04 | 18 | 88 |
| | 72.56 | 123.75 | 127.93 | 127.93 | |
| | 726 | 1239 | 1281 | 1281 | |
| | 896 | 1528 | 1580 | 1580 | |

CFS
CMS
INCHES
AC-FT
THOUS CU M

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 7 | | TOTAL VOLUME | |
|-------------------|--------|----------------------|---------|--------------|---------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | 24-HOUR | 72-HOUR |
| 1795 | 1465 | 625 | 259 | 3092 | |
| 51 | 41 | 18 | 3 04 | 18 | 88 |
| | 72.56 | 123.75 | 127.93 | 127.93 | |
| | 726 | 1239 | 1281 | 1281 | |
| | 896 | 1528 | 1580 | 1580 | |

CFS
CMS
INCHES
AC-FT
THOUS CU M

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 7 | | TOTAL VOLUME | |
|-------------------|--------|----------------------|---------|--------------|---------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | 24-HOUR | 72-HOUR |
| 1795 | 1465 | 625 | 259 | 3092 | |
| 51 | 41 | 18 | 3 04 | 18 | 88 |
| | 72.56 | 123.75 | 127.93 | 127.93 | |
| | 726 | 1239 | 1281 | 1281 | |
| | 896 | 1528 | 1580 | 1580 | |

CFS
CMS
INCHES
AC-FT
THOUS CU M

AD-A109 795

FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT
NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)
JUL 81 H C FLAHERTY

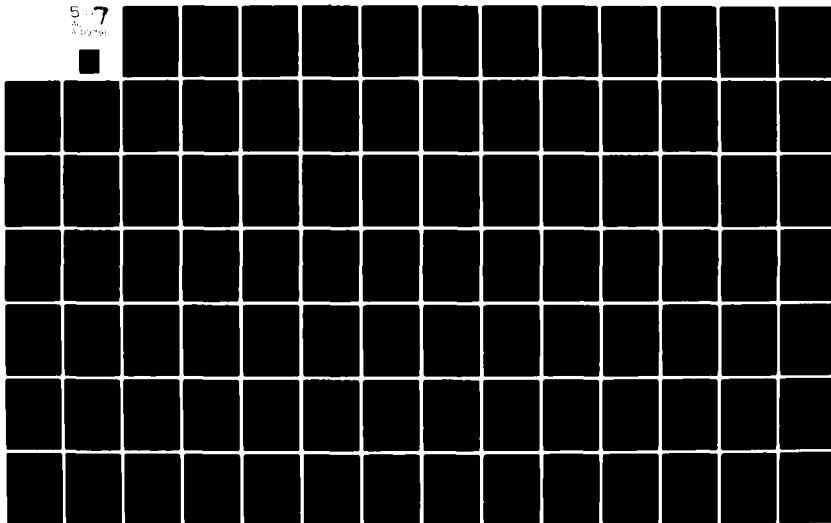
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DACW51-81-C-0006

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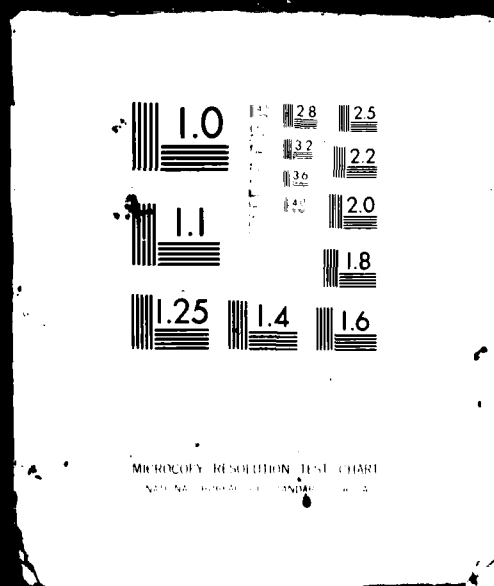
5-7
A-109



5 OF 7

AD-

A109795



CMS 154. 126 94 22 2659
 INCHES 8 66 14 76 15 26 15 26
 AC-FT 219 89 374 99 387 66 387 66
 THOUS CU M 2201 3754 4630 3881 4787

COMBINE HYDROGRAPHS

COMBINE 2 INFLOW HYDROGRAPHS IECON 0 ITAPE 0 JPLT 0 JPRT INAME IBTAGE I AUTO
 1 2 0 0 0 0 0 0

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 1 | | | |
|-------------------------|------|--------|------|---------|-------|--------------|-------|
| 23 | 22 | 21 | 20 | 19 | 18 | 17 | 16 |
| 11 | 11 | 14 | 14 | 13 | 12 | 12 | 11 |
| 10 | 10 | 10 | 10 | 10 | 10 | 10 | 10 |
| 12 | 12 | 11 | 11 | 10 | 10 | 10 | 10 |
| 13 | 13 | 11 | 11 | 10 | 10 | 10 | 10 |
| 129 | 153 | 198 | 260 | 342 | 442 | 558 | 683 |
| 1055 | 1162 | 1279 | 1436 | 1659 | 1968 | 2383 | 2914 |
| 5557 | 6826 | 8134 | 9407 | 10531 | 11379 | 11886 | 12017 |
| 10927 | 9715 | 8857 | 8016 | 7233 | 6522 | 5879 | 5300 |
| 3880 | 3489 | 3132 | 2805 | 2509 | 2241 | 2023 | 1842 |
| 1418 | 1331 | 1251 | 1176 | 1107 | 1042 | 982 | 935 |
| PEAK | | 9-HOUR | | 24-HOUR | | TOTAL VOLUME | |
| CFS | | 12017 | | 10254 | | 233184 | |
| CMS | | 340 | | 4711 | | 6603 | |
| INCHES | | 1 41 | | 133 | | 3 06 | |
| AC-FT | | 40 99 | | 2 97 | | 77 68 | |
| THOUS CU M | | 5085 | | 7344 | | 9636 | |
| | | 6272 | | 11326 | | 11885 | |

OVF

STATION

INFLOW(1), OUTFLOW(0) AND OBSERVED FLOW(0) 2000 4000 6000 8000 10000 12000

0 11 30 11 30 31 11 30 41 11 30 51 11 30 61 11 30 71 11 30 81 11 30 91 11 30 101 11 30 111 11 30 121 11 30 131

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FLAHERTY GIAVARA ASSOCIATES, P. C.

141
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7 30 141
8 30 171
9 30 181
10 30 201
11 30 211
12 30 221
13 30 231
14 30 241
15 30 251
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94 30 1041
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59 00 119
60 00 120

C-332

SUM OF 2 HYDROGRAPHS AT 1 PLAN 1 RTIO 2
20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

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FLAHERTY GIAVARA ASSOCIATES, P.C.

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8 00 601
9 00 611
10 00 621
11 00 631
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46 00 981
47 00 991
48 00 1001
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52 00 1041
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54 00 1061
55 00 1071
56 00 1081
57 00 1091
58 00 1101
59 00 1111
60 00 1121
61 00 1131

7 00114
7 30115
7 00116
7 30117
7 00118
7 30119
7 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTID 4 | |
|-------------------------|-------|--------|-------|--------|-------|
| 32 | 31 | 29 | 30 | 27 | 28 |
| 22 | 21 | 20 | 21 | 19 | 18 |
| 16 | 15 | 14 | 15 | 13 | 12 |
| 17 | 16 | 15 | 16 | 14 | 13 |
| 17 | 16 | 15 | 16 | 14 | 13 |
| 41 | 37 | 76 | 76 | 137 | 122 |
| 307 | 403 | 889 | 884 | 1357 | 1258 |
| 1782 | 2223 | 3051 | 3673 | 1517 | 1524 |
| 12608 | 14581 | 17638 | 18424 | 18626 | 19263 |
| 13729 | 12424 | 10109 | 9112 | 8216 | 7409 |
| 4854 | 4348 | 3473 | 3123 | 2601 | 2401 |
| 1939 | 1823 | 1616 | 1523 | 1449 | 1391 |
| 2197 | 2063 | | | | |

| PEAK | | 6-HOUR | | 24-HOUR | | 72-HOUR | | TOTAL VOLUME | |
|------|-------|--------|--------|---------|--------|---------|--------|--------------|--------|
| CFS | CHS | 15874 | 7302 | 7302 | 3012 | 3012 | 3012 | 3012 | 3012 |
| 527 | 450 | 207 | 85 | 207 | 85 | 207 | 85 | 207 | 85 |
| | 2.50 | 4.60 | 4.74 | 4.60 | 4.74 | 4.60 | 4.74 | 4.60 | 4.74 |
| | 63.93 | 116.76 | 120.40 | 116.76 | 120.40 | 116.76 | 120.40 | 116.76 | 120.40 |
| | 7881 | 14484 | 14933 | 14484 | 14933 | 14484 | 14933 | 14484 | 14933 |
| | 4722 | 17865 | 18422 | 17865 | 18422 | 17865 | 18422 | 17865 | 18422 |

OVF

STATION 1

| INFLW(I), OUTFLOW(O) AND OBSERVED FLOW(S) | | 4000 | | 6000 | | 8000 | | 10000 | | 12000 | | 14000 | | 16000 | | 18000 | | 20000 | |
|---|----|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|---|-------|---|-------|---|-------|---|
| 0 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 1 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 2 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 3 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 4 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 5 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 6 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 7 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 8 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 9 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 10 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 11 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 12 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 13 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 14 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 15 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 16 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 17 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 18 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 19 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 20 11 | 30 | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 20000 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

| | | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 1688. | 1850. | 2046. | 2277. | 2634. | 3147. | 3813. | 4662. | 5702. | 7090. |
| 8891. | 10922. | 13015. | 15031. | 16849. | 18207. | 19018. | 19227. | 18852. | 17999. |
| 16846. | 15945. | 14172. | 12825. | 11574. | 10435. | 9406. | 8481. | 7648. | 6894. |
| 4208. | 5583. | 5011. | 4488. | 4014. | 3585. | 3236. | 2947. | 2685. | 2448. |
| 2268. | 2130. | 2001. | 1882. | 1771. | 1668. | 1572. | 1495. | 1436. | 1379. |

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
 1927 16407 7538 3109 373094
 CFS 544 213 88 10565
 CMR 469 4 74 4 89
 INCHES 2.58 120.52 124.28
 AC-FT 65.58 14931 15417
 THOUS CU M 8136 18442 19017

OVF

STATION 1
 INFLOW(1), OUTFLOW(2) AND OBSERVED FLOW(3)

2000. 4000. 6000. 8000. 10000. 12000. 14000. 16000. 18000. 20000. 0. 0.

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39

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-C-343

*** QWERTY ***

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

88

31 41 51 61 71 81 91 101 111 121 131 141 151 161 171 181 191 201 211 221 231 241 251 261 271 281 291 301 311 321 331 341 351 361 371 381 391 401 411 421 431 441 451 461 471 481 491 501 511 521 531 541 551 561 571 581 591 601 611 621 631 641 651 661 671 681 691 701 711 721 731 741 751 761 771 781 791 801 811 821 831 841 851 861 871 881 891 901 911 921 931 941 951 961 971 981 991

FLAHERTY GIOVARA ASSOCIATES, P. C.

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7 30 63
8 30 64
9 30 65
10 30 66
11 30 67
12 30 68
13 30 69
14 30 70
15 30 71
16 30 72
17 30 73
18 30 74
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33 30 89
34 30 90
35 30 91
36 30 92
37 30 93
38 30 94
39 30 95
40 30 96
41 30 97
42 30 98
43 30 99
44 30 00
45 30 01
46 30 02
47 30 03
48 30 04
49 30 05
50 30 06
51 30 07
52 30 08
53 30 09
54 30 10
55 30 11
56 30 12
57 30 13
58 30 14
59 30 15
60 30 16

11. 30119.
12. 00120.

END

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 7 | |
|-------------------------|-------|--------|-------|--------|-------|
| 37 | 33 | 32 | 29 | 28 | 27 |
| 26 | 34 | 22 | 30 | 20 | 19 |
| 25 | 23 | 22 | 21 | 20 | 16 |
| 18 | 17 | 16 | 16 | 16 | 21 |
| 18 | 17 | 20 | 21 | 23 | 21 |
| 17 | 18 | 16 | 13 | 13 | 16 |
| 20 | 17 | 14 | 13 | 13 | 16 |
| 12 | 83 | 124 | 152 | 154 | 153 |
| 42 | 83 | 124 | 152 | 154 | 153 |
| 337 | 581 | 752 | 1161 | 1380 | 1523 |
| 1744 | 2820 | 4348 | 4456 | 6057 | 7123 |
| 13828 | 17402 | 20207 | 20429 | 20030 | 17123 |
| 15992 | 19345 | 20207 | 20429 | 20030 | 17123 |
| 13627 | 12347 | 9474 | 9011 | 8126 | 7361 |
| 4769 | 4263 | 3131 | 3131 | 2851 | 2601 |
| 2000 | 1882 | 1772 | 1587 | 1356 | 1465 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|--------|--------|---------|---------|---------|--------|
| CFR | 20429. | 17432. | 8009. | 3303. | 392413. | |
| CHB | 378. | 194. | 227. | 94. | 19263. | |
| INCHES | 2.78 | 2.78 | 5.04 | 5.20 | 5.20 | |
| MM | 49.68 | 128.05 | 128.05 | 132.05 | 132.05 | |
| AC-FT | 8444. | 15883. | 15883. | 16381. | 16381. | |
| THOUS | 10462. | 15574. | 20205. | 20205. | 20205. | |

♦♦♦♦♦

| STATION | 1 | INFLOW(I),
2000. | OUTFLOW(O),
4000. | AND OBSERVED FLOW(S),
6000. | 8000. | 10000. | 12000. | 14000. | 16000. | 18000. | 20000. | 22000. | 0. |
|---------|----|---------------------|----------------------|--------------------------------|-------|--------|--------|--------|--------|--------|--------|--------|----|
| 0.1 | 1 | | | | | | | | | | | | |
| 1.2 | 2 | | | | | | | | | | | | |
| 2.3 | 3 | | | | | | | | | | | | |
| 3.4 | 4 | | | | | | | | | | | | |
| 4.5 | 5 | | | | | | | | | | | | |
| 5.6 | 6 | | | | | | | | | | | | |
| 6.7 | 7 | | | | | | | | | | | | |
| 7.8 | 8 | | | | | | | | | | | | |
| 8.9 | 9 | | | | | | | | | | | | |
| 9.0 | 10 | | | | | | | | | | | | |
| 10.1 | 11 | | | | | | | | | | | | |
| 11.2 | 12 | | | | | | | | | | | | |
| 12.3 | 13 | | | | | | | | | | | | |
| 13.4 | 14 | | | | | | | | | | | | |
| 14.5 | 15 | | | | | | | | | | | | |
| 15.6 | 16 | | | | | | | | | | | | |
| 16.7 | 17 | | | | | | | | | | | | |
| 17.8 | 18 | | | | | | | | | | | | |
| 18.9 | 19 | | | | | | | | | | | | |
| 19.0 | 20 | | | | | | | | | | | | |
| 20.1 | 21 | | | | | | | | | | | | |
| 21.2 | 22 | | | | | | | | | | | | |
| 22.3 | 23 | | | | | | | | | | | | |
| 23.4 | 24 | | | | | | | | | | | | |
| 24.5 | 25 | | | | | | | | | | | | |
| 25.6 | 26 | | | | | | | | | | | | |
| 26.7 | 27 | | | | | | | | | | | | |
| 27.8 | 28 | | | | | | | | | | | | |
| 28.9 | 29 | | | | | | | | | | | | |
| 29.0 | 30 | | | | | | | | | | | | |
| 30.1 | 31 | | | | | | | | | | | | |
| 31.2 | 32 | | | | | | | | | | | | |
| 32.3 | 33 | | | | | | | | | | | | |
| 33.4 | 34 | | | | | | | | | | | | |
| 34.5 | 35 | | | | | | | | | | | | |
| 35.6 | 36 | | | | | | | | | | | | |
| 36.7 | 37 | | | | | | | | | | | | |
| 37.8 | 38 | | | | | | | | | | | | |
| 38.9 | 39 | | | | | | | | | | | | |
| 39.0 | 40 | | | | | | | | | | | | |
| 40.1 | 41 | | | | | | | | | | | | |
| 41.2 | 42 | | | | | | | | | | | | |
| 42.3 | 43 | | | | | | | | | | | | |
| 43.4 | 44 | | | | | | | | | | | | |
| 44.5 | 45 | | | | | | | | | | | | |
| 45.6 | 46 | | | | | | | | | | | | |
| 46.7 | 47 | | | | | | | | | | | | |
| 47.8 | 48 | | | | | | | | | | | | |
| 48.9 | 49 | | | | | | | | | | | | |
| 49.0 | 50 | | | | | | | | | | | | |
| 50.1 | 51 | | | | | | | | | | | | |
| 51.2 | 52 | | | | | | | | | | | | |
| 52.3 | 53 | | | | | | | | | | | | |
| 53.4 | 54 | | | | | | | | | | | | |
| 54.5 | 55 | | | | | | | | | | | | |
| 55.6 | 56 | | | | | | | | | | | | |
| 56.7 | 57 | | | | | | | | | | | | |
| 57.8 | 58 | | | | | | | | | | | | |
| 58.9 | 59 | | | | | | | | | | | | |
| 59.0 | 60 | | | | | | | | | | | | |
| 60.1 | 61 | | | | | | | | | | | | |

PAGE 0099

FLAHERTY GIOVANA ASSOCIATES, P. C.

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SUM OF 2 HYDROGRAPHS AT
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|------------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 30042 | 25636 | 11778 | 4838 | 582960 |
| 851 | 726 | 334 | 138 | 16308 |
| | 4.03 | 7.41 | 7.63 | |
| CFS | 102.47 | 186.31 | 194.19 | |
| CMS | 12712 | 23361 | 24083 | |
| INCHES | 15680 | 28815 | 29714 | |
| AC-FT | | | | |
| THOUS CU M | | | | |

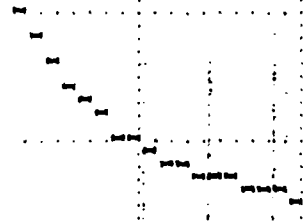
OVF

STATION 1

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|---|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 |
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 | 41 | 42 | 43 | 44 |

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OVN

C-351

| SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 9 | 86 | 83 | 80 |
|-------------------------|--------|--------|-----|-----|-----|
| 101 | 93 | 90 | 86 | 83 | 80 |
| 97 | 89 | 86 | 83 | 80 | 77 |
| 94 | 86 | 83 | 80 | 77 | 74 |
| 91 | 83 | 80 | 77 | 74 | 71 |
| 88 | 80 | 77 | 74 | 71 | 68 |
| 85 | 77 | 74 | 71 | 68 | 65 |
| 82 | 74 | 71 | 68 | 65 | 62 |
| 79 | 71 | 68 | 65 | 62 | 59 |
| 76 | 68 | 65 | 62 | 59 | 56 |
| 73 | 65 | 62 | 59 | 56 | 53 |
| 70 | 62 | 59 | 56 | 53 | 50 |
| 67 | 59 | 56 | 53 | 50 | 47 |
| 64 | 56 | 53 | 50 | 47 | 44 |
| 61 | 53 | 50 | 47 | 44 | 41 |
| 58 | 50 | 47 | 44 | 41 | 38 |
| 55 | 47 | 44 | 41 | 38 | 35 |
| 52 | 44 | 41 | 38 | 35 | 32 |
| 49 | 41 | 38 | 35 | 32 | 29 |
| 46 | 38 | 35 | 32 | 29 | 26 |
| 43 | 35 | 32 | 29 | 26 | 23 |
| 40 | 32 | 29 | 26 | 23 | 20 |
| 37 | 29 | 26 | 23 | 20 | 17 |
| 34 | 26 | 23 | 20 | 17 | 14 |
| 31 | 23 | 20 | 17 | 14 | 11 |
| 28 | 20 | 17 | 14 | 11 | 8 |
| 25 | 17 | 14 | 11 | 8 | 5 |
| 22 | 14 | 11 | 8 | 5 | 2 |
| 19 | 11 | 8 | 5 | 2 | -1 |
| 16 | 8 | 5 | 2 | -1 | -4 |
| 13 | 5 | 2 | -1 | -4 | -7 |
| 10 | 2 | -1 | -4 | -7 | -10 |
| 7 | -1 | -4 | -7 | -10 | -13 |
| 4 | -4 | -7 | -10 | -13 | -16 |
| 1 | -7 | -10 | -13 | -16 | -19 |

| PEAK | 9-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|-------|--------|---------|---------|--------------|
| 40085 | 51272 | 23535 | 9716 | 1265919 |
| 1701 | 1452 | 1467 | 1873 | 53013 |
| | 8.07 | 14.83 | 15.24 | |
| | 204.75 | 376.63 | 388.38 | |
| | 23424 | 46721 | 48178 | |
| | 31360 | 57630 | 59427 | |

OVF

| INFLW(1), | OUTFLOW(2) | AND OBSERVED FLOW(3) |
|-----------|------------|----------------------|
| 0 | 20000 | 40000 |
| 1 | 30000 | 50000 |
| 2 | 40000 | 60000 |
| 3 | 50000 | 70000 |
| 4 | 60000 | 80000 |
| 5 | 70000 | 90000 |
| 6 | 80000 | 100000 |
| 7 | 90000 | 110000 |
| 8 | 100000 | 120000 |
| 9 | 110000 | 130000 |
| 10 | 120000 | 140000 |
| 11 | 130000 | 150000 |
| 12 | 140000 | 160000 |
| 13 | 150000 | 170000 |
| 14 | 160000 | 180000 |
| 15 | 170000 | 190000 |
| 16 | 180000 | 200000 |
| 17 | 190000 | 210000 |
| 18 | 200000 | 220000 |
| 19 | 210000 | 230000 |
| 20 | 220000 | 240000 |

STATION 1

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OVN

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH - SUBWATERSHED NO. 3
 IETAG 1 IECON 0 ITAPE 0 JPLT 0 JPRT 0 INAME 1 ISTAGE 0 IAUTQ 0

1HYDQ 1 IUNG 1 TAREA 1 5.56 0.00 SNAP 0.00 TRSDA 0.00 TRSPC 0.00 RATIO 0.000 IBNDW 0 ISAME 1 LDCAL 0

PRECIP DATA
 SPFE 0.00 PMS 17.30 R6 86.00 R12 112.00 R48 119.00 R72 0.00 R96 0.00
 TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA
 LRPT 0 STRKR 0.00 DLYR 0.00 RYIOL 0.00 ERAIN 0.00 STRKS 0.00 R1LK 0.00 STRTL 0.00 CNSTL 0.00 ALSMX 0.00 RTIMP 0.00

UNIT HYDROGRAPH DATA
 TP= 3.05 CP=0.63 NTA= 0

APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 6.98 AND R= 5.41 INTERVALS
 STRIG= -2.00 RECESION DATA
 GRCSN= 10.10 RTIOR= 1.50

UNIT HYDROGRAPH 33 END-OF-PERIOD ORIGINATES, LAG= 3.02 HOURS: CP= 0.63 VOL= 1.00
 47 383 170 318 50 8
 60 41 264 219 34 6
 9 41 264 219 34 6

| MO DA | HR MN | PERIOD | RAIN | EXCS | LOSS | END-OF-PERIOD FLOW
COMP G | MO DA | HR MN | PERIOD | RAIN | EXCS | LOSS | COMP G |
|-------|-------|--------|------|------|------|------------------------------|-------|-------|--------|------|------|------|--------|
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 11 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 77 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 10 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 100 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 10 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 142 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 9 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 203 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 9 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 283 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 8 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 374 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 8 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 444 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 8 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 544 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 8 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 610 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 8 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 663 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 7 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 711 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 7 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 749 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 7 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 803 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 7 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 842 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 6 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 912 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 6 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 1033 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 6 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 1183 |
| 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 6 | 1 | 0 | 1 | 0.00 | 0.00 | 0.00 | 1253 |


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STATION 1
INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

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| TIME | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | PEAK | CFB | INCHES | AC-FT | THOUS CU FT |
|-------|--------|---------|---------|--------------|------|------|--------|-------|-------------|
| 11:00 | 5694 | 2265 | 950 | 112758 | 7373 | 5694 | 209 | | |
| 11:05 | 161 | 64 | 27 | 3132 | | 161 | | | |
| 11:10 | 2953 | 1316 | 13732 | 15732 | | 2953 | | | |
| 11:15 | 4179 | 3805 | 37932 | 37932 | | 4179 | | | |
| 11:20 | 3883 | 444 | 4637 | 4637 | | 3883 | | | |
| 11:25 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:30 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:35 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:40 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:45 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:50 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 11:55 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:00 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:05 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:10 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:15 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:20 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:25 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:30 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:35 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:40 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:45 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:50 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 12:55 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:00 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:05 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:10 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:15 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:20 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:25 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:30 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:35 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:40 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:45 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:50 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 13:55 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:00 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:05 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:10 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:15 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:20 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:25 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:30 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:35 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
| 14:40 | 3883 | 3883 | 3883 | 3883 | | 3883 | | | |
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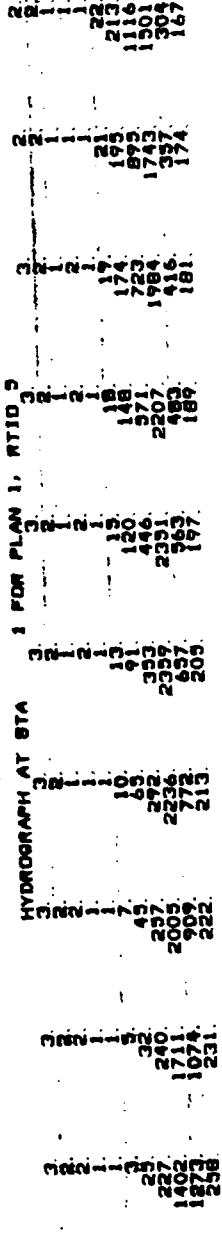
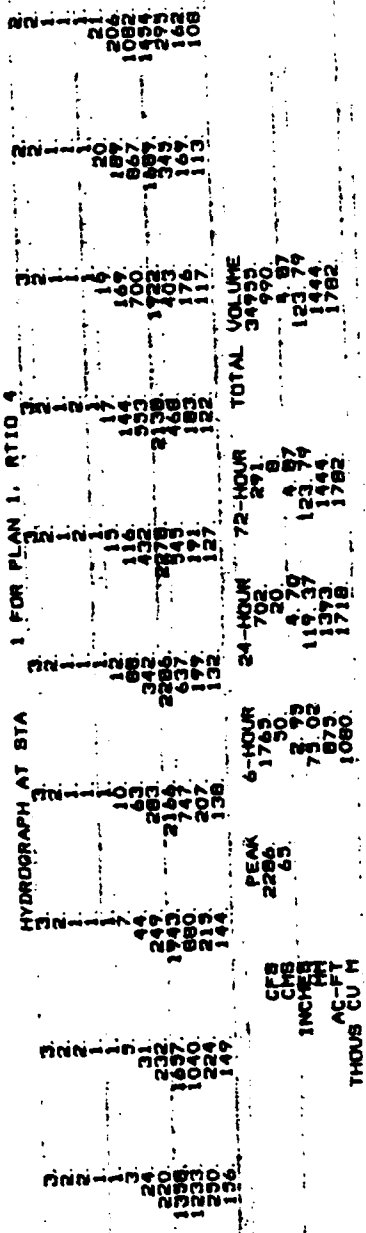
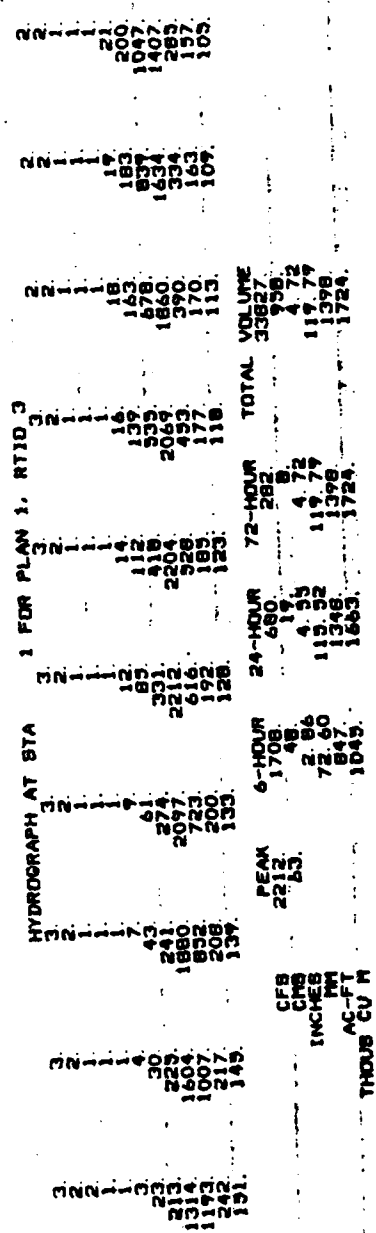
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| 9 | 9 | 0 | 0 | 1 | 1 | 2 |
| | 1 | 1 | 1 | 1 | 1 | |

#NYC

[illegible]

C-358

[illegible]



HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 6

C-360

HYDROGRAPH AT STA 1 FOR PLAN 1, RTIO 8

| HYDROGRAPH AT STA | | 1 FOR PLAN 1. RTIO 7 | | 82442222 | |
|-------------------|----|----------------------|---|----------|---|
| 10 | 10 | 9 | 8 | 8 | 8 |
| 9 | 9 | 7 | 7 | 7 | 7 |
| 8 | 8 | 6 | 6 | 6 | 6 |
| 7 | 7 | 5 | 5 | 5 | 5 |
| 6 | 6 | 4 | 4 | 4 | 4 |
| 5 | 5 | 3 | 3 | 3 | 3 |
| 4 | 4 | 2 | 2 | 2 | 2 |
| 3 | 3 | 1 | 1 | 1 | 1 |
| 2 | 2 | 0 | 0 | 0 | 0 |
| 1 | 1 | | | | |

C-361

[illegible]

| | PEAK | 0-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|-------------|-------|--------|---------|---------|--------------|
| CFB | 13285 | 11330 | 3182 | 2131 | 25736 |
| CMB | 376 | 321 | 146 | 60 | 7242 |
| INCHES | | 1.43 | 2.47 | 3.07 | |
| AC-FM | | 41.40 | 75.44 | 77.86 | 77.86 |
| AC-CU | | 5618 | 10239 | 10568 | 10568 |
| THOUS CU YD | | 4930 | 12629 | 13039 | 13039 |

● 2010

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

[illegible]

C-362

17 00 341
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OVN

C-364

| SUM OF 2 HYDROGRAPHS AT | PLAN 1 | RTIO 2 | TOTAL VOLUME |
|-------------------------|---------|--------------|--------------|
| 33 | 20 | 27 | 37817 |
| 23 | 19 | 15 | 10300 |
| 16 | 15 | 12 | 4.44 |
| 17 | 14 | 11 | 112.90 |
| 17 | 14 | 11 | 15323 |
| 45 | 104 | 147 | 18901 |
| 329 | 750 | 1148 | |
| 2087 | 3238 | 4880 | |
| 13612 | 18631 | 19223 | |
| 13667 | 9967 | 8062 | |
| 4742 | 3427 | 2633 | |
| 1948 | 1630 | 1465 | |
| PEAK | 72-HOUR | TOTAL VOLUME | |
| 17233 | 3070 | 37817 | |
| 545 | 212 | 10300 | |
| | 4.44 | 112.90 | |
| | 109.39 | 15323 | |
| | 14846 | 18901 | |
| | 10048 | | |
| CFS | | | |
| CMS | | | |
| INCHES | | | |
| TH | | | |
| AC-FT | | | |
| THOUS CU M | | | |

OVF

STATION 1
INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| INFLOW(I) | OUTFLOW(O) | OBSERVED FLOW(*) |
|-----------|------------|------------------|
| 0.11 | 3000 | 0.11 |
| 121 | 3000 | 121 |
| 31 | 3000 | 31 |
| 45 | 3000 | 45 |
| 51 | 3000 | 51 |
| 61 | 3000 | 61 |
| 81 | 3000 | 81 |
| 101 | 3000 | 101 |
| 112 | 3000 | 112 |
| 121 | 3000 | 121 |
| 131 | 3000 | 131 |
| 141 | 3000 | 141 |
| 151 | 3000 | 151 |
| 161 | 3000 | 161 |
| 171 | 3000 | 171 |
| 181 | 3000 | 181 |
| 191 | 3000 | 191 |
| 201 | 3000 | 201 |
| 211 | 3000 | 211 |
| 221 | 3000 | 221 |
| 231 | 3000 | 231 |
| 241 | 3000 | 241 |
| 251 | 3000 | 251 |
| 261 | 3000 | 261 |
| 271 | 3000 | 271 |
| 281 | 3000 | 281 |
| 291 | 3000 | 291 |
| 301 | 3000 | 301 |
| 311 | 3000 | 311 |
| 321 | 3000 | 321 |
| 331 | 3000 | 331 |
| 341 | 3000 | 341 |
| 351 | 3000 | 351 |
| 361 | 3000 | 361 |
| 371 | 3000 | 371 |
| 381 | 3000 | 381 |
| 391 | 3000 | 391 |
| 401 | 3000 | 401 |
| 411 | 3000 | 411 |
| 421 | 3000 | 421 |
| 431 | 3000 | 431 |
| 441 | 3000 | 441 |
| 451 | 3000 | 451 |
| 461 | 3000 | 461 |
| 471 | 3000 | 471 |
| 481 | 3000 | 481 |
| 491 | 3000 | 491 |
| 501 | 3000 | 501 |
| 511 | 3000 | 511 |
| 521 | 3000 | 521 |
| 531 | 3000 | 531 |
| 541 | 3000 | 541 |
| 551 | 3000 | 551 |
| 561 | 3000 | 561 |
| 571 | 3000 | 571 |
| 581 | 3000 | 581 |
| 591 | 3000 | 591 |
| 601 | 3000 | 601 |
| 611 | 3000 | 611 |
| 621 | 3000 | 621 |
| 631 | 3000 | 631 |
| 641 | 3000 | 641 |
| 651 | 3000 | 651 |
| 661 | 3000 | 661 |
| 671 | 3000 | 671 |
| 681 | 3000 | 681 |
| 691 | 3000 | 691 |
| 701 | 3000 | 701 |
| 711 | 3000 | 711 |
| 721 | 3000 | 721 |
| 731 | 3000 | 731 |
| 741 | 3000 | 741 |
| 751 | 3000 | 751 |
| 761 | 3000 | 761 |
| 771 | 3000 | 771 |
| 781 | 3000 | 781 |
| 791 | 3000 | 791 |
| 801 | 3000 | 801 |
| 811 | 3000 | 811 |
| 821 | 3000 | 821 |
| 831 | 3000 | 831 |
| 841 | 3000 | 841 |
| 851 | 3000 | 851 |
| 861 | 3000 | 861 |
| 871 | 3000 | 871 |
| 881 | 3000 | 881 |
| 891 | 3000 | 891 |
| 901 | 3000 | 901 |
| 911 | 3000 | 911 |
| 921 | 3000 | 921 |
| 931 | 3000 | 931 |
| 941 | 3000 | 941 |
| 951 | 3000 | 951 |
| 961 | 3000 | 961 |
| 971 | 3000 | 971 |
| 981 | 3000 | 981 |
| 991 | 3000 | 991 |
| 1001 | 3000 | 1001 |

351
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4 00 11
4 00 12

FLAHERTY GIOVARA ASSOCIATES, P.C.

8 30113
9 00114
9 30115
10 00116
10 30117
11 00118
11 30119
12 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | 1 PLAN 1 | | RTIO 3 | |
|-------------------------|-------|----------|-------|--------|-------|
| 34 | 35 | 31 | 32 | 29 | 30 |
| 36 | 37 | 31 | 32 | 29 | 30 |
| 24 | 25 | 17 | 18 | 15 | 16 |
| 17 | 18 | 17 | 18 | 15 | 16 |
| 16 | 17 | 17 | 18 | 15 | 16 |
| 19 | 20 | 17 | 18 | 15 | 16 |
| 32 | 33 | 108 | 109 | 130 | 131 |
| 215 | 216 | 775 | 776 | 4107 | 4108 |
| 1758 | 1759 | 3370 | 3371 | 19898 | 19899 |
| 11813 | 11814 | 19213 | 19214 | 9372 | 9373 |
| 15280 | 15281 | 10315 | 10316 | 2933 | 2934 |
| 2421 | 2422 | 1687 | 1688 | 1515 | 1516 |
| 2141 | 2142 | | | | |

PEAK
19898
563
CFB
CFB
INCHES
AC-FT
THOUS CU M

6-HOUR
16993
481
2.44
62.07
8427
10395

24-HOUR
7743
217
4.46
113.16
15358
18944

72-HOUR
3197
91
4.40
116.79
15851
19552

TOTAL VOLUME
383603
10862
4.60
116.79
15851
19552

OVF

STATION 1

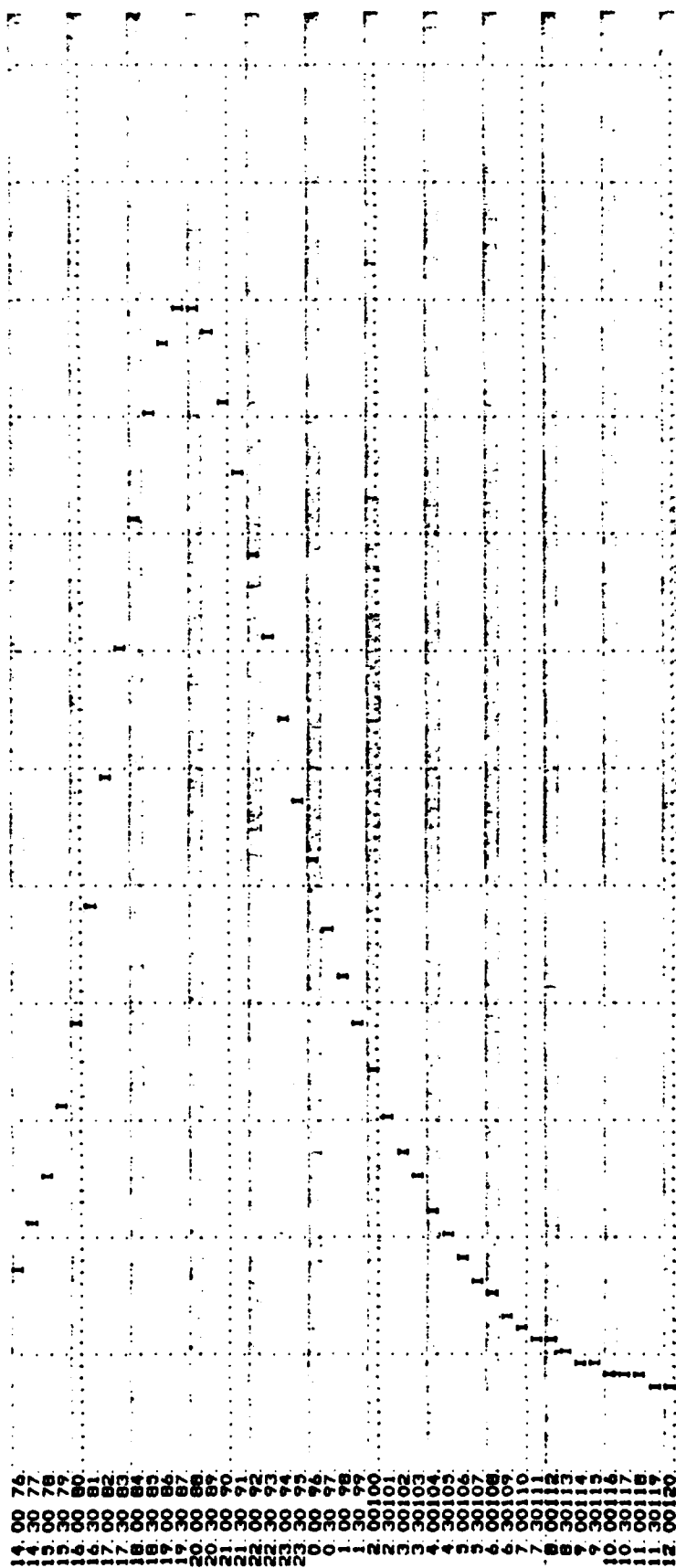
INFLWD(1), OUTFLOW(1) AND OBSERVED FLOW(1)

4000 6000 8000 10000 12000 14000 16000 18000 20000

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
30 0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17

FLAHERTY GIAVARA ASSOCIATES, P. C.

9 00 181
10 00 201
11 00 221
12 00 241
13 00 261
14 00 281
15 00 301
16 00 321
17 00 341
18 00 361
19 00 381
20 00 401
21 00 421
22 00 441
23 00 461
0 00 481
1 00 501
2 00 521
3 00 541
4 00 561
5 00 581
6 00 601
7 00 621
8 00 641
9 00 661
10 00 681
11 00 701
12 00 721
13 00 741
13 30



C-369

DYN

SUM OF 2 HYDROGRAPHS AT

| | | |
|----|----|----|
| 37 | 34 | 33 |
| 27 | 23 | 23 |
| 17 | 17 | 17 |
| 14 | 16 | 14 |
| 18 | 17 | 18 |
| 48 | 67 | 88 |

PLAN 1

| | |
|----|-----|
| 32 | 30 |
| 22 | 21 |
| 16 | 16 |
| 20 | 21 |
| 19 | 14 |
| 11 | 155 |

27

| | | | |
|----|-----|-----|-----|
| 27 | 20 | 16 | 13 |
| 19 | 16 | 12 | 157 |
| 16 | 12 | 13 | |
| 12 | 13 | 178 | |
| 18 | 178 | | |

| | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 224 | 272 | 331 | 444 | 618 | 801 | 1008 | 1227 | 1447 | 1659 |
| 1874 | 2034 | 2231 | 2308 | 2913 | 3483 | 4246 | 5217 | 6391 | 7930 |
| 9971 | 12038 | 14301 | 16747 | 18408 | 19913 | 20341 | 20549 | 19932 | 18890 |
| 17333 | 18098 | 18609 | 19172 | 18809 | 10454 | 9381 | 8418 | 7734 | 6973 |
| 6884 | 5853 | 5089 | 4355 | 4087 | 3664 | 3218 | 3031 | 2770 | 2534 |
| 2353 | 2213 | 2082 | 1981 | 1896 | 1793 | 1643 | 1566 | 1504 | 1444 |

| | | | | |
|-------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 20361 | 17362 | 8001 | 3503 | 376370 |
| 582 | 477 | 227 | 94 | 11223 |
| CF8 | CM8 | INCHES | MM | AC-FT |
| THOUS | CU | M | | |

OVF

STATION 1

| INFLW(I), | OUTFLW(O) | AND OBSERVED FLOW(*) |
|-----------|-----------|----------------------|
| 2000. | 4000. | 8000. |

| | | | | | | | | | |
|----|----|----|----|----|----|----|----|----|----|
| 0 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 |
| 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 |
| 30 | 31 | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 |
| 40 | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 |
| 50 | 51 | 52 | 53 | 54 | 55 | 56 | 57 | 58 | 59 |
| 60 | 61 | 62 | 63 | 64 | 65 | 66 | 67 | 68 | 69 |
| 70 | 71 | 72 | 73 | 74 | 75 | 76 | 77 | 78 | 79 |
| 80 | 81 | 82 | 83 | 84 | 85 | 86 | 87 | 88 | 89 |
| 90 | 91 | 92 | 93 | 94 | 95 | 96 | 97 | 98 | 99 |

FLAHERTY GIAVARA ASSOCIATES, P. C.

[illegible]

C-371

0 30 97
1 30 94
2 30 91
3 30 88
4 30 85
5 30 82
6 30 79
7 30 76
8 30 73
9 30 70
10 30 67
11 30 64
12 30 61

DVN

| SUM OF 2 HYDROGRAPHS AT | 1 | PLAN 1 | RTID 5 | 28 |
|-------------------------|--------|---------|--------------|-------|
| 37 | 33 | 31 | 30 | 28 |
| 23 | 22 | 22 | 21 | 20 |
| 17 | 17 | 16 | 16 | 14 |
| 20 | 20 | 21 | 22 | 22 |
| 17 | 15 | 14 | 13 | 14 |
| 91 | 118 | 137 | 162 | 204 |
| 638 | 827 | 1041 | 1267 | 1494 |
| 3007 | 3595 | 4383 | 5385 | 6597 |
| 19209 | 20558 | 21225 | 21211 | 20595 |
| 12231 | 10998 | 9870 | 8896 | 8004 |
| 4219 | 3782 | 3425 | 3129 | 2859 |
| 1908 | 1799 | 1698 | 1616 | 1552 |
| PEAK | 8-HOUR | 72-HOUR | TOTAL VOLUME | |
| 21225 | 8259 | 3410 | 409177 | |
| 401 | 234 | 97 | 11587 | |
| CFS | 513 | 4.90 | 4.90 | |
| INCHES | 2.61 | 4.75 | 124.58 | |
| AC-FT | 66.23 | 120.70 | 124.58 | |
| THOUS CU M | 8989 | 16382 | 16908 | |
| | 11088 | 20207 | 20656 | |

DVF

STATION 1

INFLOW(1), OUTFLOW(0) AND OBSERVED FLOW(1)
4000 5000 10000 12000 14000 16000 18000 20000 22000 24000

0 30 91

PAGE 0125

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6 30 62
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11. 00118.
11. 30119.
12. 00120.

#NWD#

| | SUM OF 2 HYDROGRAPHS AT | 1 PLAN 1 | RTIO 0 |
|------------|-------------------------|----------|---------|
| 41 | 37 | 26 | 72 |
| 28 | 36 | 32 | 72 |
| 20 | 25 | 32 | 72 |
| 17 | 14 | 17 | 72 |
| 12 | 18 | 17 | 72 |
| 24 | 20 | 17 | 72 |
| 23 | 31 | 16 | 152 |
| 209 | 71 | 16 | 152 |
| 1975 | 374 | 3708 | 1520 |
| 13027 | 2670 | 21300 | 21888 |
| 17138 | 17828 | 11341 | 10199 |
| 86683 | 14021 | 37591 | 3532 |
| 4668 | 2379 | 1859 | 1751 |
| 2355 | 4849 | 1859 | |
| | 2088 | | |
| | 4-HOUR | 24-HOUR | 72-HOUR |
| PEAK | 1895 | 8517 | 3516 |
| CBS | 21888 | 21 | 100 |
| CBS | 220 | 229 | 506 |
| INCHES | 269 | 4.90 | 128.47 |
| MM | 68.30 | 124.48 | 17437 |
| ACT | 11430 | 16894 | 17437 |
| THOUS CU M | 11430 | 20838 | 21508 |

• DVF •

[illegible]

11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80

30 00 81
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SUM OF 2 HYDROGRAPHS AT
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| 2381. | 2427. | 2284. | 2191. | 2027. | 1911. | 1804. | 1717. | 1649. | 1584. |
|-------|-------|------------|--------|---------|---------|--------------|-------|-------|-------|
| | | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME | | | |
| | | 22551 | 19261 | 8775 | 3423 | 434751 | | | |
| | | 639 | 595 | 248 | 103 | 12311 | | | |
| | | | 2.77 | 2.05 | 1.21 | 2.31 | | | |
| | | INCHES | 70.37 | 128.25 | 132.57 | 132.57 | | | |
| | | AC-FT | 9331 | 17908 | 17965 | 17965 | | | |
| | | THOUS CU H | 11781 | 21470 | 22159 | 22159 | | | |

ADVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(H)

| 0.00 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 6.00 | 7.00 | 8.00 | 9.00 | 10.00 | 11.00 | 12.00 | 13.00 | 14.00 | 15.00 | 16.00 | 17.00 | 18.00 | 19.00 | 20.00 | 21.00 | 22.00 |
|------|------|------|------|------|------|------|------|------|------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 0.00 | 1.00 | 2.00 | 3.00 | 4.00 | 5.00 | 6.00 | 7.00 | 8.00 | 9.00 | 10.00 | 11.00 | 12.00 | 13.00 | 14.00 | 15.00 | 16.00 | 17.00 | 18.00 | 19.00 | 20.00 | 21.00 | 22.00 |

441
00 451
00 461
00 471
00 481
00 491
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00 901
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00 971
00 981
00 991
00 1001

71 81 91 101 111 121 131 141 151 161 171 181 191 201 211 221 231 241 251 261 271 281 291 301 311 321 331 341 351 361 371 381 391 401 411 421 431 441 451 461 471 481 491 501 511 521 531 541 551 561 571 581 591 601 611 621 631 641

8 30 45
9 30 46
10 30 47
11 30 48
12 30 49
13 30 50
14 30 51
15 30 52
16 30 53
17 30 54
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73 30 110
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77 30 114
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80 30 117
81 30 118
82 30 119
83 30 120

DYN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | RTIO 7 | |
|-------------------------|-------|--------|-------|--------|-------|
| 124 | 119 | 102 | 98 | 94 | 88 |
| 84 | 81 | 73 | 68 | 64 | 60 |
| 60 | 58 | 52 | 51 | 50 | 47 |
| 51 | 53 | 44 | 48 | 48 | 47 |
| 63 | 59 | 44 | 48 | 48 | 47 |
| 72 | 107 | 39 | 43 | 37 | 32 |
| 598 | 656 | 258 | 322 | 307 | 252 |
| 32166 | 39476 | 11233 | 17678 | 1827 | 2543 |
| 56622 | 51933 | 64243 | 66327 | 66286 | 50733 |
| 20206 | 18170 | 34368 | 30903 | 27801 | 22494 |
| 7590 | 7138 | 13184 | 10704 | 9777 | 8174 |
| | | 5961 | 5305 | 5051 | 4658 |
| | | 6326 | 5622 | | |

| PEAK | | 6-HOUR | | 24-HOUR | | 72-HOUR | | TOTAL VOLUME | |
|------------|-------|--------|--------|---------|---------|---------|--|--------------|--|
| CFS | 66327 | 56650 | 25810 | 10656 | 1278678 | | | | |
| CMS | 1878 | 1604 | 731 | 302 | 36208 | | | | |
| INCHES | | 8.15 | 14.85 | 15.33 | | | | | |
| MM | | 206.98 | 377.20 | 389.32 | | | | | |
| AC-FT | | 28091 | 51193 | 52838 | | | | | |
| THOUS CU M | | 34650 | 63146 | 65175 | | | | | |

DVF

| STATION 1 | | INFLW(1), OUTFLOW(0) AND OBSERVED FLOW(1) | |
|-----------|-------|---|-------|
| 10000 | 20000 | 30000 | 40000 |
| 50000 | 60000 | 70000 | 80000 |

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99

14 00 281
15 00 291
16 00 301
17 00 311
18 00 321
19 00 331
20 00 341
21 00 351
22 00 361
23 00 371
24 00 381
25 00 391
26 00 401
27 00 411
28 00 421
29 00 431
30 00 441
31 00 451
32 00 461
33 00 471
34 00 481
35 00 491
36 00 501
37 00 511
38 00 521
39 00 531
40 00 541
41 00 551
42 00 561
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63 00 771
64 00 781
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66 00 801
67 00 811
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69 00 831
70 00 841
71 00 851

19 00 86.
19 30 87.
20 00 88.
20 30 89.
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23 30 95.
24 00 96.
24 30 97.
25 00 98.
25 30 99.
26 00 00.
26 30 01.
27 00 02.
27 30 03.
28 00 04.
28 30 05.
29 00 06.
29 30 07.
30 00 08.
30 30 09.
31 00 10.
31 30 11.
32 00 12.
32 30 13.
33 00 14.
33 30 15.
34 00 16.
34 30 17.
35 00 18.
35 30 19.
36 00 20.

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DVN

INFLOW HYDROGRAPH - SUBWATERSHED NO. 4
ISTAQ 1 ICDF 0 ITAPE 0 JPLI 0 JPRT 0 INAME 1 IASTAGE 0 IAUFD 0

SUB-AREA RUNOFF COMPUTATION

HYDROGRAPH DATA
INHYDQ 1 IUNQ 1 TAREA 10.33 SNAP 0.00 TRSDA TRSFC
PRECIP DATA
R12 R24 R48 R72 R96
0.00 17.30 86.00 100.00 112.00 117.00
TRSPC COMPUTED BY THE PROGRAM IS 0.801

QVT

C-387

[illegible]

C-389

◆ ◆ ◆ ◆ ◆

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO_1

HYDROGRAPH AT STA 1 FOR PLAN 1. RTIO 1

| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTIO 3 | | | | TOTAL VOLUME |
|-------------------|---------|----------------------|-------|--------|--------|--------------|
| 6-HOUR | 24-HOUR | 72-HOUR | PEAK | CFS | INCHES | AC-FY |
| 3197 | 1269 | 57 | 4153 | 118 | 63259 | 1984 |
| 91 | 15 | 15 | 118 | 91 | 1792 | 1231 |
| 2 88 | 3 57 | 4 75 | 2 88 | 3 57 | 4 75 | 1231 |
| 13 11 | 116 08 | 120 60 | 13 11 | 116 08 | 120 60 | 1231 |
| 1585 | 2316 | 2614 | 1585 | 2316 | 2614 | 1231 |

THOUS CU M

1955

3104

3225

3225

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO 4

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

CFB
CHS
INCHES
AC-FT
THOUS CU M

PEAK
4304
122
3383
74
2 57
75 55
1438
2020

24-HOUR
1311
37
4 72
114 95
2400
3208

72-HOUR
545
15
4 71
124 62
2702
3332

TOTAL VOLUME
65378
1831
4 71
124 62
2702
3332

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

C-391

THOUS CU M

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO 5

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

PEAK
4443
126
3410
77
3 07
177 77
1641
2085

24-HOUR
1353
38
4 87
123 82
2684
3311

72-HOUR
562
16
3 06
129 84
2787
3440

TOTAL VOLUME
67487
1911
3 06
129 84
2787
3440

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

THOUS CU M

HYDROGRAPH AT STA

1 FOR PLAN 1, RTIO 6

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

5 4 3 2 1

6 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

PEAK
4443
126
3410
77
3 07
177 77
1641
2085

24-HOUR
1353
38
4 87
123 82
2684
3311

72-HOUR
562
16
3 06
129 84
2787
3440

TOTAL VOLUME
67487
1911
3 06
129 84
2787
3440

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

5 4 3 2 1
4 3 2 1
10 6 1
48 39
276 313
237 190
481 168
257 276

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|------|--------|---------|---------|--------|--------|
| CFS | 4982 | 3516 | 1376 | 580 | 63796 | 1971 |
| CMS | 130 | 100 | 40 | 16 | 522 | 532 |
| INCHES | | 30.17 | 2.03 | 13.66 | 138.66 | 138.66 |
| MM | | 80.43 | 127.69 | 348.88 | 3579 | 3579 |
| CU M | | 1744 | 2668 | 3397 | 3547 | 3547 |
| THOUS | | 1.744 | 2.668 | 3.397 | 3.547 | 3.547 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL |
|--------|------|--------|---------|---------|-------|
| CSB | 4720 | 3623 | 1438 | 598 | 7105 |
| CSB | 134 | 103 | 41 | 17 | 205 |
| INCHES | | 3.26 | 1.18 | 3.38 | |
| FT | | 82.66 | 31.14 | 136.68 | |
| FT | | 1796 | 2882 | 3763 | |
| AC-11 | | 2216 | 3518 | 3635 | |
| THROW | | | | | 3635 |

| | 449. | 431. | 414. | 398. | 382. | 367. | 352. |
|--------|------|------|--------|--------|--------|-------|--------|
| PEAK | 6142 | 6172 | 5129 | 2110 | 872 | 10249 | 70249 |
| CFB | | | 5129 | 2110 | 872 | 10249 | 70249 |
| CHB | | | 5129 | 2110 | 872 | 10249 | 70249 |
| INCHES | | | 4.80 | 7.62 | 25 | 7.91 | 200.99 |
| AC-FT | | | 121.80 | 193.46 | 200.94 | 4337. | 4337. |
| CU-M | | | 2642 | 4174 | 5375 | 5375 | 5375 |
| TURNS | | | 3259 | 5173 | 5375 | 5375 | 5375 |

DVF

STATION 1

INFLW(I), OUTFLOW(I) AND OBSERVED FLOW(I*)

2000. 4000. 6000. 8000. 10000. 12000. 14000. 16000. 0. 0. 0. 0.

0.11 30 01 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53

FLAHERTY DIAVARA ASSOCIATES, P. C.

35 00 341
36 00 351
37 00 361
38 00 371
39 00 381
40 00 391
41 00 401
42 00 411
43 00 421
44 00 431
45 00 441
46 00 451
47 00 461
48 00 471
49 00 481
50 00 491
51 00 501
52 00 511
53 00 521
54 00 531
55 00 541
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58 00 571
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67 00 661
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69 00 681
70 00 691
71 00 701
72 00 711
73 00 721
74 00 731
75 00 741
76 00 751
77 00 761
78 00 771
79 00 781
80 00 791
81 00 801
82 00 811
83 00 821
84 00 831
85 00 841
86 00 851
87 00 861
88 00 871
89 00 881
90 00 891
91 00 901
92 00 911
93 00 921
94 00 931
95 00 941
96 00 951
97 00 961
98 00 971
99 00 981
100 00 991
101 00 1001
102 00 1011
103 00 1021
104 00 1031
105 00 1041
106 00 1051
107 00 1061
108 00 1071
109 00 1081
110 00 1091
111 00 1101

8 00112
9 30113
9 30114
9 30115
10 30116
10 30117
11 30118
11 30119
12 00120

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | PLAN 2 | |
|-------------------------|-------|--------|------|--------|-------|
| 42 | 40 | 36 | 34 | 32 | 30 |
| 27 | 27 | 25 | 24 | 22 | 21 |
| 21 | 20 | 18 | 18 | 18 | 18 |
| 19 | 20 | 24 | 25 | 26 | 26 |
| 24 | 23 | 19 | 17 | 14 | 14 |
| 27 | 40 | 20 | 13 | 12 | 12 |
| 254 | 312 | 81 | 33 | 18 | 203 |
| 2126 | 2313 | 332 | 337 | 1457 | 1651 |
| 11738 | 13397 | 2846 | 4026 | 1202 | 7520 |
| 18336 | 18842 | 1997 | 2134 | 2738 | 2183 |
| 6381 | 9660 | 1395 | 1084 | 938 | 7839 |
| 2473 | 2331 | 462 | 360 | 342 | 2866 |
| | | 2075 | 1852 | 1751 | 1603 |
| | | | | | 20174 |
| | | | | | 9357 |
| | | | | | 1918 |
| | | | | | 7022 |
| | | | | | 2653 |
| | | | | | 1539 |

C-396

OVF

| STATION 1 | |
|-----------|---------------------------------|
| INFLW(1), | OUTFLOW(2) AND OBSERVED FLOW(3) |
| 8000 | 20000 |
| 4000 | 24000 |

0 11
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1 30
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30 171
8 30 181
9 30 191
10 30 201
11 30 211
12 30 221
13 30 231
14 30 241
15 30 251
16 30 261
17 30 271
18 30 281
19 30 291
20 30 301
21 30 311
22 30 321
23 30 331
24 30 341
25 30 351
26 30 361
27 30 371
28 30 381
29 30 391
30 30 401
31 30 411
32 30 421
33 30 431
34 30 441
35 30 451
36 30 461
37 30 471
38 30 481
39 30 491
40 30 501
41 30 511
42 30 521
43 30 531
44 30 541
45 30 551
46 30 561
47 30 571
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49 30 591
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53 30 631
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55 30 651
56 30 661
57 30 671
58 30 681
59 30 691
60 30 701
61 30 711
62 30 721
63 30 731
64 30 741

13 30 75
14 00 76
15 30 77
16 00 78
17 30 79
18 00 80
19 30 81
20 00 82
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22 00 84
23 30 85
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28 00 90
29 30 91
30 00 92
31 30 93
32 00 94
33 30 95
34 00 96
35 30 97
36 00 98
37 30 99
38 00 100
39 30 101
40 00 102
41 30 103
42 00 104
43 30 105
44 00 106
45 30 107
46 00 108
47 30 109
48 00 110
49 30 111
50 00 112
51 30 113
52 00 114
53 30 115
54 00 116
55 30 117
56 00 118
57 30 119
58 00 120

C-398

OVN

| SUM OF 2 HYDROGRAPHS AT | | PLAN 1 | | ATTIO 3 | |
|-------------------------|----|--------|----|---------|----|
| 40 | 37 | 36 | 34 | 33 | 31 |
| 27 | 26 | 25 | 24 | 23 | 22 |
| 20 | 19 | 18 | 17 | 16 | 15 |
| 21 | 20 | 19 | 18 | 17 | 16 |
| 22 | 21 | 20 | 19 | 18 | 17 |
| 23 | 22 | 21 | 20 | 19 | 18 |
| 20 | 19 | 18 | 17 | 16 | 15 |
| 42 | 38 | 36 | 34 | 33 | 31 |
| 28 | 26 | 25 | 24 | 23 | 22 |
| 21 | 20 | 19 | 18 | 17 | 16 |
| 20 | 19 | 18 | 17 | 16 | 15 |
| 23 | 22 | 21 | 20 | 19 | 18 |
| 20 | 19 | 18 | 17 | 16 | 15 |

28 263 42 61 84 110 137 144 189 212 232
 200 293 323 571 764 992 1243 1499 1749 1984
 12142 17443 2614 2944 3446 4163 5127 6338 7779 9679
 19175 17422 19693 20169 22173 23398 27748 33336 39337 50869
 5997 5855 5294 4781 4063 3313 2589 1894 1350 8109 2364
 2358 2274 2274 2146 2027 1916 1812 1727 1658 1592

PEAK 6-HOUR 24-HOUR 72-HOUR TOTAL VOLUME
 23748 20036 9007 3724 48873
 672 567 253 105 12854
 2 49 4 47 4 62
 63 12 13 51 17 32
 9935 12866 18466
 12255 25037 22777

THOUS CU M

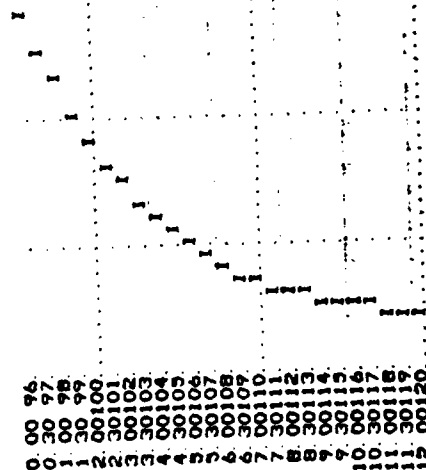
STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(O*)

0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37

FLAHERTY GIVARA ASSOCIATES, P. C.

19 00 381
19 30 391
20 00 401
20 30 411
21 00 421
21 30 431
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47 00 941
47 30 951



• Q •

C-401

[illegible]

• END •

59 30 00 60 30 00 61 30 00 62 30 00 63 30 00 64 30 00 65 30 00 66 30 00 67 30 00 68 30 00 69 30 00 70 30 00 71 30 00 72 30 00 73 30 00 74 30 00 75 30 00 76 30 00 77 30 00 78 30 00 79 30 00 80 30 00 81 30 00 82 30 00 83 30 00 84 30 00 85 30 00 86 30 00 87 30 00 88 30 00 89 30 00 90 30 00 91 30 00 92 30 00 93 30 00 94 30 00 95 30 00 96 30 00 97 30 00 98 30 00 99 30 00 00 30 00 01 30 00 02 30 00 03 30 00 04 30 00 05 30 00 06 30 00 07 30 00 08 30 00 09 30 00 10 30 00 11 30 00 12 30 00 13 30 00 14 30 00 15 30 00 16 30 00

[illegible]

• JVD •

STATION

| INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|------------|------------|----------------------|
| 12000. | 16000. | 20000. |
| | | 24000. |

[illegible]

C-407

21 30 431
 22 00 441
 23 00 451
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 76 00 981
 77 00 991
 78 00 1001

30101 30102 30103 30104 30105 30106 30107 30108 30109 30110 30111 30112 30113 30114 30115 30116 30117 30118 30119 30120

W.D.

C-409

[illegible]

• END •

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STATION

| | INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|-------|------------|------------|----------------------|
| 10000 | 10000 | 10000 | 10000 |
| 12000 | 12000 | 12000 | 12000 |
| 14000 | 14000 | 14000 | 14000 |
| 16000 | 16000 | 16000 | 16000 |
| 18000 | 18000 | 18000 | 18000 |
| 20000 | 20000 | 20000 | 20000 |
| 22000 | 22000 | 22000 | 22000 |
| 24000 | 24000 | 24000 | 24000 |
| 26000 | 26000 | 26000 | 26000 |
| 28000 | 28000 | 28000 | 28000 |
| 30000 | 30000 | 30000 | 30000 |

28000.

Q

6.

FLAHERTY GIAVARA ASSOCIATES, P. C.

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17 00118
18 00119
19 00120

DVN

SUB-AREA RUNOFF COMPUTATION

INFLOW HYDROGRAPH - SUBWATERSHED NO. 7 (OTSEGO LAKE)
ISTAG ICDP IECON ITAPE JPL JPRI INAME ISTAGE IAUTO

HYDO IUNQ TAREA SNAP TRSDA TRSPC RATIO ISNOW ISAME LOCAL
1 1 1.38 0.00 0.38 0.00 0.00 0 0 1 0

PRECIP DATA
R12 R24 R48 R72 R96
0.00 17.30 86.00 100.00 112.00 117.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.800

LOSS DATA
LROPT STARR DLTAR RTIOL ERAIN STRAS RTIOM STRTL CNSTL ALBRK RTIMP
0 0.00 0.00 1.00 0.00 0.00 1.00 0.00 0.00 0.00 1.00

UNIT HYDROGRAPH DATA
TP= 0.00 CP=0.63 NTA= 0

RECESSION DATA
STRTO= -2.00 GRCSN= -0.10 RTIOR= 1.50

TC INCREASED TO THREE OF 0.50
R INCREASED TO MINIMUM OF 0.5
CLARK DID NOT CONVERGE TO GIVEN SNYDER COEFFICIENTS
APPROXIMATE CLARK COEFFICIENTS FROM GIVEN SNYDER CP AND TP ARE TC= 1.00 AND R= 0.50 INTERVALS

UNIT HYDROGRAPH 2 END-OF-PERIOD ORDINATES, LAQ= 0.39 HOURS, CP= 0.50 VOL= 1.00
4115

NO. DA HR. MN PERIOD RAIN EXCS LOSS END-OF-PERIOD FLOW NO. DA HR. MN PERIOD RAIN EXCS LOSS COMP 0

◆ QVF ◆

STATION

| INFLOW(I), | OUTFLOW(O) | AND OBSERVED FLOW(*) |
|------------|------------|----------------------|
| 12000 | 14000 | 20000 |
| | | 24000 |

C-419

FLAHERTY O'AVARA ASSOCIATES, P. C.

[illegible]

C-420

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| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTID 1 | | 1 FOR PLAN 1, RTID 2 | | TOTAL VOLUME | |
|-------------------|------|----------------------|------|----------------------|------|--------------|------|
| 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| 20 | 14 | 20 | 20 | 20 | 20 | 36382 | 20 |
| 114 | 20 | 44 | 19 | 69 | 76 | 1030 | 103 |
| 123 | 246 | 86 | 76 | 78 | 43 | 4 | 102 |
| 102 | 21 | 19 | 20 | 18 | 18 | 102 | 102 |
| 199 | 102 | 102 | 102 | 102 | 102 | 102 | 102 |
| 297 | 297 | 297 | 297 | 297 | 297 | 102 | 297 |
| 392 | 495 | 1202 | 1073 | 1312 | 1475 | 1639 | 4152 |
| 322 | 1366 | 1202 | 1202 | 407 | 391 | 360 | 346 |
| 222 | 306 | 677 | 1294 | 271 | 261 | 290 | 231 |
| 148 | 204 | 188 | 196 | 181 | 174 | 167 | 151 |
| | 136 | 126 | 131 | 121 | 116 | 111 | 103 |
| PEAK | | 24-HOUR | | 72-HOUR | | TOTAL VOLUME | |
| CF8 | CM8 | 6 | 7 | 8 | 9 | 10 | 11 |
| 4153 | 1783 | 61 | 61 | 303 | 7 | 36382 | 20 |
| 118 | 50 | 19 | 19 | 4 | 4 | 1030 | 103 |
| INCHES | | 3.84 | | 4.42 | | 4.42 | |
| AC-FT | | 77.75 | | 112.28 | | 112.28 | |
| THOUS CU M | | 1618 | | 1834 | | 1834 | |
| HYDROGRAPH AT STA | | 1 FOR PLAN 1, RTID 1 | | 1 FOR PLAN 1, RTID 2 | | TOTAL VOLUME | |
| 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 |
| 20 | 12 | 12 | 12 | 12 | 12 | 36382 | 20 |
| 114 | 20 | 44 | 19 | 69 | 76 | 1030 | 103 |
| 123 | 246 | 86 | 76 | 78 | 43 | 4 | 102 |
| 102 | 21 | 19 | 20 | 18 | 18 | 102 | 102 |
| 199 | 102 | 102 | 102 | 102 | 102 | 102 | 102 |
| 297 | 297 | 297 | 297 | 297 | 297 | 102 | 297 |
| 392 | 495 | 1202 | 1073 | 1312 | 1475 | 1639 | 4152 |
| 322 | 1366 | 1202 | 1202 | 407 | 391 | 360 | 346 |
| 222 | 306 | 677 | 1294 | 271 | 261 | 290 | 231 |
| 148 | 204 | 188 | 196 | 181 | 174 | 167 | 151 |
| | 136 | 126 | 131 | 121 | 116 | 111 | 103 |

| | | | | | | | | |
|------|------|------|------|------|------|------|------|------|
| 33 | 31 | 29 | 28 | 27 | 26 | 25 | 81 | 148 |
| 148 | 148 | 148 | 148 | 148 | 148 | 148 | 148 | 148 |
| 287 | 430 | 430 | 430 | 430 | 430 | 430 | 430 | 430 |
| 430 | 1007 | 1585 | 1743 | 1902 | 2139 | 2377 | 2634 | 6022 |
| 5686 | 2219 | 1981 | 982 | 590 | 567 | 544 | 523 | 502 |
| 482 | 463 | 427 | 410 | 393 | 378 | 363 | 348 | 335 |
| 321 | 308 | 296 | 273 | 262 | 252 | 242 | 232 | 223 |
| 214 | 206 | 190 | 182 | 173 | 168 | 161 | 155 | 149 |

| THOUS CU M | AC-FT | INCHES | CM | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------------|-------|--------|----|------|--------|---------|---------|--------------|
| | | | | 6022 | 2583 | 959 | 440 | 52754 |
| | | | | 171 | 73 | 27 | 12 | 1494 |
| | | | | | 3.77 | 3.57 | 6.41 | |
| | | | | | 93.75 | 142.03 | 162.81 | |
| | | | | | 1282 | 1902 | 2180 | |
| | | | | | 1581 | 2346 | 2689 | |

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|------|------|------|------|------|------|------|------|------|
| 8 | 13 | 13 | 13 | 13 | 12 | 12 | 12 | 12 |
| 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 29 | 29 | 29 | 29 | 29 | 29 | 29 | 29 | 29 |
| 171 | 390 | 369 | 144 | 126 | 114 | 104 | 104 | 104 |
| 34 | 33 | 31 | 30 | 29 | 27 | 26 | 24 | 23 |
| 133 | 133 | 133 | 133 | 133 | 133 | 133 | 133 | 133 |
| 259 | 443 | 423 | 423 | 423 | 423 | 423 | 423 | 423 |
| 443 | 1042 | 1802 | 1802 | 1802 | 2213 | 2457 | 2723 | 6227 |
| 5822 | 2235 | 2049 | 1802 | 167 | 2213 | 2457 | 2723 | 6227 |
| 482 | 463 | 427 | 410 | 393 | 378 | 363 | 348 | 335 |
| 321 | 308 | 296 | 273 | 262 | 252 | 242 | 232 | 223 |
| 222 | 213 | 204 | 188 | 181 | 174 | 167 | 160 | 154 |

| THOUS CU M | AC-FT | INCHES | CM | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------------|-------|--------|----|------|--------|---------|---------|--------------|
| | | | | 6227 | 2675 | 972 | 453 | 54573 |
| | | | | 176 | 76 | 28 | 13 | 1945 |
| | | | | | 3.90 | 5.78 | 6.63 | |
| | | | | | 99.05 | 146.72 | 168.42 | |
| | | | | | 1326 | 1967 | 2253 | |
| | | | | | 1636 | 2427 | 2782 | |

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|------|------|------|------|------|------|------|------|------|
| 9 | 13 | 13 | 13 | 13 | 13 | 13 | 13 | 12 |
| 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 |
| 130 | 30 | 31 | 31 | 31 | 31 | 31 | 31 | 30 |
| 177 | 403 | 381 | 149 | 133 | 117 | 107 | 104 | 104 |
| 35 | 34 | 32 | 31 | 30 | 29 | 27 | 26 | 25 |
| 158 | 158 | 158 | 158 | 158 | 158 | 158 | 158 | 158 |
| 309 | 460 | 460 | 460 | 460 | 460 | 460 | 460 | 460 |
| 4078 | 2372 | 2118 | 1863 | 1863 | 2287 | 2531 | 2815 | 6437 |
| 515 | 495 | 475 | 456 | 431 | 404 | 382 | 372 | 358 |
| 343 | 330 | 317 | 304 | 292 | 283 | 273 | 265 | 258 |
| 229 | 220 | 211 | 203 | 195 | 187 | 180 | 166 | 159 |

| THOUS CU M | AC-FT | INCHES | CM | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------------|-------|--------|----|------|--------|---------|---------|--------------|
| | | | | 6437 | 2744 | 1025 | 470 | 56327 |
| | | | | 182 | 78 | 29 | 13 | 1957 |

| | | | |
|------------|--------|--------|---------|
| CBS | PEAK | 6-HOUR | 24-HOUR |
| CBS | 645 | 2853 | 1058 |
| INCHES | 188 | 81 | 30 |
| MM | | 4 16 | 6 17 |
| AC-FT | 107 45 | 174 65 | 179 85 |
| THOUS CU M | 1713 | 2403 | 2403 |
| | 1735 | 2967 | 2967 |
| | | | 58211 |
| | | | 1648 |
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| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------------|------|--------|---------|---------|-------|--------|
| CFS | 7060 | 3031 | 1124 | 515 | | 81850 |
| CMB | 200 | 86 | 32 | 15 | | 1751 |
| INCHES | | 4 | 6 | 7 | | 7 |
| MM | | 12 | 146 | 190 | | 190 |
| AC-FT | | 26 | 51 | 68 | | 88 |
| | | 1503 | 2230 | 2556 | | 3152 |
| THOUS CU M | | 1854 | 2750 | 3152 | | 3152 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------------|-------|--------|---------|---------|-------|--------|
| CFR | 10392 | 4450 | 1633 | 750 | 70955 | |
| CMS | 294 | 126 | 47 | 21 | 2576 | |
| INCHES | | 6.50 | 7.64 | 11.05 | | 11.05 |
| MM | | 163.08 | 244.87 | 280.71 | | 280.71 |
| AC-FT | | 3210 | 3279 | 3758 | | 3758 |
| THOUS CU M | | 2726 | 4044 | 4636 | | 4636 |

| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------|-------|--------|---------|---------|--------------|
| CF8 | 20764 | 8915 | 3306 | 1516 | 18190 |
| CF8 | 588 | 252 | 94 | 43 | 5151 |
| INC8 | | 13 00 | 19 28 | 22 10 | 22 16 |

AD-A109 795

FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT

F/G 13/13

NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)

JUL 81 H C FLAHERTY

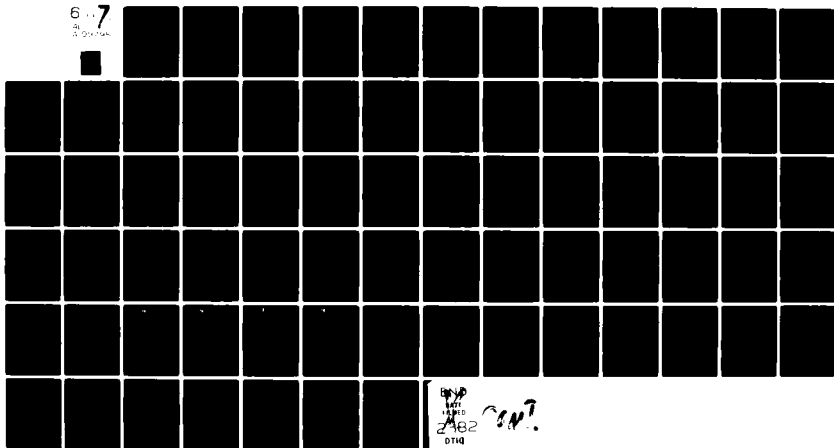
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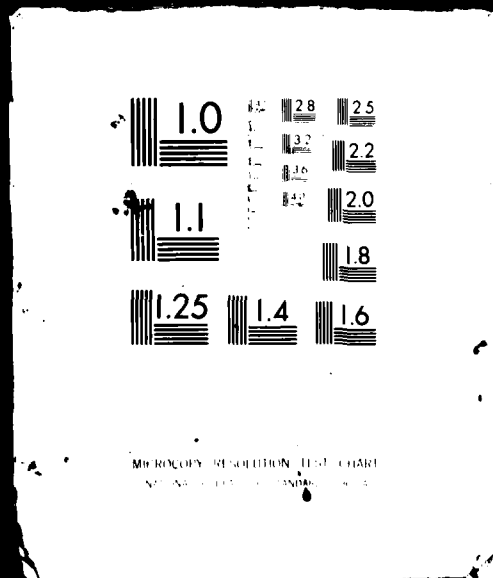
CONF

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OF

AD

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DYN

SUM OF 2 HYDROGRAPHS AT

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PLAN 1 RTIO 2

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|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 57. | 54. | 49. | 46. | 44. | 41. | 39. | 76. | 156. |
| 175. | 188. | 229. | 254. | 280. | 306. | 330. | 352. | 372. |
| 343. | 742. | 982. | 1168. | 1390. | 1632. | 1880. | 2121. | 2348. |
| 256. | 2744. | 4431. | 5075. | 5928. | 7096. | 8504. | 10154. | 15378. |
| 17423. | 16407. | 21240. | 22416. | 23208. | 23923. | 23102. | 22106. | 20679. |
| 19018. | 17304. | 14023. | 12578. | 11287. | 10136. | 9108. | 8187. | 7356. |
| 6402. | 5969. | 4906. | 4443. | 4022. | 3675. | 3384. | 3118. | 2876. |
| 2687. | 2536. | 2264. | 2142. | 2037. | 1919. | 1830. | 1758. | 1688. |

| | | | | |
|-------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 23923 | 20396 | 9629 | 4037 | 484731 |
| 666 | 578 | 273 | 114 | 13726 |
| | 2.33 | 4.40 | 4.62 | 4.62 |
| | 59.22 | 111.83 | 117.28 | 117.28 |
| | 10114 | 19039 | 20030 | 20030 |
| | 12475 | 23339 | 24707 | 24707 |

CFS

CMS

INCHES

AC-FT

THOUS CU M

DVF

STATION 1

| | | | | | |
|------------|-------------|-----------------------|--------|--------|--------|
| 4000. | 8000. | 12000. | 16000. | 20000. | 24000. |
| INFLOW (1) | OUTFLOW (2) | AND OBSERVED FLOW (3) | | | |

| | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|
| 0.1 | 0.2 | 0.3 | 0.4 | 0.5 | 0.6 | 0.7 | 0.8 | 0.9 | 1.0 | 1.1 | 1.2 | 1.3 | 1.4 | 1.5 | 1.6 | 1.7 | 1.8 | 1.9 | 2.0 | 2.1 | 2.2 | 2.3 | 2.4 | 2.5 | 2.6 | 2.7 | 2.8 | 2.9 | 3.0 | 3.1 | 3.2 | 3.3 | 3.4 | 3.5 | 3.6 | 3.7 | 3.8 | 3.9 | 4.0 | 4.1 | 4.2 | 4.3 | 4.4 | 4.5 | 4.6 | 4.7 | 4.8 | 4.9 | 5.0 | 5.1 | 5.2 | 5.3 | 5.4 | 5.5 | 5.6 | 5.7 | 5.8 | 5.9 | 6.0 | 6.1 | 6.2 | 6.3 | 6.4 | 6.5 | 6.6 | 6.7 | 6.8 | 6.9 | 7.0 | 7.1 | 7.2 | 7.3 | 7.4 | 7.5 | 7.6 | 7.7 | 7.8 | 7.9 | 8.0 | 8.1 | 8.2 | 8.3 | 8.4 | 8.5 | 8.6 | 8.7 | 8.8 | 8.9 | 9.0 | 9.1 | 9.2 | 9.3 | 9.4 | 9.5 | 9.6 | 9.7 | 9.8 | 9.9 | 10.0 |
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|------|

FLAHERTY GIOVARE ASSOCIATES, P. C.

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11 00118
11 30119
12 00120

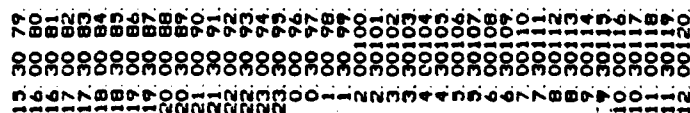
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C-433

#JVD#

| STATION | INFLW(I) | OUTFLW(O) | AND OBSERVED FLOW(S) |
|---------|----------|-----------|----------------------|
| 0 | 4000 | 8000 | 12000 |
| 1 | 1000 | 15000 | 20000 |
| 2 | 1000 | 15000 | 24000 |
| 3 | 1000 | 15000 | 28000 |
| 4 | 1000 | 15000 | 28000 |
| 5 | 1000 | 15000 | 28000 |
| 6 | 1000 | 15000 | 28000 |
| 7 | 1000 | 15000 | 28000 |
| 8 | 1000 | 15000 | 28000 |
| 9 | 1000 | 15000 | 28000 |
| 10 | 1000 | 15000 | 28000 |
| 11 | 1000 | 15000 | 28000 |
| 12 | 1000 | 15000 | 28000 |
| 13 | 1000 | 15000 | 28000 |
| 14 | 1000 | 15000 | 28000 |
| 15 | 1000 | 15000 | 28000 |
| 16 | 1000 | 15000 | 28000 |
| 17 | 1000 | 15000 | 28000 |
| 18 | 1000 | 15000 | 28000 |
| 19 | 1000 | 15000 | 28000 |
| 20 | 1000 | 15000 | 28000 |



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| | | | | | | | | | |
|-------|-------|-------|-------|-------|-------|-------|-------|------|------|
| 20983 | 19093 | 17231 | 13474 | 13880 | 12433 | 11184 | 10030 | 9034 | 8117 |
| 7285 | 6386 | 5974 | 5413 | 4902 | 4438 | 4055 | 3734 | 3440 | 3174 |
| 2965 | 2799 | 2644 | 2499 | 2363 | 2236 | 2118 | 2020 | 1939 | 1862 |

PEAK 25956
 CFS 22506
 CMS 637
 INCHES 4.86
 MW 2.57
 AC-FT 69.34
 THOUS CU M 11160
 13766

72-HOUR 4457
 TOTAL VOLUME 334875
 15146
 5.10
 129.41
 22102
 27263

DVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| | | | | | | | | | | |
|------|------|-------|-------|-------|-------|-------|---|---|---|---|
| 4000 | 8000 | 12000 | 16000 | 20000 | 24000 | 28000 | 0 | 0 | 0 | 0 |
|------|------|-------|-------|-------|-------|-------|---|---|---|---|

21 00 421
21 30 431
22 00 441
22 30 451
23 00 461
23 30 471
24 00 481
24 30 491
25 00 501
25 30 511
26 00 521
26 30 531
27 00 541
27 30 551
28 00 561
28 30 571
29 00 581
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34 30 691
35 00 701
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40 00 801
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45 00 901
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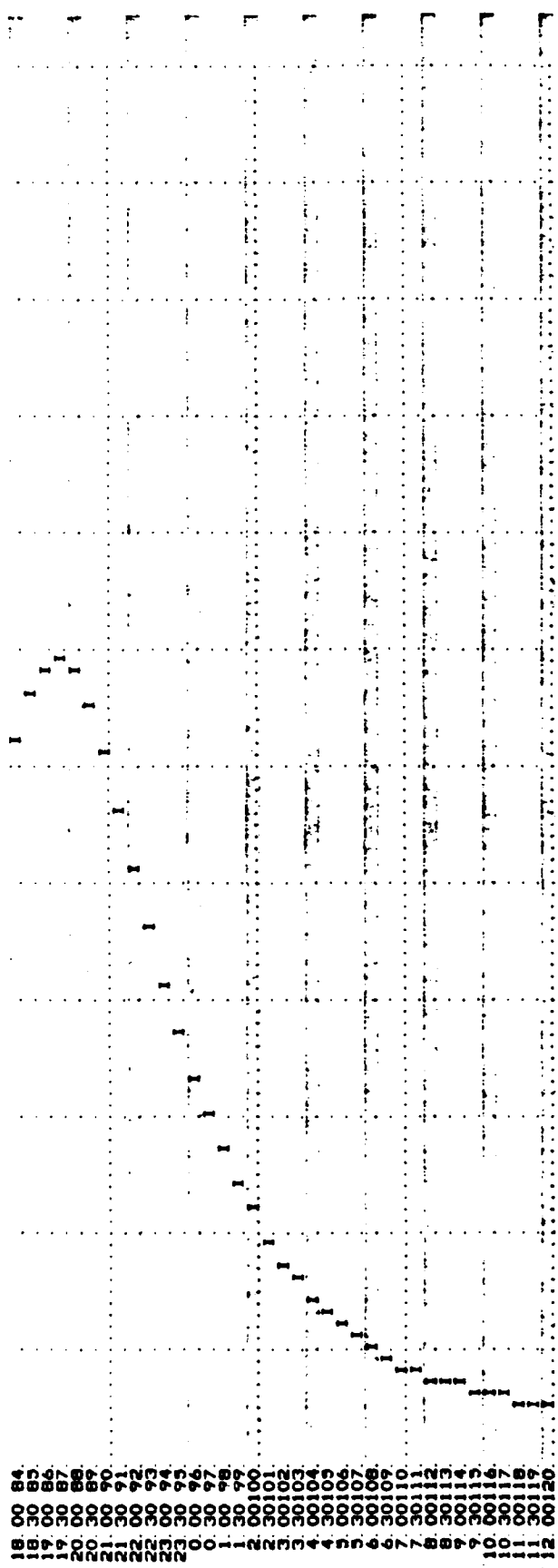
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| | PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|--------|-------|--------|---------|---------|--------|--------|
| CFS | 27979 | 11289 | 11289 | 4736 | 568305 | |
| CHS | 781 | 677 | 320 | 134 | 16093 | |
| INCHES | | 2.73 | 5.16 | 3.41 | | |
| MM | | 69.43 | 131.11 | 87.50 | | |
| AC-FT | | 1158 | 2392 | 2384 | 13790 | |
| AC-FT | | 1074 | 2730 | 2867 | 23484 | |
| | | | | | 28967 | |

Registration

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13 00 261
14 00 281
15 00 291
16 00 301
17 00 311
18 00 321
19 00 331
20 00 341
21 00 351
22 00 361
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26 00 401
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28 00 421
29 00 431
30 00 441
31 00 451
32 00 461
33 00 471
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35 00 491
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37 00 511
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39 00 531
40 00 541
41 00 551
42 00 561
43 00 571
44 00 581
45 00 591
46 00 601
47 00 611
48 00 621
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53 00 671
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56 00 701
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63 00 771
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65 00 791
66 00 801
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69 00 831
70 00 841
71 00 851
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85 00 991



#N/A#

| SUM OF 2 HYDROGRAPHS AT | | | | 1. PLAN 1 | | RTIO 8 | | PEAK | | | | TOTAL VOLUME | |
|-------------------------|-------|-------|-------|-----------|-------|--------|-------|-------|-------|-------|-------|--------------|-------|
| | 80 | 82 | 84 | 80 | 82 | 84 | 86 | 72 | 72 | 72 | 72 | 72 | 72 |
| 84 | 80 | 82 | 84 | 80 | 82 | 84 | 86 | 88 | 88 | 88 | 88 | 88 | 88 |
| 69 | 81 | 83 | 85 | 81 | 83 | 85 | 87 | 89 | 89 | 89 | 89 | 89 | 89 |
| 318 | 82 | 84 | 86 | 82 | 84 | 86 | 88 | 90 | 90 | 90 | 90 | 90 | 90 |
| 98 | 650 | 650 | 650 | 204 | 204 | 204 | 204 | 231 | 231 | 231 | 231 | 231 | 231 |
| 301 | 88 | 90 | 92 | 77 | 77 | 77 | 77 | 152 | 152 | 152 | 152 | 152 | 152 |
| 408 | 356 | 356 | 356 | 483 | 483 | 483 | 483 | 527 | 527 | 527 | 527 | 527 | 527 |
| 4730 | 1498 | 1498 | 1498 | 2326 | 2326 | 2326 | 2326 | 2814 | 2814 | 2814 | 2814 | 2814 | 2814 |
| 3040 | 1674 | 1674 | 1674 | 10220 | 10220 | 10220 | 10220 | 12234 | 12234 | 12234 | 12234 | 12234 | 12234 |
| 2833 | 2770 | 2770 | 2770 | 40957 | 40957 | 40957 | 40957 | 49873 | 49873 | 49873 | 49873 | 49873 | 49873 |
| 10391 | 24178 | 24178 | 24178 | 19460 | 19460 | 19460 | 19460 | 17475 | 17475 | 17475 | 17475 | 17475 | 17475 |
| 4373 | 8459 | 8459 | 8459 | 6934 | 6934 | 6934 | 6934 | 5834 | 5834 | 5834 | 5834 | 5834 | 5834 |
| | 3904 | 3904 | 3904 | 3494 | 3494 | 3494 | 3494 | 3156 | 3156 | 3156 | 3156 | 3156 | 3156 |
| | 3693 | 3693 | 3693 | 3309 | 3309 | 3309 | 3309 | 3030 | 3030 | 3030 | 3030 | 3030 | 3030 |
| | 4131 | 4131 | 4131 | 3309 | 3309 | 3309 | 3309 | 3030 | 3030 | 3030 | 3030 | 3030 | 3030 |

FLAHERTY GIAVARA ASSOCIATES, P.C.

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GVN

| STATION | INFLW (I) | OUTFLW (O) | AND OBSERVED FLOW (F) |
|---------|-----------|------------|-----------------------|
| 1 | 172 | 182 | 172 |
| 2 | 138 | 134 | 138 |
| 3 | 149 | 167 | 149 |
| 4 | 634 | 1369 | 634 |
| 5 | 194 | 186 | 194 |
| 6 | 602 | 648 | 602 |
| 7 | 1872 | 2339 | 1872 |
| 8 | 8815 | 7461 | 8815 |
| 9 | 40081 | 37266 | 40081 |
| 10 | 65378 | 56570 | 65378 |
| 11 | 23744 | 20581 | 23744 |
| 12 | 9264 | 8746 | 9264 |

CFB
CMB
INCHES
AC-FT
THOUS CU M

GVF

| STATION | INFLW (I) | OUTFLW (O) | AND OBSERVED FLOW (F) |
|---------|-----------|------------|-----------------------|
| 1 | 172 | 182 | 172 |
| 2 | 138 | 134 | 138 |
| 3 | 149 | 167 | 149 |
| 4 | 634 | 1369 | 634 |
| 5 | 194 | 186 | 194 |
| 6 | 602 | 648 | 602 |
| 7 | 1872 | 2339 | 1872 |
| 8 | 8815 | 7461 | 8815 |
| 9 | 40081 | 37266 | 40081 |
| 10 | 65378 | 56570 | 65378 |
| 11 | 23744 | 20581 | 23744 |
| 12 | 9264 | 8746 | 9264 |

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45 00 118
46 00 120

FLAHERTY GIARARA ASSOCIATES, P. C.

HYDROGRAPH ROUTING

OTSEGO LAKE ROUTING - MODIFIED PULS METHOD
 IECON ITAPE JPLT JPRI INAME ISTAGE IAUTO

ROUTING DATA IDPT IPMP LBTR
 IRES ISAME 1 0 0

LAG AMEKK X TSK STORA ISPRAT
 0 0.000 0.000 0.000 0.000 0.000

NSDPL 0
 1170.00 1171.00 1172.00 1172.50 1172.80 1173.00

1173.10 1174.00 1174.20 1174.50 1174.80 1175.00

23.40 171.80 313.20 483.80 678.70 732.20

1052.80 1317.30 1428.10 1897.20 13734.10 16108.50

27400. 37800. 112820.

1192. 1194. 1220.

1190. 1192. 1194. 1220.

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| | | | | | | | | | |
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| 20618 | 20636 | 20659 | 20684 | 20714 | 20730 | 20793 | 20841 | 20898 | 20960 |
| 23029 | 21104 | 21192 | 21303 | 21439 | 21596 | 21780 | 22001 | 22264 | 22628 |
| 23993 | 23974 | 24077 | 24644 | 25257 | 25897 | 26551 | 27202 | 27831 | 28423 |
| 28971 | 29468 | 29915 | 30314 | 30668 | 30983 | 31261 | 31508 | 31725 | 31918 |
| 32088 | 32238 | 32370 | 32488 | 32592 | 32683 | 32762 | 32832 | 32892 | 32948 |
| 32997 | 33041 | 33081 | 33117 | 33148 | 33176 | 33202 | 33224 | 33244 | 33261 |

PEAK OUTFLOW IS 747 AT TIME 80.00 HOURS

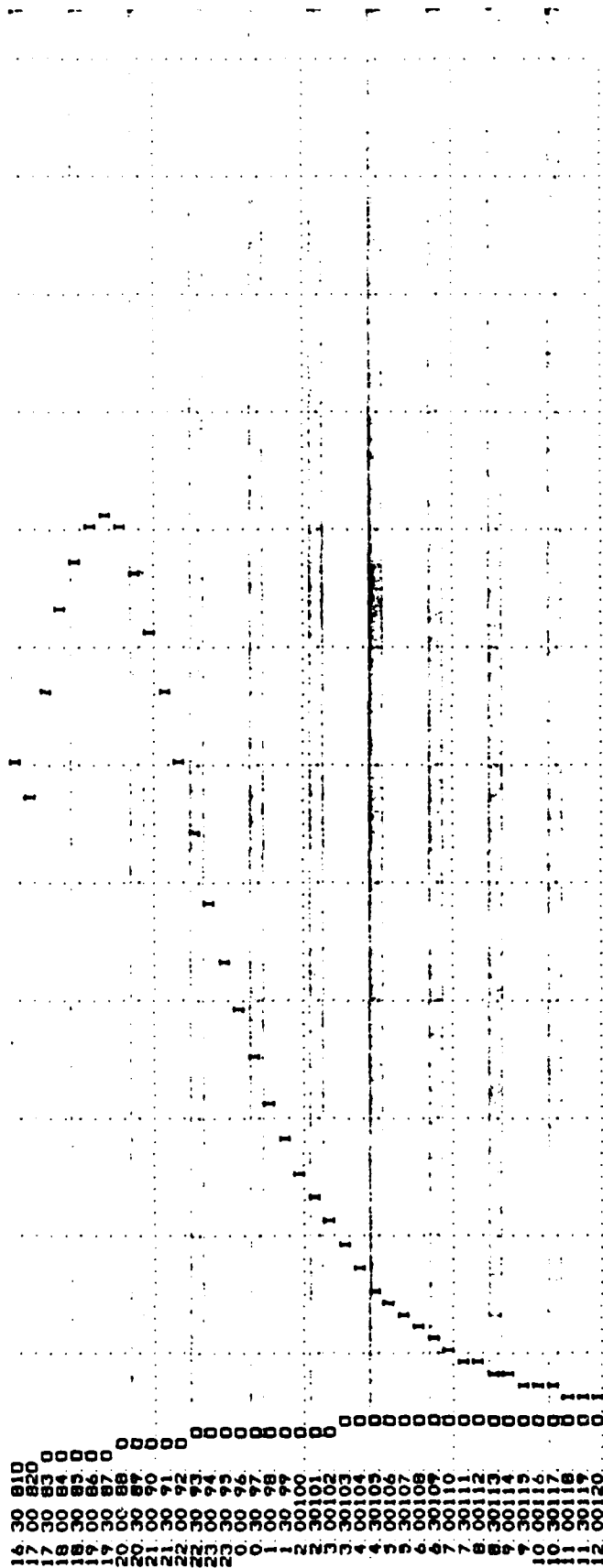
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------------|--------|---------|---------|--------------|
| 747 | 734 | 169 | 188 | 2897 |
| 21 | 21 | 13 | 5 | 840 |
| CFS | 0.08 | 0.21 | 0.22 | 0.22 |
| CMS | 2.13 | 5.44 | 5.46 | 5.46 |
| INCHES | 364 | 730 | 733 | 733 |
| MM | 449 | 1147 | 1151 | 1151 |
| AC-FT | | | | |
| THOUS CU M | | | | |

OVF

STATION 1

INFLOW(1), OUTFLOW(1) AND OBSERVED FLOW(*)

| | 2000 | 4000 | 6000 | 8000 | 10000 | 12000 | 14000 | 16000 | 18000 | 0 | 0 | 0 |
|----|------|------|------|------|-------|-------|-------|-------|-------|---|---|---|
| 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 30 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 2 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 3 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 4 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 5 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 6 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 7 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 8 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 9 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 10 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |
| 11 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

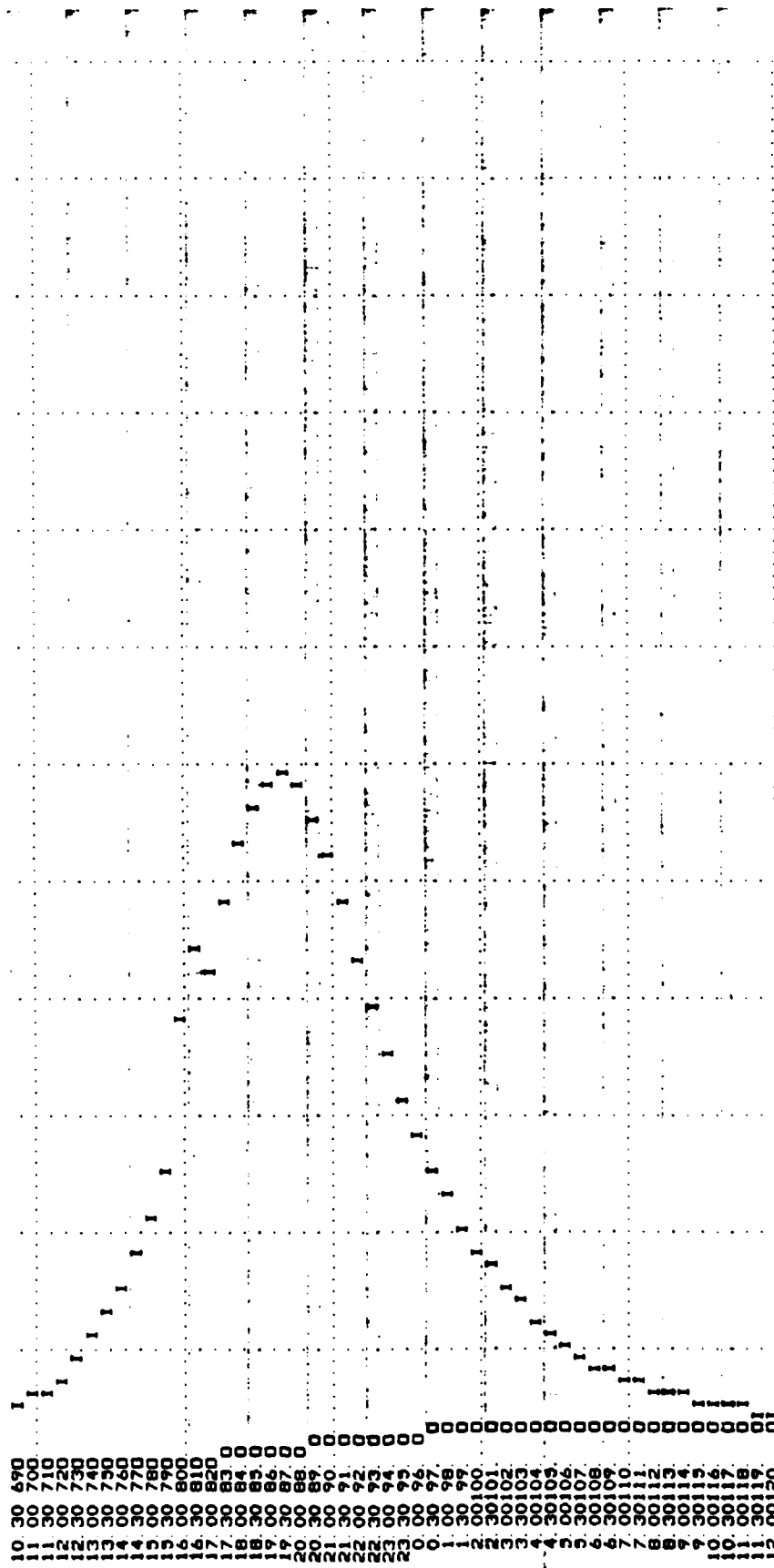


STATION 1, PLAN 1, RATIO 2
END-OF-PERIOD HYDROGRAPH ORDINATES

| OUTFLOW | 17 | 19 | 20 | 23 | 32 | 37 | 43 |
|-----------|----|----|----|----|----|----|----|
| 000-1-225 | 17 | 19 | 20 | 23 | 32 | 37 | 43 |

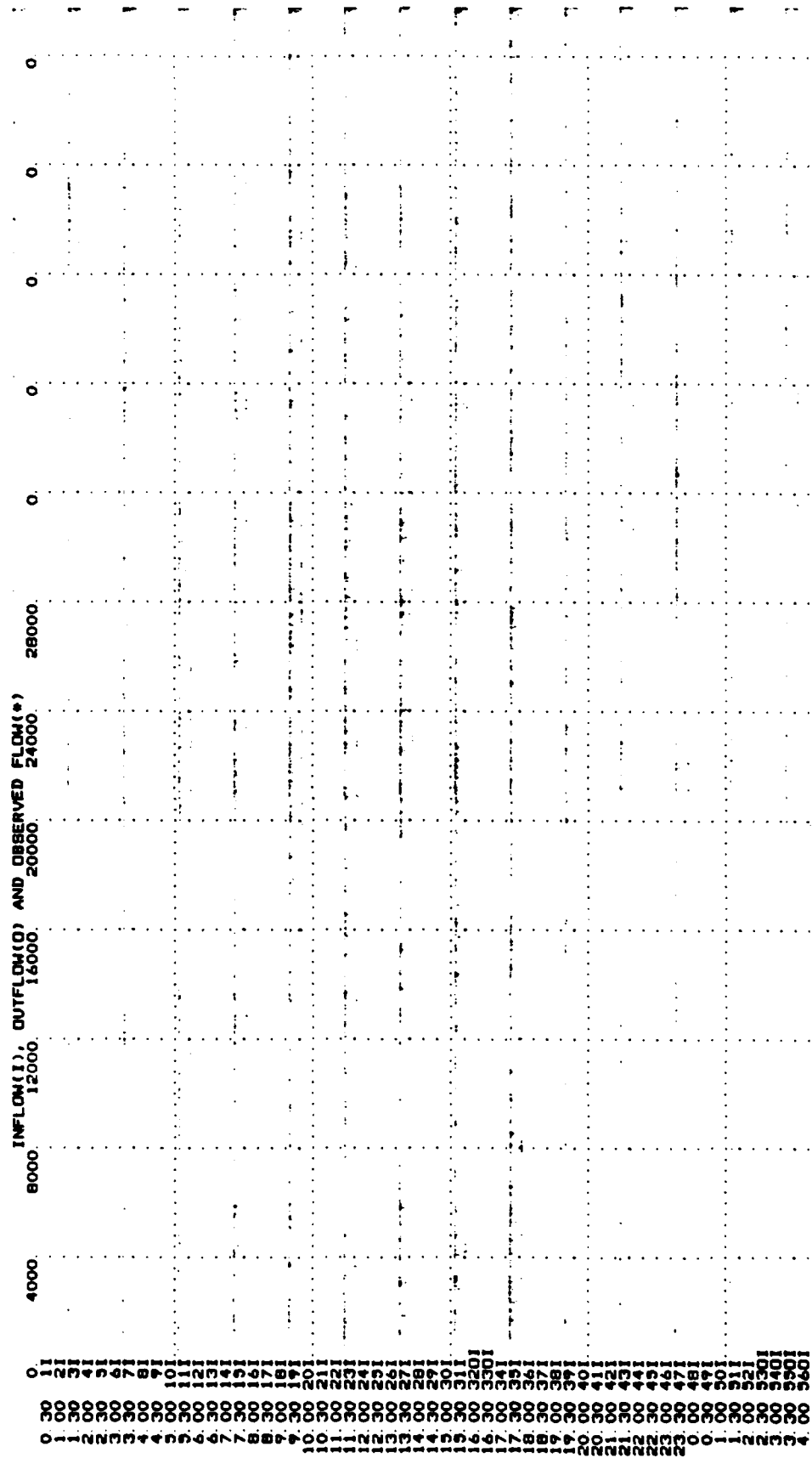
DVI

FLAHERTY GIAVARA ASSOCIATES, P. C.



DYN

STATION 1, PLAN 1, RATIO 3



FLAHERTY GIAVARA ASSOCIATES, P. C.

9 30115
10 00116
11 00117
12 00118
13 00119
14 00120

OVN

STATION 1. PLAN 1. RATIO 4
END-OF-PERIOD HYDROGRAPH ORDINATES

| OUTFLOW | STORAGE | STAGE |
|-------------|-------------|-------------|
| 000-1-222-4 | 000-1-222-4 | 000-1-222-4 |
| 11 | 11 | 11 |
| 12 | 12 | 12 |
| 13 | 13 | 13 |
| 14 | 14 | 14 |
| 15 | 15 | 15 |
| 16 | 16 | 16 |
| 17 | 17 | 17 |
| 18 | 18 | 18 |
| 19 | 19 | 19 |
| 20 | 20 | 20 |
| 21 | 21 | 21 |
| 22 | 22 | 22 |
| 23 | 23 | 23 |
| 24 | 24 | 24 |
| 25 | 25 | 25 |
| 26 | 26 | 26 |
| 27 | 27 | 27 |
| 28 | 28 | 28 |
| 29 | 29 | 29 |
| 30 | 30 | 30 |
| 31 | 31 | 31 |
| 32 | 32 | 32 |
| 33 | 33 | 33 |
| 34 | 34 | 34 |
| 35 | 35 | 35 |
| 36 | 36 | 36 |
| 37 | 37 | 37 |
| 38 | 38 | 38 |
| 39 | 39 | 39 |
| 40 | 40 | 40 |
| 41 | 41 | 41 |
| 42 | 42 | 42 |
| 43 | 43 | 43 |
| 44 | 44 | 44 |
| 45 | 45 | 45 |
| 46 | 46 | 46 |
| 47 | 47 | 47 |
| 48 | 48 | 48 |
| 49 | 49 | 49 |
| 50 | 50 | 50 |
| 51 | 51 | 51 |
| 52 | 52 | 52 |
| 53 | 53 | 53 |
| 54 | 54 | 54 |
| 55 | 55 | 55 |
| 56 | 56 | 56 |
| 57 | 57 | 57 |
| 58 | 58 | 58 |
| 59 | 59 | 59 |
| 60 | 60 | 60 |
| 61 | 61 | 61 |
| 62 | 62 | 62 |
| 63 | 63 | 63 |
| 64 | 64 | 64 |
| 65 | 65 | 65 |
| 66 | 66 | 66 |
| 67 | 67 | 67 |
| 68 | 68 | 68 |
| 69 | 69 | 69 |
| 70 | 70 | 70 |
| 71 | 71 | 71 |
| 72 | 72 | 72 |
| 73 | 73 | 73 |
| 74 | 74 | 74 |
| 75 | 75 | 75 |
| 76 | 76 | 76 |
| 77 | 77 | 77 |
| 78 | 78 | 78 |
| 79 | 79 | 79 |
| 80 | 80 | 80 |
| 81 | 81 | 81 |
| 82 | 82 | 82 |
| 83 | 83 | 83 |
| 84 | 84 | 84 |
| 85 | 85 | 85 |
| 86 | 86 | 86 |
| 87 | 87 | 87 |
| 88 | 88 | 88 |
| 89 | 89 | 89 |
| 90 | 90 | 90 |
| 91 | 91 | 91 |
| 92 | 92 | 92 |
| 93 | 93 | 93 |
| 94 | 94 | 94 |
| 95 | 95 | 95 |
| 96 | 96 | 96 |
| 97 | 97 | 97 |
| 98 | 98 | 98 |
| 99 | 99 | 99 |
| 100 | 100 | 100 |

PEAK OUTFLOW IS 1478 AT TIME 60.00 HOURS

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL | VOLUME |
|------|--------|---------|---------|-------|--------|
| 1476 | 1443 | 883 | 393 | 42530 | |
| 42 | 41 | 123 | 10 | 1203 | |
| | 0.16 | 0.40 | 0.41 | 0.41 | |
| | 4.19 | 10.26 | 10.30 | 10.30 | |
| | 716 | 1752 | 1758 | 1758 | |
| | 883 | 2162 | 2169 | 2169 | |

OVF

STATION 1

| | | 4000 | 8000 | 12000 | 16000 | 20000 | 24000 | 28000 | | |
|-------|------|--|------|-------|-------|-------|-------|-------|--|---|
| | | INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(S) | | | | | | | | |
| 0 | 11 | | | | | | | | | 0 |
| 30 | 12 | | | | | | | | | 0 |
| 1.00 | 31 | | | | | | | | | 0 |
| 1.30 | 41 | | | | | | | | | 0 |
| 2.00 | 51 | | | | | | | | | 0 |
| 2.30 | 61 | | | | | | | | | 0 |
| 3.00 | 71 | | | | | | | | | 0 |
| 3.30 | 81 | | | | | | | | | 0 |
| 4.00 | 91 | | | | | | | | | 0 |
| 4.30 | 101 | | | | | | | | | 0 |
| 5.00 | 111 | | | | | | | | | 0 |
| 5.30 | 121 | | | | | | | | | 0 |
| 6.00 | 131 | | | | | | | | | 0 |
| 6.30 | 141 | | | | | | | | | 0 |
| 7.00 | 151 | | | | | | | | | 0 |
| 7.30 | 161 | | | | | | | | | 0 |
| 8.00 | 171 | | | | | | | | | 0 |
| 8.30 | 181 | | | | | | | | | 0 |
| 9.00 | 191 | | | | | | | | | 0 |
| 9.30 | 201 | | | | | | | | | 0 |
| 10.00 | 211 | | | | | | | | | 0 |
| 10.30 | 221 | | | | | | | | | 0 |
| 11.00 | 231 | | | | | | | | | 0 |
| 11.30 | 241 | | | | | | | | | 0 |
| 12.00 | 251 | | | | | | | | | 0 |
| 12.30 | 261 | | | | | | | | | 0 |
| 13.00 | 271 | | | | | | | | | 0 |
| 13.30 | 281 | | | | | | | | | 0 |
| 14.00 | 291 | | | | | | | | | 0 |
| 14.30 | 301 | | | | | | | | | 0 |
| 15.00 | 311 | | | | | | | | | 0 |
| 15.30 | 3201 | | | | | | | | | 0 |
| 16.00 | 3301 | | | | | | | | | 0 |
| 16.30 | 341 | | | | | | | | | 0 |
| 17.00 | 351 | | | | | | | | | 0 |
| 17.30 | 361 | | | | | | | | | 0 |
| 18.00 | 371 | | | | | | | | | 0 |
| 18.30 | 381 | | | | | | | | | 0 |
| 19.00 | 391 | | | | | | | | | 0 |
| 19.30 | 401 | | | | | | | | | 0 |
| 20.00 | 411 | | | | | | | | | 0 |
| 20.30 | 421 | | | | | | | | | 0 |
| 21.00 | 431 | | | | | | | | | 0 |
| 21.30 | 44 | | | | | | | | | 0 |

FLAHERTY GIAVARA ASSOCIATES, P. C.

22 30 431
23 00 441
24 00 451
25 00 461
26 00 471
27 00 481
28 00 491
29 00 501
30 00 511
31 00 521
32 00 531
33 00 541
34 00 551
35 00 561
36 00 571
37 00 581
38 00 591
39 00 601
40 00 611
41 00 621
42 00 631
43 00 641
44 00 651
45 00 661
46 00 671
47 00 681
48 00 691
49 00 701
50 00 711
51 00 721
52 00 731
53 00 741
54 00 751
55 00 761
56 00 771
57 00 781
58 00 791
59 00 801
60 00 811
61 00 821
62 00 831
63 00 841
64 00 851
65 00 861
66 00 871
67 00 881
68 00 891
69 00 901
70 00 911
71 00 921
72 00 931
73 00 941
74 00 951
75 00 961
76 00 971
77 00 981
78 00 991
79 00 1001
80 00 1011
81 00 1021
82 00 1031
83 00 1041
84 00 1051
85 00 1061
86 00 1071
87 00 1081
88 00 1091
89 00 1101
90 00 1111
91 00 1121
92 00 1131
93 00 1141
94 00 1151
95 00 1161
96 00 1171
97 00 1181
98 00 1191
99 00 1201
100 00 1211
101 00 1221
102 00 1231

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STATION 1, PLAN 1, RATIO 3
END-OF-PERIOD HYDROGRAPH ORDINATES

[illegible]

FLAHERTY GIAVARA ASSOCIATES, P. C.

16 30 3301
17 00 341
18 00 351
19 00 361
20 00 371
21 00 381
22 00 391
23 00 401
24 00 411
25 00 421
26 00 431
27 00 441
28 00 451
29 00 461
30 00 471
31 00 481
32 00 491
33 00 501
34 00 511
35 00 521
36 00 531
37 00 541
38 00 551
39 00 561
40 00 571
41 00 581
42 00 591
43 00 601
44 00 611
45 00 621
46 00 631
47 00 641
48 00 651
49 00 661
50 00 671
51 00 681
52 00 691
53 00 701
54 00 711
55 00 721
56 00 731
57 00 741
58 00 751
59 00 761
60 00 771
61 00 781
62 00 791
63 00 801
64 00 811
65 00 821
66 00 831
67 00 841
68 00 851
69 00 861
70 00 871
71 00 881
72 00 891
73 00 901

| | | | | | | | | |
|--------|--------|--------|--------|--------|--------|--------|--------|--------|
| 20572 | 20594 | 20598 | 20600 | 20601 | 20603 | 20604 | 20606 | 20611 |
| 20618 | 20626 | 20644 | 20655 | 20666 | 20679 | 20693 | 20708 | 20724 |
| 20745 | 20775 | 20853 | 20903 | 20963 | 21033 | 21114 | 21208 | 21312 |
| 21427 | 21590 | 21882 | 22104 | 22361 | 22666 | 23030 | 23466 | 24062 |
| 24825 | 25617 | 27378 | 28387 | 29441 | 30517 | 31587 | 32621 | 33595 |
| 34494 | 35310 | 36696 | 37275 | 37787 | 38240 | 38639 | 38991 | 39299 |
| 39569 | 39806 | 40194 | 40350 | 40484 | 40599 | 40699 | 40785 | 40857 |
| 40919 | 40973 | 41059 | 41092 | 41120 | 41142 | 41159 | 41172 | 41182 |
| | | | STAGE | | | | | |
| 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 |
| 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 |
| 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.0 |
| 1190.0 | 1190.0 | 1190.0 | 1190.0 | 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 |
| 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 | 1190.1 |
| 1190.2 | 1190.3 | 1190.3 | 1190.4 | 1190.4 | 1190.4 | 1190.4 | 1190.2 | 1190.2 |
| 1191.0 | 1191.2 | 1191.4 | 1191.6 | 1192.0 | 1192.3 | 1192.3 | 1192.7 | 1192.7 |
| 1193.1 | 1193.3 | 1193.4 | 1193.5 | 1193.8 | 1193.9 | 1194.0 | 1194.0 | 1194.1 |
| 1194.2 | 1194.3 | 1194.3 | 1194.3 | 1194.4 | 1194.4 | 1194.5 | 1194.5 | 1194.6 |
| 1194.6 | 1194.6 | 1194.6 | 1194.6 | 1194.7 | 1194.7 | 1194.7 | 1194.7 | 1194.7 |

PEAK OUTFLOW IS 1716 AT TIME 60.00 HOURS

| | | | | |
|-------------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 1716 | 1682 | 1001 | 402 | 48193 |
| 49 | 48 | 28 | 11 | 1363 |
| CBS | 0.17 | 0.46 | 0.46 | 0.46 |
| CBS | 4.88 | 11.62 | 11.66 | 11.66 |
| INCHES | 834 | 1785 | 1771 | 1771 |
| AC-FT | 1029 | 2449 | 2456 | 2456 |
| THOUS CU FT | | | | |

OVF

STATION 1

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

0 11
1 12
2 21
3 41
4 51
5 61
6 71
7 81
8 91
9 101
10 111
11 121
12 131
13 141
14 151
15 161
16 171
17 181
18 191
19 201

4000.

8000.

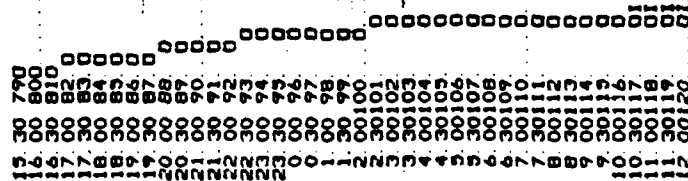
16000.

28000.

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#DND#

STATION 1, PLAN 1, RATIO 7
END-OF-PERIOD HYDROGRAPH ORDINATES

OUTFLOW

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ဝဝ-ကနဏ

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00-NNNN

00-NNNN

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00-NNNN

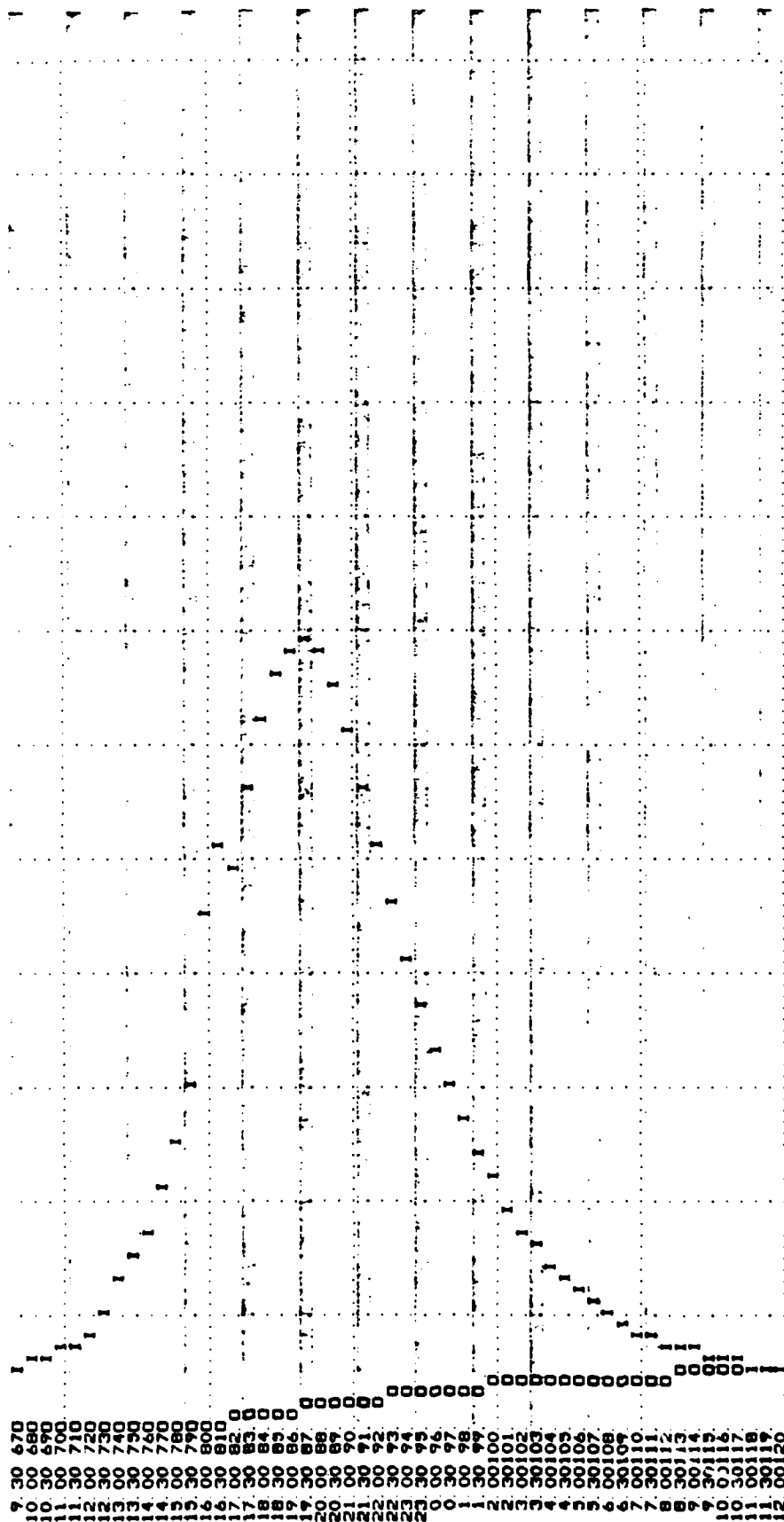
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FLAHERTY GIAVARA ASSOCIATES, P. C.



OVN

STATION 1. PLAN 1, RATIO 8
END-OF-PERIOD HYDROGRAPH ORDINATES

| OUTFLOW | STORAGE | STAGE | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|---------|---------|-------|--------|---------|---------|--------------|
| 0.00 | 20443 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20471 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20501 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20570 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20670 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20720 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20752 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21923 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 27023 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 41483 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 48888 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50270 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20446 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20473 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20504 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20590 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20670 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20720 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20753 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20920 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22140 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22920 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47427 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50257 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20450 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20475 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20507 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20616 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20683 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21020 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22322 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22920 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47427 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50253 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20453 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20478 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20510 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20634 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20686 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21084 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22645 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22920 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47427 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50250 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20456 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20481 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20514 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20645 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20690 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21129 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 22920 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47427 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50257 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20459 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20485 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20521 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20655 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20692 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20723 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21247 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23370 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 24072 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47427 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50256 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20462 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20488 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20524 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20662 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20698 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20817 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21336 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 23380 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 24380 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 37313 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 37477 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 47114 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50028 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50133 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50153 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20467 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20494 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20527 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20670 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20700 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 20863 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21421 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21779 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 21779 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 25936 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 40337 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 48343 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50241 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |
| 0.00 | 50108 | 1190 | 0.00 | 0.00 | 0.00 | 1190 |

PEAK OUTFLOW IS 4092 AT TIME 36.50 HOURS

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|------------|--------|---------|---------|--------------|
| 4092 | 4077 | 2421 | 770 | 116430 |
| 116 | 115 | 69 | 27 | 3297 |
| CFS | | | | |
| CMS | | | | |
| INCHES | | | | |
| MM | | | | |
| AC-FT | | | | |
| THOUS CU M | | | | |

OVF

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(O)

| 5000 | 10000 | 15000 | 20000 | 25000 | 30000 | 35000 | 40000 | 45000 | 0 |
|------|-------|-------|-------|-------|-------|-------|-------|-------|---|
| 0 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 0 |
| 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 30 | 0 |
| 60 | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 60 | 0 |
| 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 0 |
| 120 | 120 | 120 | 120 | 120 | 120 | 120 | 120 | 120 | 0 |
| 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 150 | 0 |
| 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 180 | 0 |
| 210 | 210 | 210 | 210 | 210 | 210 | 210 | 210 | 210 | 0 |
| 240 | 240 | 240 | 240 | 240 | 240 | 240 | 240 | 240 | 0 |
| 270 | 270 | 270 | 270 | 270 | 270 | 270 | 270 | 270 | 0 |
| 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 300 | 0 |
| 330 | 330 | 330 | 330 | 330 | 330 | 330 | 330 | 330 | 0 |
| 360 | 360 | 360 | 360 | 360 | 360 | 360 | 360 | 360 | 0 |
| 390 | 390 | 390 | 390 | 390 | 390 | 390 | 390 | 390 | 0 |
| 420 | 420 | 420 | 420 | 420 | 420 | 420 | 420 | 420 | 0 |
| 450 | 450 | 450 | 450 | 450 | 450 | 450 | 450 | 450 | 0 |
| 480 | 480 | 480 | 480 | 480 | 480 | 480 | 480 | 480 | 0 |
| 510 | 510 | 510 | 510 | 510 | 510 | 510 | 510 | 510 | 0 |
| 540 | 540 | 540 | 540 | 540 | 540 | 540 | 540 | 540 | 0 |

3301
3003601
4003701
5003801
6003901
7004001
800410
900420
1000430
1100440
1200450
1300460
1400470
1500480
1600490
1700500
1800510
1900520
2000530
2100540
2200550
2300560
2400570
2500580
2600590
2700600
2800610
2900620
3000630
3100640
3200650
3300660
3400670
3500680
3600690
3700700
3800710
3900720
4000730
4100740
4200750
4300760
4400770
4500780
4600790
4700800
4800810
4900820
5000830
5100840
5200850
5300860
5400870
5500880
5600890
5700900
5800910
5900920
6000930
6100940
6200950
6300960
6400970
6500980
6600990
6701000
6801010
6901020
7001030
7101040
7201050
7301060
7401070
7501080
7601090
7701100
7801110
7901120

8 30113.
9 00114.
10 30115.
10 00116.
10 30117.
11 00118.
11 30119.
12 00120.

OVN

STATION 1. PLAN 1. RATIO 9
END-OF-PERIOD HYDROGRAPH ORDINATES

| OUTFLOW | | STORAGE | | STAGE | |
|---------|-----|---------|-----|-------|---|
| 0 | 1 | 0 | 1 | 0 | 1 |
| 0 | 1 | 0 | 1 | 0 | 1 |
| 2 | 2 | 1 | 2 | 0 | 1 |
| 3 | 3 | 2 | 3 | 0 | 1 |
| 4 | 4 | 3 | 4 | 0 | 1 |
| 5 | 5 | 4 | 5 | 0 | 1 |
| 6 | 6 | 5 | 6 | 0 | 1 |
| 7 | 7 | 6 | 7 | 0 | 1 |
| 8 | 8 | 7 | 8 | 0 | 1 |
| 9 | 9 | 8 | 9 | 0 | 1 |
| 10 | 10 | 9 | 10 | 0 | 1 |
| 11 | 11 | 10 | 11 | 0 | 1 |
| 12 | 12 | 11 | 12 | 0 | 1 |
| 13 | 13 | 12 | 13 | 0 | 1 |
| 14 | 14 | 13 | 14 | 0 | 1 |
| 15 | 15 | 14 | 15 | 0 | 1 |
| 16 | 16 | 15 | 16 | 0 | 1 |
| 17 | 17 | 16 | 17 | 0 | 1 |
| 18 | 18 | 17 | 18 | 0 | 1 |
| 19 | 19 | 18 | 19 | 0 | 1 |
| 20 | 20 | 19 | 20 | 0 | 1 |
| 21 | 21 | 20 | 21 | 0 | 1 |
| 22 | 22 | 21 | 22 | 0 | 1 |
| 23 | 23 | 22 | 23 | 0 | 1 |
| 24 | 24 | 23 | 24 | 0 | 1 |
| 25 | 25 | 24 | 25 | 0 | 1 |
| 26 | 26 | 25 | 26 | 0 | 1 |
| 27 | 27 | 26 | 27 | 0 | 1 |
| 28 | 28 | 27 | 28 | 0 | 1 |
| 29 | 29 | 28 | 29 | 0 | 1 |
| 30 | 30 | 29 | 30 | 0 | 1 |
| 31 | 31 | 30 | 31 | 0 | 1 |
| 32 | 32 | 31 | 32 | 0 | 1 |
| 33 | 33 | 32 | 33 | 0 | 1 |
| 34 | 34 | 33 | 34 | 0 | 1 |
| 35 | 35 | 34 | 35 | 0 | 1 |
| 36 | 36 | 35 | 36 | 0 | 1 |
| 37 | 37 | 36 | 37 | 0 | 1 |
| 38 | 38 | 37 | 38 | 0 | 1 |
| 39 | 39 | 38 | 39 | 0 | 1 |
| 40 | 40 | 39 | 40 | 0 | 1 |
| 41 | 41 | 40 | 41 | 0 | 1 |
| 42 | 42 | 41 | 42 | 0 | 1 |
| 43 | 43 | 42 | 43 | 0 | 1 |
| 44 | 44 | 43 | 44 | 0 | 1 |
| 45 | 45 | 44 | 45 | 0 | 1 |
| 46 | 46 | 45 | 46 | 0 | 1 |
| 47 | 47 | 46 | 47 | 0 | 1 |
| 48 | 48 | 47 | 48 | 0 | 1 |
| 49 | 49 | 48 | 49 | 0 | 1 |
| 50 | 50 | 49 | 50 | 0 | 1 |
| 51 | 51 | 50 | 51 | 0 | 1 |
| 52 | 52 | 51 | 52 | 0 | 1 |
| 53 | 53 | 52 | 53 | 0 | 1 |
| 54 | 54 | 53 | 54 | 0 | 1 |
| 55 | 55 | 54 | 55 | 0 | 1 |
| 56 | 56 | 55 | 56 | 0 | 1 |
| 57 | 57 | 56 | 57 | 0 | 1 |
| 58 | 58 | 57 | 58 | 0 | 1 |
| 59 | 59 | 58 | 59 | 0 | 1 |
| 60 | 60 | 59 | 60 | 0 | 1 |
| 61 | 61 | 60 | 61 | 0 | 1 |
| 62 | 62 | 61 | 62 | 0 | 1 |
| 63 | 63 | 62 | 63 | 0 | 1 |
| 64 | 64 | 63 | 64 | 0 | 1 |
| 65 | 65 | 64 | 65 | 0 | 1 |
| 66 | 66 | 65 | 66 | 0 | 1 |
| 67 | 67 | 66 | 67 | 0 | 1 |
| 68 | 68 | 67 | 68 | 0 | 1 |
| 69 | 69 | 68 | 69 | 0 | 1 |
| 70 | 70 | 69 | 70 | 0 | 1 |
| 71 | 71 | 70 | 71 | 0 | 1 |
| 72 | 72 | 71 | 72 | 0 | 1 |
| 73 | 73 | 72 | 73 | 0 | 1 |
| 74 | 74 | 73 | 74 | 0 | 1 |
| 75 | 75 | 74 | 75 | 0 | 1 |
| 76 | 76 | 75 | 76 | 0 | 1 |
| 77 | 77 | 76 | 77 | 0 | 1 |
| 78 | 78 | 77 | 78 | 0 | 1 |
| 79 | 79 | 78 | 79 | 0 | 1 |
| 80 | 80 | 79 | 80 | 0 | 1 |
| 81 | 81 | 80 | 81 | 0 | 1 |
| 82 | 82 | 81 | 82 | 0 | 1 |
| 83 | 83 | 82 | 83 | 0 | 1 |
| 84 | 84 | 83 | 84 | 0 | 1 |
| 85 | 85 | 84 | 85 | 0 | 1 |
| 86 | 86 | 85 | 86 | 0 | 1 |
| 87 | 87 | 86 | 87 | 0 | 1 |
| 88 | 88 | 87 | 88 | 0 | 1 |
| 89 | 89 | 88 | 89 | 0 | 1 |
| 90 | 90 | 89 | 90 | 0 | 1 |
| 91 | 91 | 90 | 91 | 0 | 1 |
| 92 | 92 | 91 | 92 | 0 | 1 |
| 93 | 93 | 92 | 93 | 0 | 1 |
| 94 | 94 | 93 | 94 | 0 | 1 |
| 95 | 95 | 94 | 95 | 0 | 1 |
| 96 | 96 | 95 | 96 | 0 | 1 |
| 97 | 97 | 96 | 97 | 0 | 1 |
| 98 | 98 | 97 | 98 | 0 | 1 |
| 99 | 99 | 98 | 99 | 0 | 1 |
| 100 | 100 | 99 | 100 | 0 | 1 |

PEAK OUTFLOW IS 12831 AT TIME 53.50 HOURS

| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
|-----------|--------|---------|---------|--------------|
| 12831 | 12728 | 8037 | 3280 | 38637 |
| 363 | 360 | 228 | 91 | 1091 |
| CFS | 1.45 | 3.67 | 3.68 | 3.68 |
| CMH | 36.96 | 93.34 | 93.49 | 93.49 |
| INCHES | 36.96 | 93.34 | 93.49 | 93.49 |
| AC-FT | 9312 | 12791 | 12760 | 12760 |
| THOUS CUM | 7785 | 12623 | 12694 | 12694 |

OVF

STATION

INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*)

| 0 | 10000 | 20000 | 30000 | 40000 | 50000 | 60000 | 70000 | 80000 | 90000 | 0 |
|----|-------|-------|-------|-------|-------|-------|-------|-------|-------|---|
| 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 0 |
| 1 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 2 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 3 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 4 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 5 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 6 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 7 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 8 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 9 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 10 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 11 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 12 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 13 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 14 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 15 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 16 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 17 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 18 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 19 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 20 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 21 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 22 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 23 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 24 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 25 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 26 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 27 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 28 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 29 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 30 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 31 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 32 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 33 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 34 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 35 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 36 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 37 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 38 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 39 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 40 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 41 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| 42 | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |


```

2 30101      I
3 30102      I
4 30103      I
5 30104      I
6 30105      I
7 30106      I
8 30107      I
9 30108      I
10 30109      I
11 30110      I
12 30111      I
13 30112      I
14 30113      I
15 30114      I
16 30115      I
17 30116      I
18 30117      I
19 30118      I
20 30119      I
21 30120      I

```

DOWN

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
 AREA IN SQUARE FEET (SQUARE KILOMETERS)

| OPERATION | STATION | AREA | PLAN | RATIO 1
0.20 | RATIO 2
0.25 | RATIO 3
0.30 | RATIO 4
0.31 | RATIO 5
0.32 | RATIO 6
0.33 | RATIO 7
0.34 | RATIO 8
0.50 | RATIO 9
1.00 |
|---------------|---------|------------------|------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|-------------------|--------------------|
| HYDROGRAPH AT | 1 | 23.84
(61.74) | 1 | 5084
(143.40) | 7343
(207.93) | 7578
(215.10) | 7847
(222.27) | 8103
(229.44) | 8356
(236.61) | 8607
(243.78) | 12660
(358.50) | 25320
(716.99) |
| HYDROGRAPH AT | 1 | 13.03
(33.75) | 1 | 3007
(85.15) | 4360
(123.46) | 4510
(127.72) | 4661
(131.98) | 4811
(136.23) | 4961
(140.49) | 5112
(144.75) | 7517
(212.86) | 15034
(425.73) |
| 2 COMBINED | 1 | 36.87
(95.49) | 1 | 7794
(226.36) | 11591
(328.22) | 11991
(339.54) | 12390
(350.85) | 12790
(362.17) | 13190
(373.49) | 13587
(384.81) | 19984
(565.89) | 39967
(1131.79) |
| HYDROGRAPH AT | 1 | 17.47
(45.25) | 1 | 3103
(87.93) | 4503
(127.50) | 4638
(131.87) | 4813
(136.29) | 4968
(140.69) | 5124
(145.08) | 5279
(149.48) | 7763
(219.82) | 15326
(439.65) |
| 2 COMBINED | 1 | 34.34
(90.74) | 1 | 10797
(310.31) | 15870
(449.95) | 16438
(465.47) | 16986
(480.98) | 17534
(496.50) | 18082
(512.02) | 18630
(527.53) | 27396
(775.78) | 54793
(1551.56) |
| HYDROGRAPH AT | 1 | 4.77
(12.35) | 1 | 1088
(30.80) | 1577
(44.66) | 1631
(46.20) | 1686
(47.74) | 1740
(49.28) | 1793
(50.82) | 1849
(52.36) | 2719
(77.00) | 5438
(153.99) |

| | | | | | | | | | | | | | | | | | | | | |
|---------------|---|---------|-------|---------|-------|---------|-------|---------|-------|---------|-------|---------|---|---------|---|---------|---|----------|---|----------|
| 2 COMBINED | 1 | 59.11 | 12017 | 17425 | 18025 | 18624 | 19227 | 19828 | 20429 | 30042 | 60083 | | | | | | | | | |
| | (| 153.09) | (| 340.28) | (| 493.41) | (| 510.42) | (| 544.45) | (| 561.47) | (| 578.48) | (| 850.70) | (| 1701.41) | | |
| HYDROGRAPH AT | 1 | 5.36 | 1475 | 2138 | 2212 | 2286 | 2359 | 2433 | 2507 | 3687 | 7373 | | | | | | | | | |
| | (| 14.40) | (| 41.76) | (| 60.55) | (| 62.64) | (| 64.72) | (| 66.81) | (| 68.90) | (| 70.99) | (| 104.39) | (| 208.78) |
| 2 COMBINED | 1 | 64.67 | 13265 | 17235 | 19898 | 20561 | 21225 | 21888 | 22551 | 33164 | 66327 | | | | | | | | | |
| | (| 167.49) | (| 375.64) | (| 544.67) | (| 563.45) | (| 582.23) | (| 601.02) | (| 619.80) | (| 638.58) | (| 939.09) | (| 1878.18) |
| HYDROGRAPH AT | 1 | 10.33 | 2777 | 4026 | 4165 | 4304 | 4443 | 4582 | 4720 | 6942 | 13883 | | | | | | | | | |
| | (| 26.75) | (| 78.63) | (| 114.01) | (| 117.94) | (| 121.87) | (| 125.80) | (| 129.73) | (| 133.67) | (| 196.57) | (| 393.14) |
| 2 COMBINED | 1 | 75.00 | 15832 | 22456 | 23748 | 24535 | 25331 | 26123 | 26914 | 39580 | 79157 | | | | | | | | | |
| | (| 194.25) | (| 448.31) | (| 650.05) | (| 672.46) | (| 694.88) | (| 717.29) | (| 739.71) | (| 762.12) | (| 1120.77) | (| 2241.53) |
| HYDROGRAPH AT | 1 | 6.38 | 4123 | 6022 | 6229 | 6437 | 6645 | 6852 | 7060 | 10382 | 20764 | | | | | | | | | |
| | (| 16.52) | (| 117.60) | (| 170.51) | (| 176.39) | (| 182.27) | (| 188.15) | (| 194.03) | (| 199.91) | (| 293.99) | (| 587.98) |
| 2 COMBINED | 1 | 81.38 | 16223 | 23523 | 24334 | 25145 | 25956 | 26767 | 27578 | 40527 | 81113 | | | | | | | | | |
| | (| 210.77) | (| 459.38) | (| 666.09) | (| 689.06) | (| 712.03) | (| 735.00) | (| 757.97) | (| 780.94) | (| 1148.44) | (| 2296.87) |
| ROUTED TO | 1 | 81.38 | 747 | 1311 | 1383 | 1478 | 1598 | 1716 | 1835 | 4092 | 12831 | | | | | | | | | |
| | (| 210.77) | (| 21.15) | (| 37.14) | (| 39.16) | (| 41.18) | (| 43.20) | (| 45.22) | (| 47.24) | (| 115.89) | (| 363.32) |

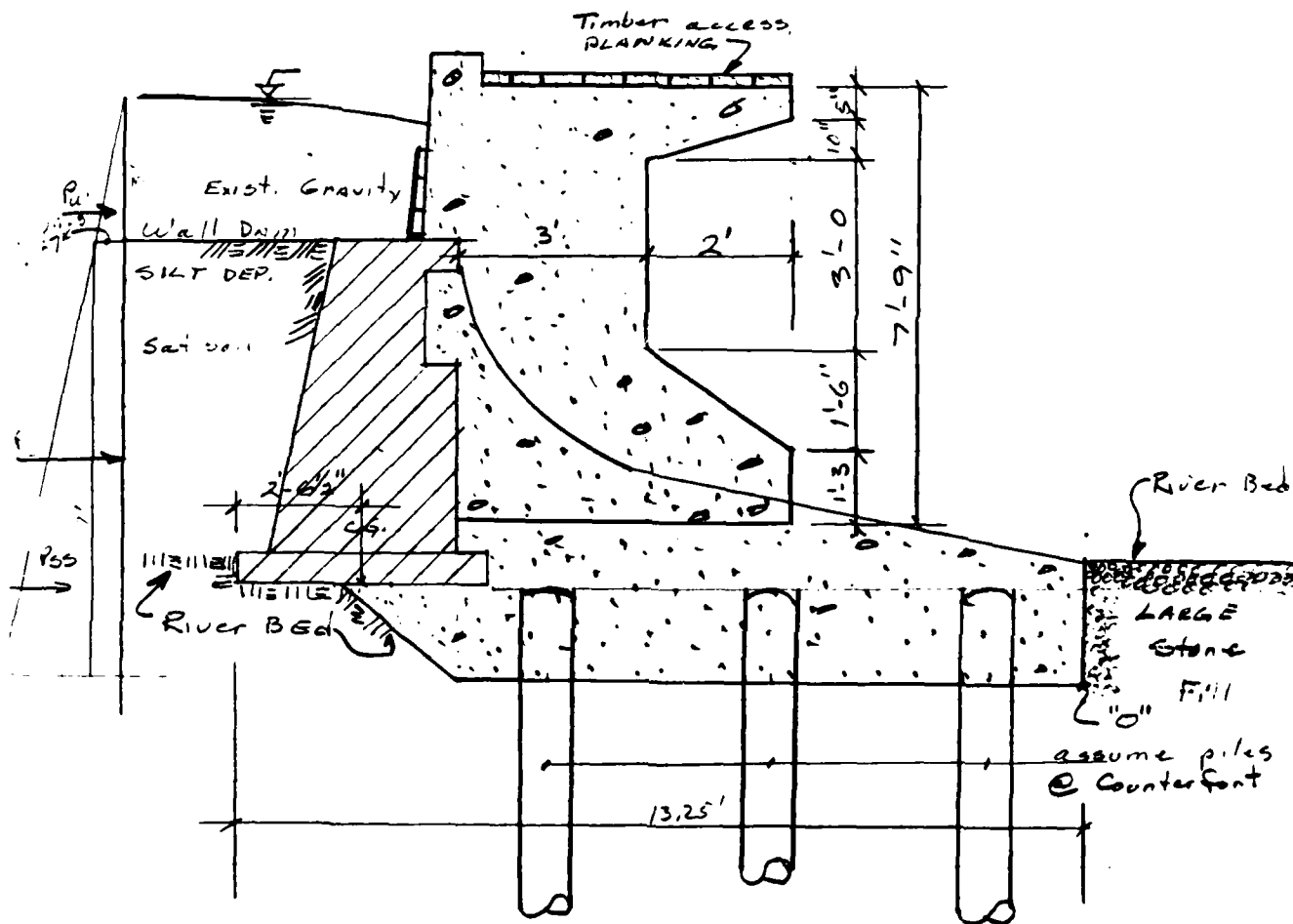
SUMMARY OF DAM SAFETY ANALYSIS

| | | | | |
|--------|-----------|---------------|----------------|------------|
| PLAN 1 | ELEVATION | INITIAL VALUE | SPILLWAY CREST | TOP OF DAM |
| | STORAGE | 1190.00 | 1190.00 | 1194.20 |
| | OUTFLOW | 20440.0 | 20440.0 | 39800.0 |

| RATIO OF PMF | MAXIMUM RESERVOIR W.S. ELEV | MAXIMUM DEPTH OVER DAM | MAXIMUM STORAGE AC-FT | MAXIMUM OUTFLOW CFS | DURATION OVER TOP HOURS | TIME OF MAX OUTFLOW HOURS | TIME OF FAILURE HOURS |
|--------------|-----------------------------|------------------------|-----------------------|---------------------|-------------------------|---------------------------|-----------------------|
| 0.20 | 1193.99 | 0.00 | 33261 | 747 | 0.00 | 0.00 | 0.00 |
| 0.25 | 1193.99 | 0.00 | 38791 | 1311 | 0.00 | 0.00 | 0.00 |
| 0.30 | 1194.12 | 0.00 | 39410 | 1383 | 0.00 | 0.00 | 0.00 |
| 0.31 | 1194.29 | 0.09 | 40041 | 1478 | 4.00 | 0.00 | 0.00 |
| 0.32 | 1194.47 | 0.27 | 40618 | 1578 | 7.50 | 0.00 | 0.00 |
| 0.33 | 1194.69 | 0.49 | 41183 | 1716 | 9.50 | 0.00 | 0.00 |
| 0.34 | 1194.87 | 0.67 | 41751 | 1835 | 10.50 | 0.00 | 0.00 |
| 0.50 | 1197.91 | 3.71 | 50293 | 4092 | 13.50 | 0.00 | 0.00 |
| 1.00 | 1206.87 | 12.69 | 75709 | 12831 | 18.50 | 23.50 | 0.00 |

 FLOOD HYDROGRAPH PACKAGE (HEC-1)
 DAM SAFETY VERSION JULY 1978
 LAST MODIFICATION 26 FEB 79

APPENDIX D
STRUCTURAL STABILITY ANALYSIS



$$P_w = \frac{3^2}{2} \times 0.0624 = 0.28 \text{ K/FT}$$

$$P_2 = .197 \times 7' = 1.31 \text{ K/FT}$$

$$P_{ss} = .056 \times \frac{7^2}{2} = 1.35 \text{ K/FT}$$

$$\Sigma FH \approx 3 \text{ K/FT}$$

$$M_{OT} = .28 \times 8' + 1.31 \times 3.5' + 1.35 \times 2.33' \approx 10 \text{ K/FT}$$

Analyze "Typical Composite Section" one Counterfort + old wall (9' section) + 9' section of Spillway on piles.

| Section | (wt.) | (dist. from "0") arm | Moment about "0" |
|--|-------------------------------------|----------------------|------------------|
| (.5 x 4.5 + 2 x 5 + .5 x 1.5 x 5) 16 | $\times .15 = 2.4$ | 10.71' | 25.71K |
| Counterfort + .83 (2 x 3 + 2 x 1.25 + 1.5 x 1.25 + 1.25 x 1.25) 24 | $\times .15 = \frac{3.6}{.07} = .4$ | 9.21' | 3.71K |
| Pile arm 2 x 1' + Radius Portion | $20 \times .15 = 3.0$ | 5.0' | 15.0 |
| (1/2 x 1.5 x 7 + 1.5 x 3 + 9(0.75)) 11.67 | $\times .15 = 1.75$ | 6.67' | 11.67 |
| | | | <u>56.01K</u> |

D-1



$$M_R = 56 \text{ .1K}$$

$$\Sigma F_v = 7.55K$$

$$F_{H.R.} = \frac{F_v}{C \text{ Coef. friction}} = \frac{7.55 \times .6}{1} = 4.53$$

$$F.S.S.L. = \frac{4.53 + 7.2}{3} = 1.75$$

Low but ok

$$P_{ass.} = .5 \times 2^2 \times 3 \times .12 = .72 K/ft$$

$$\frac{6.09}{10} = .616 \text{ OK}$$

$$F.S.C.T. = \frac{56}{10} = 5.6 \text{ OK}$$

$$Upl. ft = \frac{2}{3} \times .0624 \times 10 = .416 K/ft$$

Press on Piles : 9' Area

$$R = \frac{56 \times 9 - 10 \times 9}{7.55 \times 9} = 6.09' \quad e = \frac{13.25}{2} - 6.09 = .54'$$

$$S.P. = \frac{7.55 \times 9}{9(10)} \left(1 \pm \frac{6 \times .54}{10} \right) = \frac{1.33}{.68} = 1.0 \times 9$$

$$Ld / Pile = \frac{11.16}{2} \times \frac{10}{3} = 18.6 K/Pile \approx \text{say } 10 \text{ T/Pile}$$

Mom. @ base of Counterfort :

$$P_w = .187 K/sf \times \frac{3}{2} = .28 K/ft \times 9' = 2.52 K \times 5' = 12.5 K$$

$$P_2 = .187 \times 4 \times .748 \times 9 \times 2 = 13.46 K$$

$$P_3 = .5 \times 4^2 \times .055 = .44 \times 9 \times 1.33 = 5.27 K$$

$$\Sigma M_{CT} = 31.23 K$$

$$d = 36.3 - 5/16 = 32.6875$$

$$A_g = \frac{31.23}{1.44 \times 32.68} = .67 \text{ in}^2/ft.$$

$$2 \text{ #5 / Counterfort } \underline{1K}$$

$$Upl. ft : \frac{2}{3} \times 10' \times .0624 = .42 K/sf \uparrow$$

vs .24 K/sf + resultant tension in conc.
 Neg.



Normal Cond. + Ice loading.

5' @ 10' above toe of section

$$F_H = 5' / \text{ft} \quad M_{OT} = 50' \text{K}$$

$$F_{SCL} = \frac{5.25}{8} = 0.65$$

* Neg
Loc.

$$F_{SOT} = \frac{56}{60} = 0.93$$

High Water Analysis

4.2' above level of old sect.

$$P_1 = \frac{4.2^2}{2} \times 0.0624 = .55' \text{K} \rightarrow$$

Loc. of Res.

$$P_2 = (4.2 \times 0.0624) \times 7 = 1.83' \text{K} \rightarrow$$

$$\frac{56 - 14.2}{7.55} = \frac{5.54}{10} = 0.55' \text{OK}$$

$$P_3 = 1.35' / \text{ft} \rightarrow \quad \Sigma F_H = 3.73' \text{K} \rightarrow$$

$$M_{OT} = .55 \times 8.4 + 1.83 \times 3.5 + 1.35 \times 2.33 = 14.2' \text{K}$$

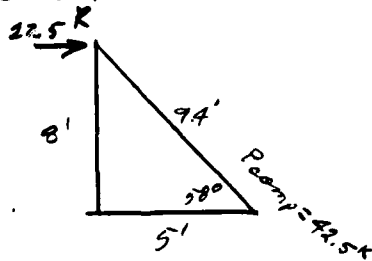
$$F_{SCL} = \frac{5.25' / \text{ft}}{3.73' / \text{ft}} = 1.4 \quad \underline{\text{Low}}$$

$$F_{SOT} = \frac{56.0}{14.2} = 3.94 \quad \underline{\text{OK}}$$

Uplift & Conc. stresses will not be meaningfully changed by add'l ht. of water.

Check Steel Section: Used as Col.

Ice Ld on
 Flashbd. Post
 $5 \times 9 = 22.5' \text{K}$



$$\frac{L}{r_{min}} = \frac{9.4}{.41} = 22.9$$

$$F_a = 20.41$$

$$\frac{42.5}{20.41} = 2.08 \text{ in}^2 \text{ min.}$$

C3x5 A=10.47

max allow Ld. = 30'K < 42.5

small channel is ineffective as support for flashbd. supports
 recommend in-plane "K" Bracing.



.5 PMF w/ flashboards:

Ht. of water 8.9' above Spillway crest

$$P_w = 8.9 \times .0624 = 0.56 \text{ K/Ft.}$$

$$P_1 = .56 \times \frac{8.9}{2} = 2.24 \text{ K/Ft.}$$

$$P_2 = .56 \times 7 = 3.92 \text{ K/Ft.}$$

$$P_3 = 1.35 \text{ K/Ft.}$$

$$\Sigma M.O.T. = 2.24 \times (7 + \frac{8.9}{3}) = 21.65 \text{ 'K} + 3.92 \times 3.5' + 1.35 \times 2.33' = 36 \text{ 'K}$$

$$\Sigma P_H = 7.51 \text{ K}$$

$$F.S.S.L. = \frac{5.25}{7.51} = 0.70 \text{ Unstable}$$

$$F.S.O.T. = \frac{56.0}{36} = 1.56 < 2 \text{ Undesirable}$$

$$Loc. \text{ of Res. } \frac{36 - 36}{56 - 36} = 2.65 \div 10 = .276$$

.5 PMF w/o Flashboards:

Ht. of water 7.9' above Spillway Crest

$$P_w = 7.9 \times .0624 = 0.49 \text{ K/Ft}^2$$

$$P_1 = .49 \times \frac{7.9}{2} = 1.95 \text{ K/Ft.}$$

$$P_2 = .49 \times 7' = 3.43 \text{ K/Ft.}$$

$$P_3 = 1.35 \text{ K/Ft.}$$

$$P_H = 1.95 + 3.43 + 1.35 = 6.28 \text{ K/Ft.}$$

$$M.O.T. = 1.95 \times (7 + \frac{7.9}{3}) + 3.43 \times 3.5 + 1.35 \times 2.33 = 33.9 \text{ 'K}$$

$$F.S.S.L. = \frac{5.25}{6.28} = 0.84 \text{ Unstable}$$

$$F.S.O.T. = \frac{56}{34} = 1.65 < 2 \text{ Undesirable}$$

$$Loc. \text{ of Res. } \frac{56 - 34}{7.55} = \frac{2.91}{D-4} \quad .296$$

APPENDIX E

PREVIOUS INSPECTION REPORTS/AVAILABLE DOCUMENTS

PREVIOUS REPORTS

(NOTICE: After filling out one of these forms as completely as possible for each dam in your district, return it at once to the Conservation Commission, Albany.)

STATE OF NEW YORK
CONSERVATION COMMISSION
ALBANY

DAM REPORT

Carpenters, N.Y. 17th, 1913
(Date)

CONSERVATION COMMISSION,

DIVISION OF INLAND WATERS.

GENTLEMEN:

I have the honor to make the following report in relation to the structure known as the Pumping Station Dam.

This dam is situated upon the Saugerties river
(Give name of stream)
in the Town of Albany & Middletown, Albany County,
about 1/4 mile from the Village or City of Carpenters, N.Y.
(State distance)
The distance up stream from the dam, to the bridge
(Up or down) (Give name of nearest important stream or of a bridge)
is about 40 feet
(State distance)

The dam is now owned by Carpenters Aqueduct Co. & Auburn Co.
(Give name in full)
and was built in or about the year 1910, and was extensively repaired or reconstructed during the year 1910.

As it now stands, the spillway portion of this dam is built of files + concrete
(State whether of masonry, concrete or timber)
and the other portions are built of same
(State whether of masonry, concrete, earth or timber with or without rock fill)

As nearly as I can learn, the character of the foundation bed under the spillway portion of the dam is clay and under the remaining portions such foundation bed is clay.

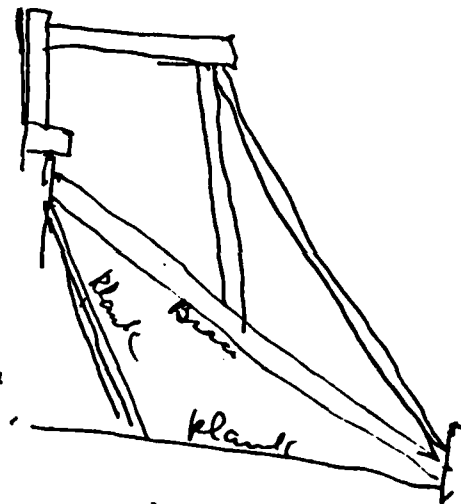
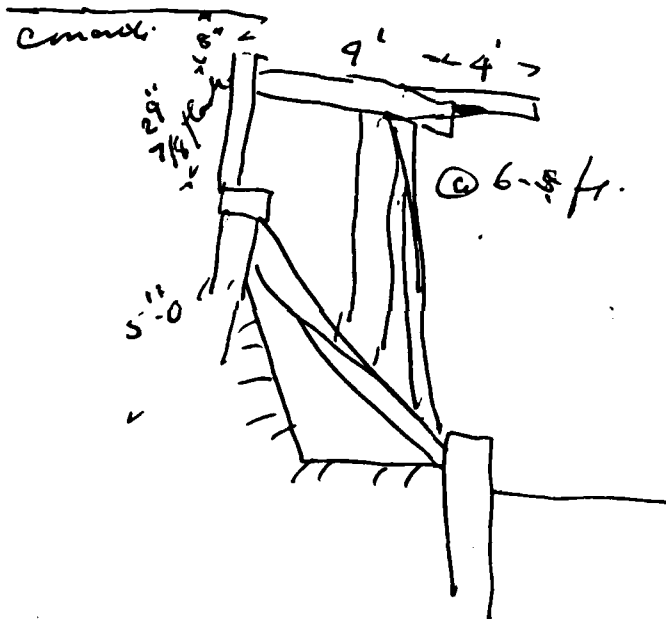
The total length of this dam is 35 feet. The spillway or waste-weir portion, is about same feet long, and the crest of the spillway is about 1 1/2 feet below the top of the dam.

The number, size and location of discharge pipes, waste pipes or gates which may be used for drawing off the water from behind the dam, are as follows: one, which is conducted by canal to Pumping Station

State briefly, in the space below, whether, in your judgment, this dam is in good condition, or bad condition, describing particularly any leaks or cracks which you may have observed.)

This dam was repaired in 1910, and should say was in great condition.

30 May 15
A R M-12



Reported by

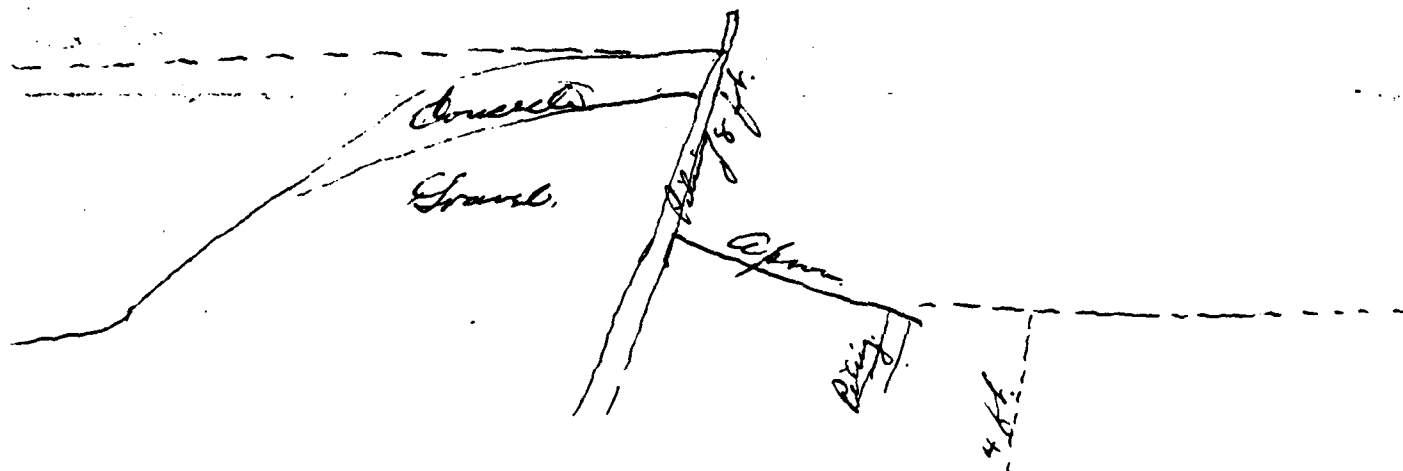
W. J. Hurrell
(Signature)

(Address—Street and number, P. O. Box or R. F. D. route)

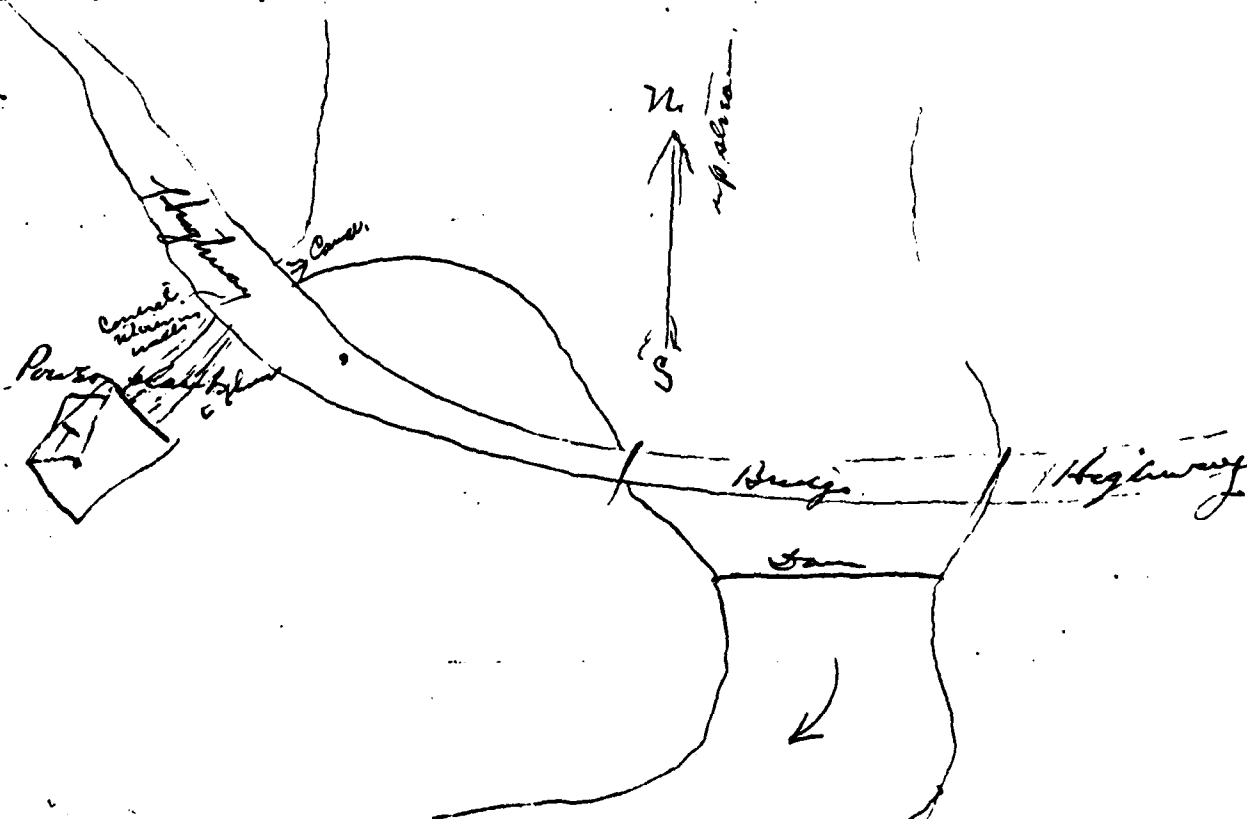
Mount Vernon, W. Va.
(Name of place)

(SEE OTHER SIDE)

(In the space below, make one sketch showing the form and dimensions of a cross section through the spillway or waste-weir of this dam, and a second sketch showing the same information for a cross section through the other portion of the dam. Show particularly the greatest height of the dam above the stream bed, its thickness at the top, and thickness at the bottom, as nearly as you can learn.)



(In the space below, make a third sketch showing the general plan of the dam, and its approximate position in relation to buildings or other conspicuous objects in the vicinity.)



(NOTICE: After filling out one of these forms as completely as possible for each dam in your district, return it at once to the Conservation Commission, Albany.)

STATE OF NEW YORK
CONSERVATION COMMISSION
ALBANY

DAM REPORT

June 6, 1917
(Date)

CONSERVATION COMMISSION,

DIVISION OF INLAND WATERS.

GENTLEMEN:

I have the honor to make the following report in relation to the structure known as the Map 144 ~~XXXXXX~~ 918 Sus Dam.

This dam is situated upon the Susquehanna River
(Give name of stream)
in the Town of Cooperstown, Otsego County,
about $\frac{1}{2}$ mile from the Village or City of Cooperstown.
(State distance)
The distance down stream from the dam, to the Otsego Lake
(Up or down) (Give name of nearest important stream or of a bridge)
is about one mile.
(State distance)

The dam is now owned by Mrs J. A. M. Johnson, Cooperstown, N.Y.
(Give name in full)
and was built in or about the year , and was extensively repaired or reconstructed during the year .

As it now stands, the spillway portion of this dam is built of timber
(State whether of masonry, concrete or timber)
and the other portions are built of concrete, timber with rock fill
(State whether of masonry, concrete, earth or timber with or without rock fill)

As nearly as I can learn, the character of the foundation bed under the spillway portion of the dam is rock with earth fill and under the remaining portions such foundation bed is earth & small stones

The total length of this dam is 60 feet. The spillway or waste-weir portion, is about 80 feet long, and the crest of the spillway is about 1.2 feet below the top of the dam.

The number, size and location of discharge pipes, waste pipes or gates which may be used for drawing off the water from behind the dam, are as follows: There are

no gates. The dam is merely used to collect water for milling

State briefly, in the space below, whether, in your judgment, this dam is in good condition, or bad condition, describing particularly any leaks or cracks which you may have observed.)

This dam is in good condition. The parts
subject to wear are built of concrete and the concrete
is as yet still in good condition.

Reported by William L. Steford
(Signature)

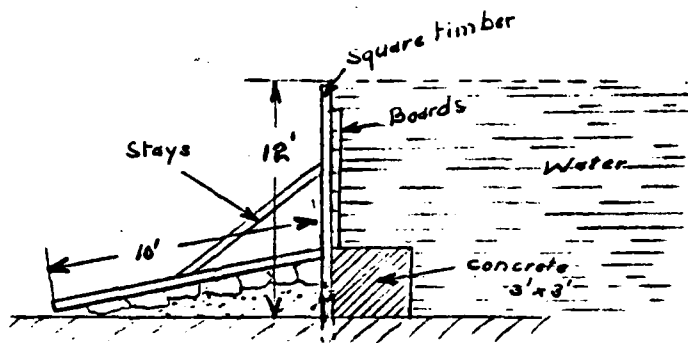
Conservation Commission, Albany, N.Y.
(Address—Street and number, P. O. Box or R. F. D. route)

Coopersstown, N.Y.
(Name of place)

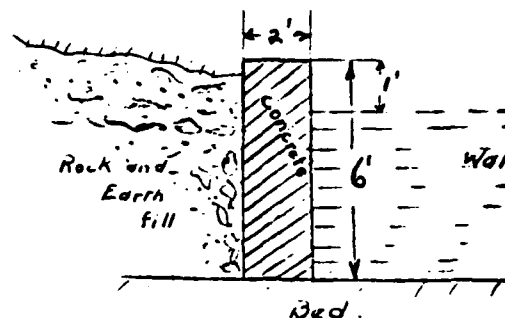
(SEE OTHER SIDE)

(In the space below, make one sketch showing the form and dimensions of a cross section through the spillway or waste-weir of this dam, and a second sketch showing the same information for a cross section through the other portion of the dam. Show particularly the greatest height of the dam above the stream bed, its thickness at the top, and thickness at the bottom, as nearly as you can learn.)

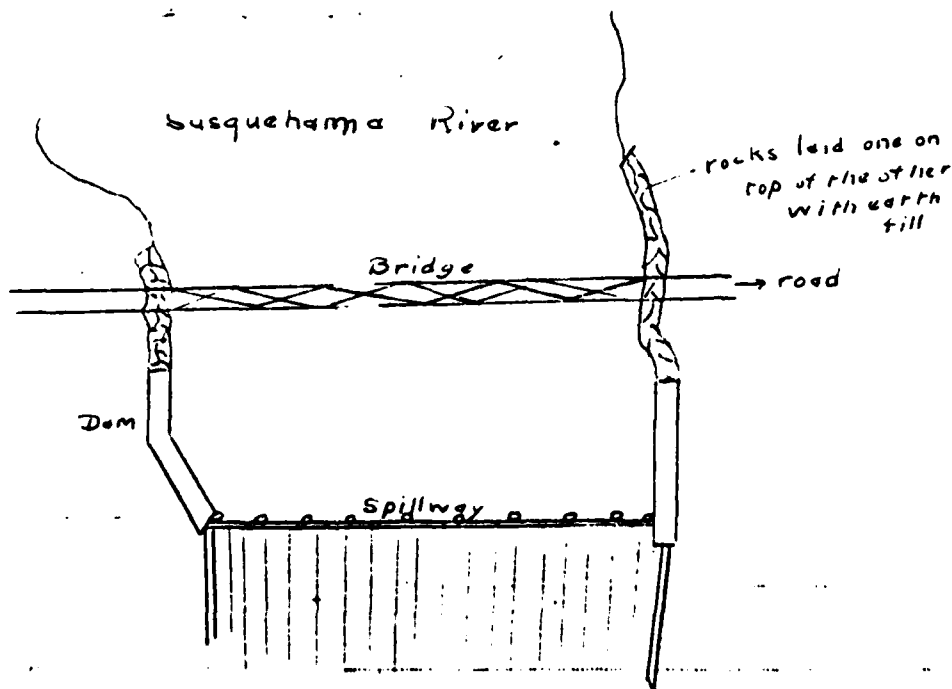
Cross-section thru Spillway.



Cross-section thru Dam.



(In the space below, make a third sketch showing the general plan of the dam, and its approximate position in relation to buildings or other conspicuous objects in the vicinity.)



PREVIOUS INSPECTION REPORTS

DEC DAM INSPECTION REPORT

outlet of Otsego Lake

| | | | | | | |
|-----------------------------|-----------------------------|-----------------------------|---------------------------------|---------------------------------|------------------------------|----------------------------|
| <input type="checkbox"/> 06 | <input type="checkbox"/> 39 | <input type="checkbox"/> 01 | <input type="checkbox"/> 000918 | <input type="checkbox"/> 102971 | <input type="checkbox"/> 002 | <input type="checkbox"/> 4 |
| RB | CTY | YR. AP. | DAM NO. | INS. DATE | USE | TYPE |

Reconstructed

AS BUILT INSPECTION

of concrete

☐ Location of Spillway
and outlet☐ Elevations☐ Size of Spillway
and outlet☐ Geometry of
Non-overflow section☐ GENERAL CONDITION OF NON-OVERFLOW SECTION☐ Settlement☐ Cracks☐ Deflections☐ Joints☐ Surface of
Concrete☐ Leakage☐ Undermining☐ Settlement of
Embankment☐ Crest of Dam☐ Downstream
Slope☐ Upstream
Slope☐ Toe of
Slope☐ GENERAL CONDITION OF SPILLWAY AND OUTLET WORKS☐ Auxiliary
Spillway☐ Service or
Concrete Spillway☐ Stilling
Basin☐ Joints☐ Surface of
Concrete☐ Spillway
Toe☐ Mechanical
Equipment☐ Plunge
Pool☐ Drain☐ Maintenance☐ Hazard Class☐ Evaluation☐ InspectorCOMMENTS:

new dam in good condition

APPENDIX F

REFERENCES

REFERENCES

1. Chow, Ven Te, Editor - Handbook of Applied Hydrology. McGraw-Hill Book Company, New York, New York, 1964.
2. Hydrologic Engineering Center, U.S. Army Corps of Engineers, HEC-1 Flood Hydrograph Package, Users Manual. Davis, California, January 1973.
3. Hydrologic Engineering Center, U.S. Army Corps of Engineers, Flood Hydrograph Package (HEC-1), Users Manual for Dam Safety Investigations, Davis, California, September 1978.
4. King, Horace and Brater, Ernest. Handbook of Hydraulics, 5th Edition. McGraw-Hill Book Company, New York, New York, 1963.
5. Riedel, J.T., Appleby, J.F. and Schloemer, R.W. Seasonal Variation of the Probable Maximum Precipitation East of the 105th Meridian for Areas from 10 to 1000 Square Miles and Durations of 6, 12, 24, and 48 Hours (Hydrometeorological Report No. 33) U.S. Department of Commerce - Weather Bureau and U.S. Department of the Army - Corps of Engineers, Washington, D.C., April 1956
6. U.S. Department of the Interior, Bureau of Reclamation, Design of Small Dams, Second Edition, Washington, D.C., 1973.

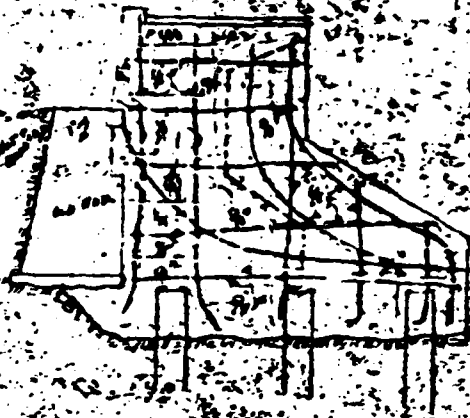
APPENDIX G

DRAWINGS

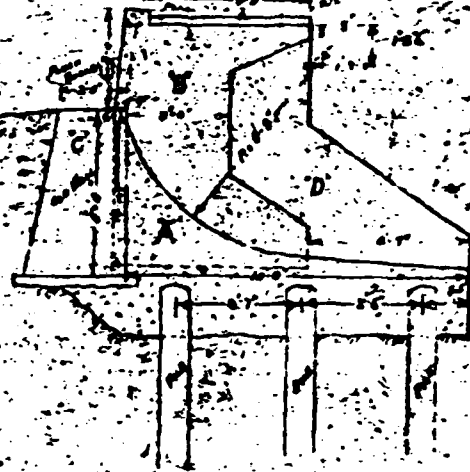
THE MUNICIPAL WATER
COOPERSTOWN, NEW YORK
PLANS FOR REPAIRS TO BE MADE TO
SCALE 1/2" = 1'

1953

DETAIL E
SCALE 1/2" = 1'

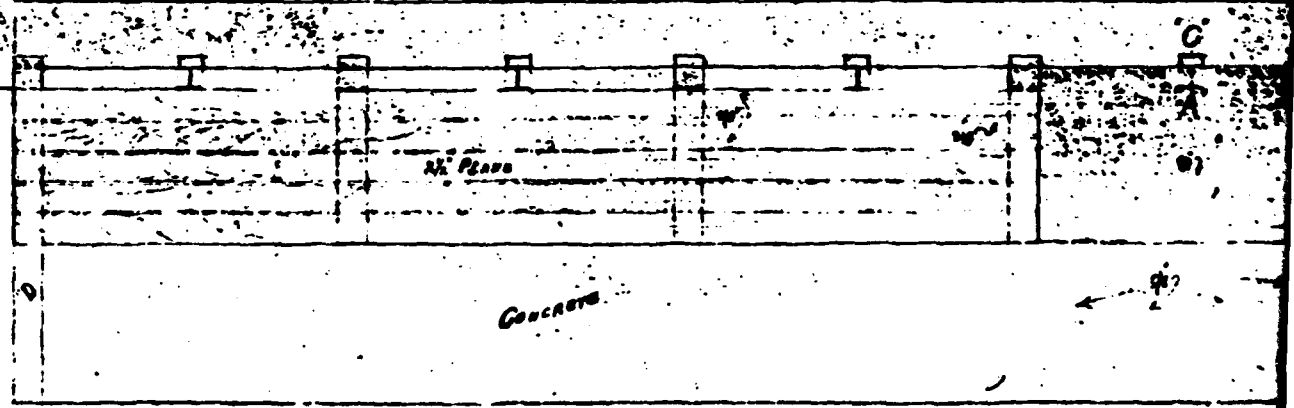


SECTIONS A-B-C-D
SHOWING LOCATION OF
REINFORCING RODS
SCALE 1/2" = 1'



SECTIONS A-B-C-D
SCALE 1/2" = 1'

NOTE -
THIS WALL
TO BE REBUILT



CHECK ALL MEASUREMENTS ON THE JOB

RIVER

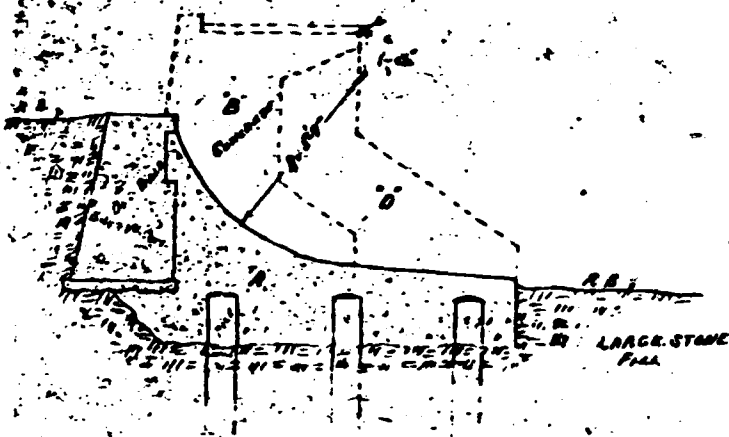
MUNICIPAL WATER WORKS

STOWN, NEW YORK

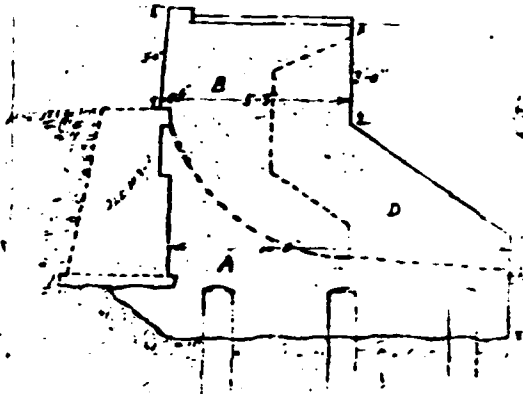
TO BE MADE TO PRESENT DAM

AS $\frac{1}{2}$ " = 1'

153



SECTION THRU 'A'
SCALE $\frac{1}{2}$ " = 1'



SECTION THRU 'D'
SCALE $\frac{1}{2}$ " = 1'

RIVER

OLD WALL

STEEL POST
SEE DETAIL

E

6'0" 18"

K

5' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

6' 0"

PLAN
SCALE $\frac{1}{2}$ " = 1'



G-1

Note:
THIS WALL
BE REINFORCED

2

END

DATE
FILMED

2-8



AD-A109 795

FLAHERTY-GIAVARA ASSOCIATES NEW HAVEN CT
NATIONAL DAM SAFETY PROGRAM. OTSEGO LAKE DAM (INVENTORY NUMBER --ETC(U)
JUL 81 H C FLAHERTY DACW51-81-C-0006

F/G 13/13

UNCLASSIFIED

NL

7 of 7
WORK



END
DATE
FILMED
4-82
DTIC

AD
AIO

SUPPLEMENTARY

INFORMATION

| | | | | | | | | | |
|------|------|------|------|------|-------|-------|-------|-------|------|
| 5173 | 6361 | 7370 | 8727 | 9723 | 10429 | 10782 | 10787 | 10427 | 9777 |
| 8948 | 8121 | 7268 | 4304 | 3787 | 3173 | 4623 | 4134 | 3677 | 3304 |
| 2348 | 2124 | 2330 | 2083 | 1821 | 1809 | 1437 | 1303 | 1183 | 1073 |
| 1007 | 957 | 920 | 872 | 856 | 822 | 740 | 758 | 728 | 699 |

| | | | | |
|-------|--------|---------|---------|--------------|
| PEAK | 6-HOUR | 24-HOUR | 72-HOUR | TOTAL VOLUME |
| 10792 | 9087 | 4021 | 1661 | 199290 |
| 306 | 257 | 114 | 47 | 5643 |
| | 2 | 4 | 4 | 4 |
| | 23 | 103 | 106 | 106 |
| | 38 | 103 | 106 | 106 |
| | 45 | 7975 | 8235 | 8235 |
| | 5553 | 9837 | 10158 | 10158 |

| | | | |
|-----|--------|-------|------------|
| CFS | INCHES | AC-FT | THOUS CU M |
| | | | |

OVF

STATION 1

| INFLOW(I), OUTFLOW(O) AND OBSERVED FLOW(*) | | STATION 1 | |
|--|-------|-----------|-------|
| 1000. | 2000. | 3000. | 4000. |
| 0. | 11 | 12 | 13 |
| 1. | 13 | 14 | 15 |
| 2. | 14 | 15 | 16 |
| 3. | 15 | 16 | 17 |
| 4. | 16 | 17 | 18 |
| 5. | 17 | 18 | 19 |
| 6. | 18 | 19 | 20 |
| 7. | 19 | 20 | 21 |
| 8. | 20 | 21 | 22 |
| 9. | 21 | 22 | 23 |
| 10. | 22 | 23 | 24 |
| 11. | 23 | 24 | 25 |
| 12. | 24 | 25 | 26 |
| 13. | 25 | 26 | 27 |
| 14. | 26 | 27 | 28 |
| 15. | 27 | 28 | 29 |
| 16. | 28 | 29 | 30 |
| 17. | 29 | 30 | 31 |
| 18. | 30 | 31 | 32 |
| 19. | 31 | 32 | 33 |
| 20. | 32 | 33 | 34 |
| | 33 | 34 | 35 |
| | 34 | 35 | 36 |
| | 35 | 36 | 37 |
| | 36 | 37 | 38 |
| | 37 | 38 | 39 |
| | 38 | 39 | 40 |
| | 39 | 40 | |
| | 40 | | |

FLAHERTY GIAVARA ASSOCIATES, P. C.

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